

When installing the shaft and bearings into the bearing bore, push against the outer race. **Never** hit the balls or ball cage.

Press the outboard oil seal (18) into the bearing cap (12) with the lip positioned as shown in Figure 2. Replace the bearing cap gasket (11), and secure the bearing cap with the hardware (13 and 14). Be careful not to damage the oil seal lip on the shaft keyway.

Install the bearing housing O-ring (30).

Lubricate the bearing housing as indicated in LU-BRICATION.

Seal Installation

(Figures 2, 5, 6 and 7)



Most cleaning solvents are toxic and

flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Clean the seal cavity and shaft with a cloth soaked in fresh cleaning solvent. Inspect the stationary seat bore in the seal plate for dirt, nicks and burrs, and remove any that exist. The stationary seat bore must be completely clean before installing the seal.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

To ease installation of the seal, lubricate the shaft sleeve O-ring and the external stationary seat O-ring with a very small amount of light lubricating oil. See Figure 5 for seal part identification.

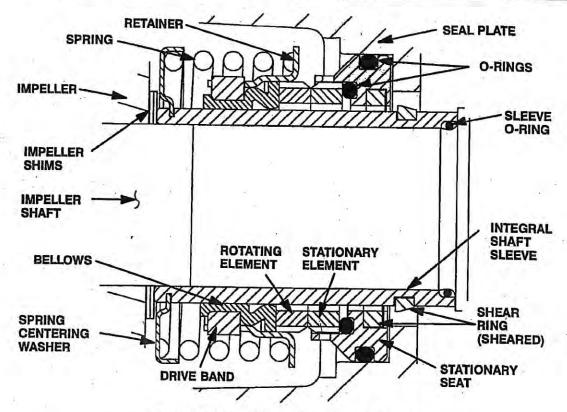


Figure 5. 46513-151 Cartridge Seal Assembly

(CAUTION

This seal is not designed for operation at temperatures above 160°F (71°C). Do not use at higher operating temperatures.

If the seal plate was removed, install the seal plate gasket (4). Position the seal plate over the shaft and secure it to the intermediate with the hardware (20 and 21).

To prevent damaging the shaft sleeve O-ring (28) on the shaft threads, stretch the O-ring over a piece of tubing 1-1/4 I.D. x 1-1/2 O.D. x 2-inches long (32 mm x 38 mm x 51 mm). Slide the tube over the shaft threads, then slide the O-ring off the tube and onto the shaft. Remove the tube, and continue to slide the O-ring down the shaft until it seats against the shaft shoulder.

When installing a new cartridge seal assembly, remove the seal from the container, and remove the mylar storage tabs, if so equipped, from between the seal faces.

(CAUTION

New cartridge seal assemblies may be equipped with mylar storage tabs between the seal faces. If so equipped, these storage tabs **must** be removed before installing the seal.

Lubricate the external stationary seat O-ring with light oil. Slide the seal assembly onto the shaft until the external stationary seat O-ring engages the bore in the seal plate.

Clean and inspect the impeller as described in Impeller Installation and Adjustment. Install the full set of impeller shims (29) provided with the seal, and screw the impeller onto the shaft until it is seated against the seal (see Figure 6).

Continue to screw the impeller onto the shaft. This will press the stationary seat into the seal plate bore.

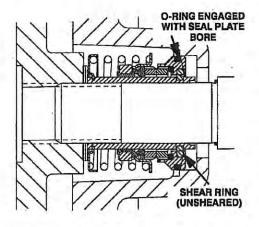


Figure 6. Seal Partially Installed

NOTE

A firm resistance will be felt as the impeller presses the stationary seat into the seal plate bore.

As the stationary seat becomes fully seated, the seal spring compresses, and the shaft sleeve will break the nylon shear ring. This allows the sleeve to slide down the shaft until seated against the shaft shoulder. Continue to screw the impeller onto the shaft until the impeller, shims, and sleeve are fully seated against the shaft shoulder (see Figure 7).

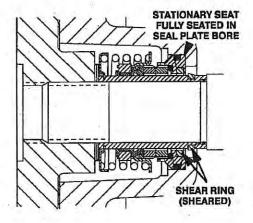


Figure 7. Seal Fully Installed

Measure the impeller-to-seal plate clearance, and remove impeller adjusting shims to obtain the proper clearance as described in impeller installation and Adjustment.

If necessary to reuse an old seal in an emergency, carefully separate the rotating and stationary seal faces from the bellows retainer and stationary seat.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

Handle the seal parts with extreme care to prevent damage. Be careful not to contaminate precision finished faces; even fingerprints on the faces can shorten seal life. If necessary, clean the faces with a non-oil based solvent and a clean, lint-free tissue. Wipe **lightly** in a concentric pattern to avoid scratching the faces.

Carefully wash all metallic parts in fresh cleaning solvent and allow to dry thoroughly.



Do not attempt to separate the rotating portion of the seal from the shaft sleeve when reusing an old seal. The rubber bellows will adhere to the sleeve during use, and attempting to separate them could damage the bellows.

Inspect the seal components for wear, scoring, grooves, and other damage that might cause leakage. Inspect the integral shaft sleeve for nicks or cuts on either end. If any components are worn, or the sleeve is damaged, replace the complete seal; never mix old and new seal parts.

Install the stationary seal element in the stationary seat. Press this stationary subassembly into the seal plate bore until it seats squarely against the bore shoulder. A push tube made from a piece of plastic pipe would aid this installation. The I.D. of

the pipe should be slightly larger than the O.D. of the shaft sleeve.

Slide the rotating portion of the seal (consisting of the integral shaft sleeve, spring centering washer, spring, bellows and retainer, and rotating element) onto the shaft until the seal faces contact.

Proceed with Impeller Installation and Adjustment.

Impeller installation

(Figure 2)

Inspect the impeller, and replace it if cracked or badly worn. Inspect the impeller and shaft threads for dirt or damage, and clean or dress the threads as required.



The shaft and impeller threads must be completely clean before reinstalling the impeller. Even the slightest amount of dirt on the threads can cause the impeller to seize to the shaft, making future removal difficult or impossible without damage to the impeller or shaft.

Install the same thickness of impeller adjusting shims (29) as previously removed. Apply 'Never-Seez' or equivalent to the shaft threads and screw the impeller onto the shaft until tight.

NOTE

At the slightest sign of binding, Immediately back the impeller off, and check the threads for dirt. Do not try to force the impeller onto the shaft.

A clearance of .025 to .040 Inch (0,64 to 1,02 mm) between the impeller and the seal plate is recommended for maximum pump efficiency. Measure this clearance, and add or remove impeller adjusting shims as required.

NOTE

If the rotating assembly has been installed in the pump casing, this clearance may be measured by reaching through the priming port with a feeler gauge.

NOTE

Proceed with Rotating Assembly Installation before installing the Impeller capscrew and washer (22 and 23). The rotating assembly must be installed in the pump casing in order to torque the impeller capscrew.

After the rotating assembly is installed in the pump casing, coat the threads of the impeller capscrew (23) with 'Never-Seez' or equivalent compound, and install the impeller washer (22) and capscrew; torque the capscrew to 90 ft. lbs. (1080 in. lbs. or 12,4 m. kg.).

Rotating Assembly Installation

(Figure 1)

NOTE

If the pump has been completely disassembled, it is recommended that the suction check valve and back cover assembly be reinstalled at this point. The back cover assembly must be in place to adjust the impeller face clearance.

Install the bearing housing and lubricate it with light grease. Ease the rotating assembly into the pump casing using the installation tool. **Be careful** not to damage the O-ring.

Install the four sets of rotating assembly adjusting shims (11) using the same thickness as previously removed. Secure the rotating assembly to the pump casing with the hardware (9 and 10). Do not fully tighten the capscrews until the back cover has been reinstalled and the impeller face clearance has been set.

A clearance of .010 to .020 inch (0,25 to 0,51 mm) between the impeller and the wear plate is also recommended for maximum pump efficiency. This clearance can be obtained by removing an equal amount of shims from each rotating assembly shim set until the impeller scrapes against the wear plate when the shaft is turned. After the impeller scrapes, add approximately .015 inch (0,4 mm) of shims to each shim set.

NOTE

An alternate method of adjusting this clearance is to

reach through the suction port with a feeler gauge and measure the gap. Add or subtract rotating assembly shims accordingly.

Suction Check Valve Installation

(Figure 1)

Inspect the check valve assembly (29), and replace it if badly worn.

NOTE

The check valve assembly must be replaced as a complete unit. Individual parts are not sold separately.

Reach through the back cover opening with the check valve (29), and position the check valve adaptor in the mounting slot in the suction flange (30). Align the adaptor with the flange hole, and secure the assembly with the check valve pin (31).

NOTE

If the suction or discharge flanges were removed, replace the respective gaskets, apply 'Permatex Aviation No. 3 Form-A-Gasket' or equivalent compound to the mating surfaces, and secure them to the pump casing with the attaching hardware.

Back Cover Installation

(Figure 1)

If the wear plate (12) was removed for replacement, carefully center it on the back cover and secure it with the hardware (13 and 14). The wear plate must be concentric to prevent binding when the back cover is installed.

Replace the back cover O-ring (15), and lubricate it with a generous amount of No. 2 grease. Clean any scale or debris from the contacting surfaces in the pump casing that might interfere or prevent a good seal with the back cover. Slide the back cover assembly into the pump casing. Be sure the wear plate does not bind against the impeller.

NOTE

To ease future disassembly, apply a film of grease or 'Never-Seez' on the back cover shoulder, or any

surface which contacts the pump casing. This action will reduce rust and scale build-up.

Secure the back cover assembly by tightening the back cover nuts (24) evenly. Do not over-tighten the hand nuts; they should be just tight enough to ensure a good seal at the back cover shoulder. Be sure the wear plate does not bind against the casing.

PRESSURE RELIEF VALVE MAINTENANCE

(Figure 1)

The back cover is equipped with a pressure relief valve (20) to provide additional safety for the pump and operator (refer to Liquid Temperature And Overheating in OPERATION).

It is recommended that the pressure relief valve assembly be replaced at each overhaul, or any time the pump overheats and activates the valve. **Never** replace this valve with a substitute which has not been specified or provided by the Gorman-Rupp Company.

Periodically, the valve should be removed for inspection and cleaning. When reinstalling the relief valve, apply 'Loctite Pipe Sealant With Teflon No. 592', or equivalent compound, on the relief valve threads. Position the valve as shown in Figure 1 with the discharge port pointing down.

Final Pump Assembly

(Figure 1)

Install the shaft key (16, Figure 2) and reconnect the power source. Be sure to install any guards used over the rotating members.



Do not operate the pump without the guards in place over the rotating parts. Exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

Install the suction and discharge lines and open all valves. Make certain that all piping connections are tight, properly supported and secure.

Be sure the pump and power source have been properly lubricated, see LUBRICATION.

Remove the fill cover assembly (36) and fill the pump casing with clean liquid. Reinstall the fill cover and tighten it. Refer to OPERATION, Section C, before putting the pump back into service.

LUBRICATION

Seal Assembly

(Figure 2)

Before starting the pump, remove the vented plug (8) and fill the seal cavity with approximately 40 ounces (1,4 liters) of SAE No. 30 non-detergent oil, or to a level just below the tapped vented plug hole. Clean and reinstall the vented plug. Maintain the oil at this level.

Bearings

(Figure 2)

The bearing housing was fully lubricated when shipped from the factory. Check the oil level regularly through the sight gauge (24) and maintain it at the middle of the gauge. When lubrication is required, add SAE No. 30 non-detergent oil through the hole for the air vent (9). Do not over-lubricate.

Over-lubrication can cause the bearings to overheat, resulting in premature bearing failure.

NOTE

The white reflector in the sight gauge must be positioned horizontally to provide proper drainage.

Under normal conditions, drain the bearing housing once each year and refill with approximately 32 ounces (1 liter) clean oil. Change the oil more frequently if the pump is operated continuously or installed in an environment with rapid temperature change.



Monitor the condition of the bearing lubricant regularly for evidence of rust or moisture condensation. This is especially important in areas where variable hot and cold temperatures are common.

For cold weather operation, consult the factory or a lubricant supplier for the recommended grade of oil.

Power Source

Consult the literature supplied with the power source, or contact your local power source representative.

THE GORMAN-RUPP COMPANY AND GORMAN-RUPP OF CANADA LIMITED 12 MONTH LIMITED WARRANTY

EXTENT AND DURATION OF WARRANTY

Coverage: The Gorman-Rupp Company or Gorman-Rupp of Canada Limited (herein individually referred to as "GR") each individually warrant that its products and parts shall be free from defects in material and workmanship for twelve (12) months from the date of purchase by the original end user.

Exceptions: This Limited Warranty shall not apply to the following products and parts: engines, motors, trade accessories and other products, components or materials not manufactured by GR. With respect to submersible pumps, the pump and motor are an integral unit and are therefore warranted as a unit. However, with respect to the electrical components in submersible pumps, this warranty is valid only when electrical controls for the pump have been specified and/or provided by GR. Wear and tear on any product resulting from normal use is not covered by this Limited Warranty.

LIMITATIONS

GR'S SOLE AND EXCLUSIVE WARRANTY WITH RESPECT TO ITS PRODUCTS AND PARTS IS THIS LIMITED WARRANTY. THIS LIMITED WARRANTY IS IN LIEU OF ALL OTHER EXPRESS AND/OR IMPLIED WARRANTIES, INCLUDING IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR PARTICULAR PURPOSE.

EXCLUSIVE REMEDY AND DAMAGES

The sole and exclusive remedy for breach of this Limited Warranty by GR, and the entire extent of its liability for such breach or for damages arising and/or resulting from the use of the products and parts covered by this Limited Warranty shall be as follows:

- 1. Repair or replacement: If inspection shows that any GR product or part covered under this LimitedWarranty is defective in materials or workmanship, GR shall repair or replace the defective product or part at its option, without charge. You must have properly installed, maintained and used the product or part claimed to be defective in accordance with the maintenance schedule and/or manual which comes with the product. No allowance will be made for labor, transportation or other charges incurred by you in connection with such repair or replacement.
- 2. To obtain the above remedy:
 - a) Immediately notify GR at the address below of the claimed defect in materials or workmanship and provide the serial number or date code of the product and/or part and provide a copy of the invoice or bill of sale referencing the product and/or part by no later than the expiration date of the Limited Warranty period.
 - b) GR will advise whether inspection of the product and/or part will be necessary and whether and how repair or replacement will be effected. If inspection by GR is necessary, the product or part must be sent freight prepaid to GR at the address stated below. Return shipment of the repaired product or part will be F.O.B. the address stated below.
- 3. Damages: GR's liability for damages for breach of this Limited Warranty shall not exceed the amount of the purchase price of the product or part in respect to which damages are claimed. IN NO EVENT SHALL GR BE LIABLE FOR INCIDENTAL, CONSEQUENTIAL OR SPECIAL DAMAGES FOR BREACH OF THIS LIMITED WARRANTY OTHER THAN AS STATED HEREIN.

Some states do not allow the exclusion or limitation of incidental or consequential damages. Accordingly, the above may not apply to you. This Limited Warranty gives you specific legal rights, and you may also have other rights which vary from state to state and province to province.

THE GORMAN-RUPP COMPANY P.O. BOX 1217 MANSFIELD, OH 44901—1217 Phone: (419) 755—1011 GORMAN-RUPP OF CANADA LIMITED 70 Burwell Road St. Thomas, Ontario N5P 3R7 Phone: (519) 631–2870



Appendix D Testing Results

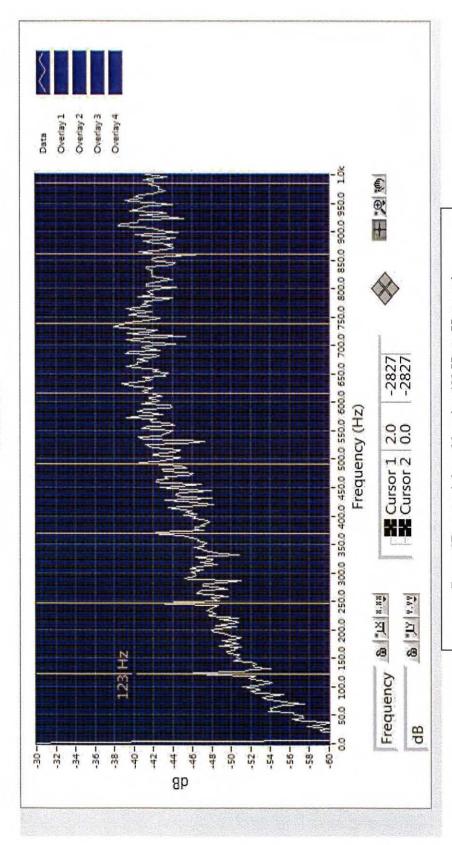


Exhibit 1

				Ultr	sonic Da	ta ~ Woo	Ultrasonic Data ~ Woodland Manor Pump Station
Date	Location Name	Point Name	Location Name Point Name Point Number	8	Frequency Sensitivity	Sensitivity	Comments
10/16/2013 10:50	PUMP 1A	MTR-0B	1	41	30	45	Noise time domain 50 percent scale - Indicative of need for Relubrication
10/16/2013 10:50	PUMP 1A	MTR-1B	2	33	30	53	Noise time domain - less saturated than all other motor bearings - Relube ASAP
10/16/2013 10:52	PUMP 1A	PU-BOTH	3	43	30	43	FFT Clean
10/16/2013 11:14	PUMP 1B	MTR-08	4	46	30	39	Time domain noisy peaking 100 percent full scale - indicative of a very dry bearing - Relube ASAP
10/16/2013 11:15	PUMP 1B	MTR-IB	2	48	30	37	Time domain noisy - 124 hertz spike starting in FFT - Bearing sounds dry - Relube ASAP
10/16/2013 11:16	PUMP 1B	PU-BOTH	9	46	30	39	Time Domain Very Noisy -
10/16/2013 11:35	PUMP 2A	MTR-0B\	7	49	30	37	FFT clean - Time domain very noisy - Bearing sounds dry - Relube ASAP
10/16/2013 11:36	PUMP 2A	MTR-18	8	49	30	37	FFT Clean - Time Domain is very noisy - Relube ASAP
10/16/2013 11:37	PUMP 2A	PU-BOTH	6	42	30	44	FFT clean waveform
10/16/2013 11:58	PUMP 2B	MTR-0B\	10	49	30	38	Time Domain is noisy - Relube ASAP
10/16/2013 11:59	PUMP 2B	MTR-IB	11	47	30	39	123 Hz harmonic present - Noisy time domain - Relube as soon as possible
10/16/2013 12:00	PUMP 2B	РО-ВОТН	12	41	30	45	FFT Clean Waveform
ACCUMPANAGORISH SPECIAL PROPERTY.	CONTRACTOR STATE OF THE PARTY O	- Contraction of the contraction	The second secon		The same of the sa		The state of the s



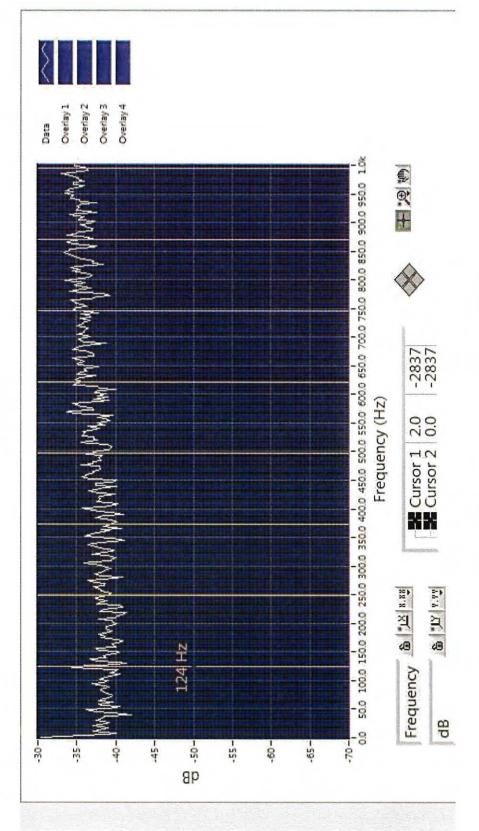
Exhibit 2



Pump 2B motor inboard bearing 123 Hertz Harmonic



Exhibit 3



Pump 1B motor inboard bearing Small 124 Hertz Spike



Exhibit 4 ${\bf Motor\ Insulation\ Resistance\ Testing \sim Woodlands\ Manor\ Pump\ Station}$

Date	Location Name	Point Name	Resistance test	
10/16/2013	PUMP 1A	Motor	1.46	Gig Ohms
10/16/2013	PUMP 1B	Motor	1.55	Gig Ohms
10/16/2013	PUMP 2A	Motor	1.77	Gig Ohms
10/16/2013	PUMP 2B	Motor	1.58	Gig Ohms

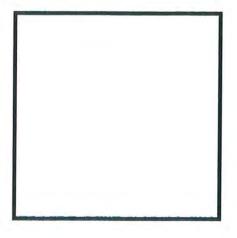
Exhibit 5

Thermal imaging ~ Woodland Manor pump station

Date	Location Name	Point Name	Thermal Imaging (infrared)
10/16/2013	PUMP 1A	Motor	No abnormal heating patterns observed
10/16/2013	PUMP 1A	Pump	No abnormal heating patterns observed
10/16/2013	PUMP 1B	Motor	No abnormal heating patterns observed
10/16/2013	PUMP 1B	Pump	No abnormal heating patterns observed
10/16/2013	PUMP 2A	Motor	No abnormal heating patterns observed
10/16/2013	PUMP 2A	Pump	No abnormal heating patterns observed
10/16/2013	PUMP 2B	Motor	No abnormal heating patterns observed
10/16/2013	PUMP 2B	Pump	No abnormal heating patterns observed



Woodland Manor Sewer Pump Station & Tiogue Avenue Sewer Force Main, Coventry Rhode Island



Woodland Manor Sewer Pump Station

Located in Coventry, Rhode Island Prepared For: HallKeen Real Estate Management and Investment

7-14-09

Revised 11-17-09

Two Stafford Court Cranston, RI 02920 Tel: (401) 943-1000 Fax: (401) 464-6006 www.DiPrete-Eng.com



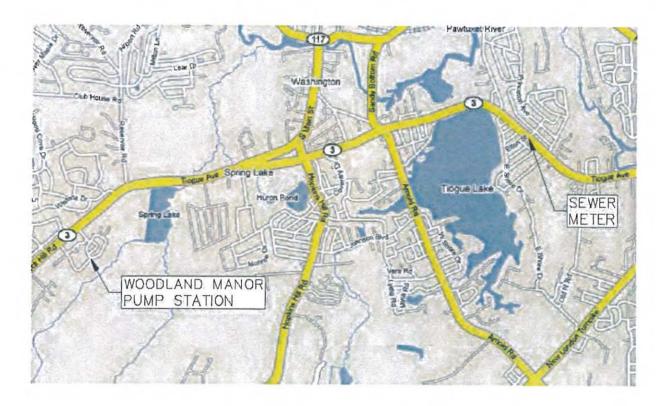
Table of Contents

Executive Summary	
1.0 Pump Station Evaluation and Inspection	1
1.1 Sewer Pump Station Inspection	1
1.2 Sewer Pump Station Inspection Photos	3
2.0 Sewer Force Main Pump Station Flow Study	
2.1 Sewer Force Main Meter Inspection	15
2.2 Sewer Force Main Meter Inspection Photos	17
2.3 Sewer Force Connection List and Calculations	21
2.4 Sewer Flow Study Conclusion	25
3.0 Summary of Findings and Recommendations	27
3.1 Maintenance Recommendations	27
3.2 General Recommendations	29
3.3 Operation and Maintenance Plan	29
4.0 Supporting Documentation	115
4.1 Sewer Connection Information	117
4.2 Kent County Water Authority Water Billing Information	131

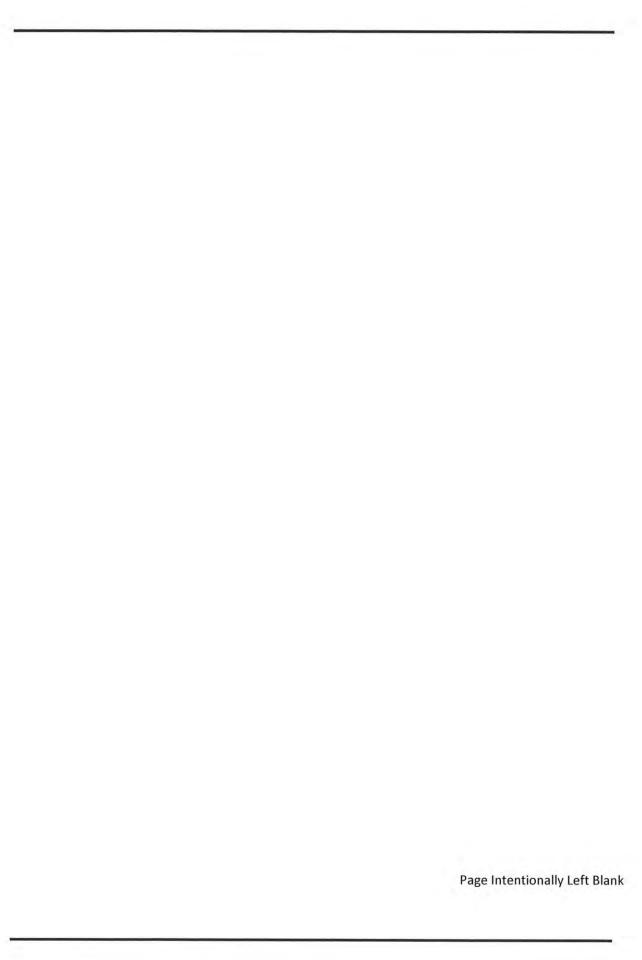


Executive Summary

The project is an evaluation of the existing private sewer pump station located at the Woodland Manor apartment complex in Coventry, Rhode Island. The pump station was built approximately 30 years ago and is connected to a sewer force main that runs east up to Tiogue Avenue (RI Rt. 3) for roughly three miles where it discharges into the City of West Warwick's gravity sewer system located at the town line. Along the private line there are several private businesses connected into the line.



This report details the inspection and evaluation of the existing sewer pump station. It also documents all known connections to the system and results of the sewer flow study that was conducted on the system. It then provides recommendations for future operation and maintenance of the pump station and sewer force main.



1.0 Pump Station Evaluation and Inspection

1.1 SEWER PUMP STATION INSPECTION

On September 19, 2008, representatives from DiPrete Engineering and Boydco Inc. of East Providence, RI conducted an inspection of the existing sewer pump station which services Woodland Manor. The Boydco engineers have extensive experience designing, installing and maintaining sewer pump stations. Below is a summary of Boydco's observations.

Pumps

The pump station is 30 years old with four self priming Gorman-Rupp (G-R) sewage pumps that are arranged in two sets of series pumps that may operate in parallel but are designed to handle the load with a single pair. The serial and model numbers of the pumps are as follows:

Pump	Serial Number	Model Number
1A*	1073103	Т6АЗ-В
1B	1192685	Т6АЗ-В
2A	1141725	Т6А60-В
2B	725344	Т6АЗ-В

^{*}Pump 1A is believed to be original while the remaining three have been replaced.

- When we arrived on 9/19/08, one pair of pumps (pumps 1A and 1B) was in the process of being rebuilt and therefore unavailable for testing.
- Pump discharges are tied into a common 8" diameter discharge which has a flow meter in the common discharge line.
- The remaining set of pumps has been arranged to run on a temporary basis by a pair of float switches which run across the ground under the station's door and into the motor control center through the partially closed door on the Motor Control Cabinet (MCC). Floats are required due to the removal of the unoperational automatic level control system. The MCC is showing signs of age and corrosion along with extensive rusting on the lower portions of the steel cabinet.
- The G-R sewage pumps are running very smoothly but are not pumping at the desired rate most likely due to accumulated wear within pump volutes and possible fouling within the piping and valves. Pump 1A has a different casing than the other pumps. A test gauge was installed but was unable to obtain an accurate reading due to an accumulation of debris. The air release valve attached to the pumps was not operational and was combined with the air release valve from the other series of pumps.
- It is true the rotating elements have been replaced but it seems to have been unsuccessful in restoring capacity of the pumps.

1

Flow Meter

- The flow meter indicates flow when pumps are running. Flow registers between 4.0-4.5 as the pump runs and flow in force main becomes stable. If the force main is 10" in diameter it would require a flow of 600 GPM to achieve self cleaning velocity of 2.5 FPS. This indicates that the remaining pair of pumps is pumping at a lower than designed volume and or that the flowmeter has lost calibration over its installed service life. There are several other issues with the installation of the meter including insufficient lay length without interruption or velocity change.
- If the meter is to be used for revenue or billing it must be repaired or replaced to have some assurance of accuracy.

Other Issues

- The Motor Control Center is of questionable reliability and it would require rebuilding or replacement if it is to be counted on to provide satisfactory service.
- The air release valve line running out of the pump station is currently split and attached to both series of pumps.
- The water supply to the building is located at the bottom of the stairs roughly six inches off the ground.
- Other problems within the station include lack of any system to lift or hoist pumps into place, failing lights, leaking chemical piping, and other housekeeping issues.
- A source of backup power was not observed and it is not clear how the station would remain functional during a power loss.

On December 22, 2008 representatives from DiPrete Engineering, Hayes Pump Inc. and Boydco conducted a follow-up inspection of the sewer pump station. Hayes Pump Inc. was present to record serial numbers from the pumps and from any other applicable components.

Upon entering the station it was clear that the two pumps that were offline at the time of the September inspection had been repaired and were now operational. The automatic level control system has been replaced and the float switches located at the outside holding tank have been removed. Therefore there is no longer a power cord running across the floor and out the door.

Please refer to the Summary of Findings and Recommendation (Section 3.0) for Boydco's recommendations for repairs and future maintenance.

1.2 SEWER PUMP STATION INSPECTION PHOTOS



Figure 1: One of the G-RT6A3-B pumps

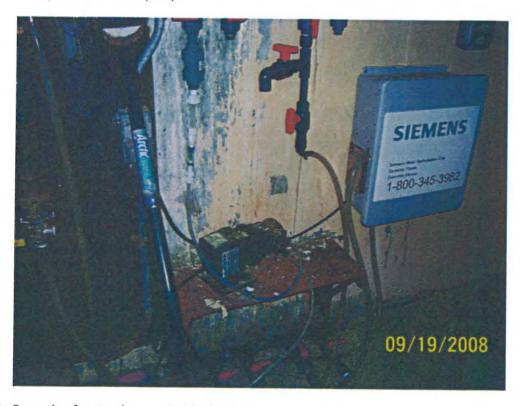


Figure 2: Example of water damage inside the station

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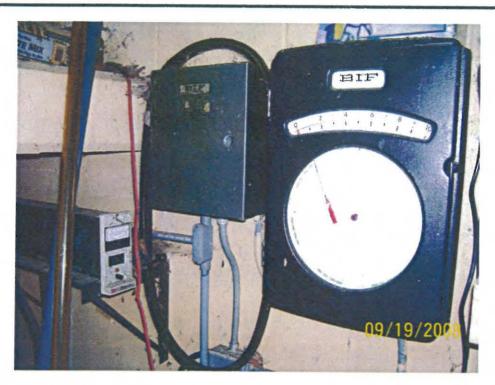


Figure 3: Existing sewer flow meter

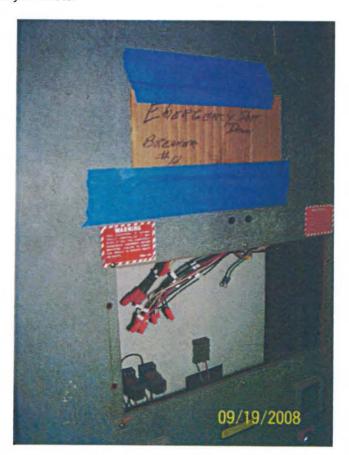


Figure 4: Missing float control panel (since repaired)

Page Intentionally Left Blank 6 APPENDIX K



Figure 5: Combined air release



Figure 6: Pump in process of being repaired (since completed)

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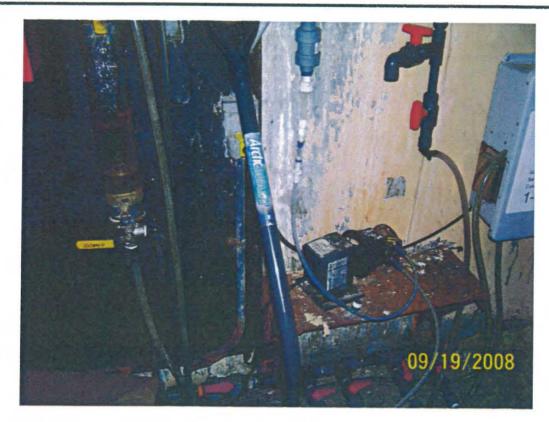


Figure 7: Various water damage and housekeeping issues

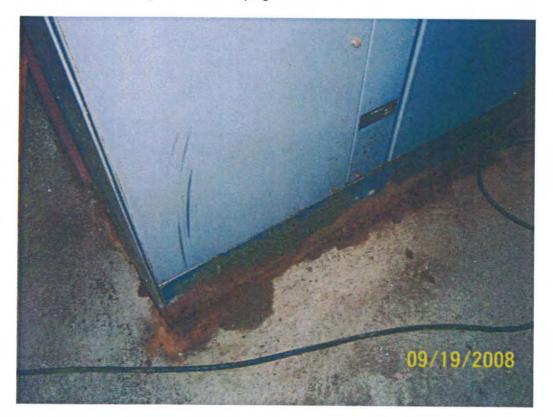


Figure 8: Rust at bottom of control panel cabinet

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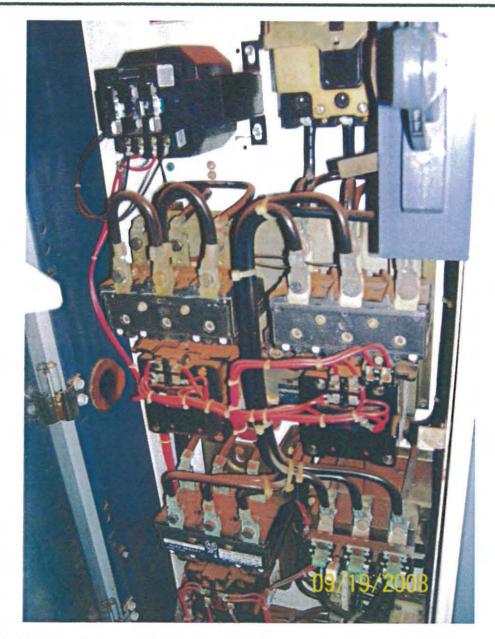


Figure 9: Inside of the motor control center





Figure 10: Inside of motor control center



Figure 11: Inside of motor control center showing evidence of water pooling

1470-002 Woodland Manor Sewer Pump Station

APPENDIX K

14

2.0 Pump Station Flow Study

2.1 SEWER FORCE MAIN METER INSPECTION

On November 25, 2008 representatives from DiPrete Engineering and Boydco conducted an inspection of the existing sewer meter located along the sewer force main at the intersection of Tiogue Avenue and Darton Street in Coventry, Rhode Island. The sewer force main then runs in a gravity state for approximately 1000' until it ties into the City of West Warwick's gravity sewer system at the Coventry-West Warwick line.

The sewer meter was found to be in good condition and was running as designed. Sewer flow readings through the meter were taken for nine weeks starting on September 29 and continuing until November 25, 2008. The results were as follows:

Start	Duration (mins)	Total Flow (gal)	Average Flow (gpm)	Average Flow (gpd)
9/29/2008 19:30	9000	506,546.2	56.28	81,047.39
10/6/2008 1:30	9000	483,492.8	53.72	77,358.85
10/12/2008 7:30	9000	468,027.8	52.00	74,884.45
10/18/2008 13:30	9000	467,313.3	51.92	74,770.13
10/24/2008 19:30	9000	452,630.8	50.29	72,420.93
10/31/2008 1:30	9000	424,204.2	47.13	67,872.67
11/6/2008 7:30	9000	428,686	47.63	68,589.76
11/12/2008 13:30	9000	452,374.7	50.26	72,379.95
11/18/2008 19:30	9000	215,366.9	23.93	34,458.70*
11/25/2008 1:30	2138	107,412.3	50.24	72,345.05
		Overall Average Flow	48.34	73,518.80

^{*}This period was during the week of Thanksgiving, and since some businesses discharging into the sewer force main were closed, the values from this week were not used in the analysis for the Overall Average Flow.



2.1 SEWER FORCE MAIN METER INSPECTION PHOTOS



Figure 12: Sewer force main meter enclosure located on Tiogue Avenue



Figure 13: Inside of meter cabinet



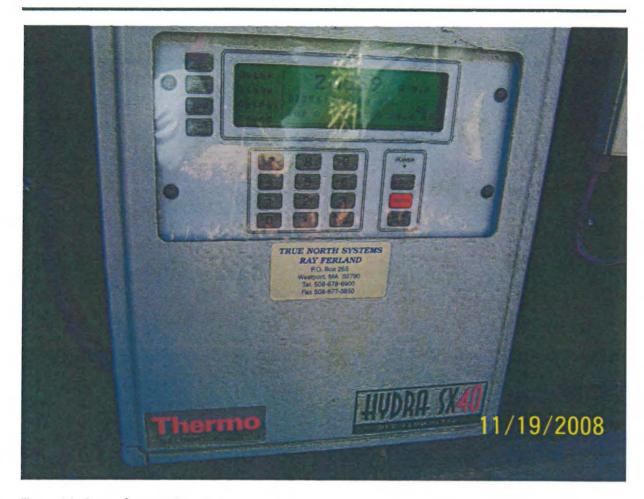


Figure 14: Sewer force main meter



2.3 SEWER FORCE CONNECTION LIST AND CALCULATIONS

DiPrete Engineering worked with the West Warwick Sewer Authority, James Geremia and Associates (the Sewer Authority consultants), the Kent County Water Authority (KCWA), and other sources to review the current connections and usage of the system. The usage information was obtained from the most recent KCWA water billings unless otherwise noted.

The connections and flow information and can be found on the following page:



Connection	Connection Address	Usage (cu. ft.)	Usage (gal)	Billing Period	Duration (days)	Water Usage (gpd)
Woodland Manor Apartments	20 Woodland Drive, Coventry RI	112,805.00	843,781.40	80/08-8/30/08/9	92	9,171.54
Borelli's Pastry Shop	765 Tiogue Avenue, Coventry RI	5,700.00	42,636.00	3/27/08-7/06/08	103	413.94
Boston Neck Realty	1650 Nooseneck Hill Road, Coventry RI	23,000.00	172,040.00	3/27/08-7/15-08	110	1.564.00
Coventry Credit Union	1076 Main Street, Coventry RI	3,300.00	24,684.00	4/22/08-7/29/08	86	251.88
CVS (Site #00621-01)	743 Tiogue Avenue, Coventry RI	3,000.00	22,440.00	3/27/08-7/08/0/	103	217.86
Vacant Unit						20:11
Haven Health Center	10 Woodland Drive, Coventry RI	257,500.00	1,926,100.00	80/08-8/30/08	92	20 935 87
Leisure Village	1620 Nooseneck Hill Road, Coventry RI	36,000.00	269,280.00	6/30/08-9/30/09	92	2,926.96
Soco Inc./ Leisure Condos	1700 Nooseneck Hill Road, Coventry RI	7,000.00	52,360.00	7/15/08-10/31/08	108	484.81
Star Brite Car Wash	1620 Nooseneck Hill Road, Coventry RI	16,000.00	119,680.00	7/16/08-10/31/08	107	1.118.50
Star Brite Laundromat	1602 Nooseneck Hill Road, Coventry RI	39,000.00	291,720.00	8/31/08-9/31/08	30	9.724.00
Father Paul R. Grenon (SS. John and Paul) Church	341 South Main Street, Coventry RI	16,991.00	127,092.68	4/09/08-7/14/08	96	1,323,88
Father John V Doyle School	343 South Main Street, Coventry RI	4,000.00	29,920.00	4/11/08-7/14/08	94	318.30
Stop & Shop Supermarket Co.	900 Tiogue Avenue, Coventry RI	37,600.00	281,248.00	3/27/08-7/31/08	126	2,232.13
Taco Bell Corp (Store #5261)	784 Tiogue Avenue, Coventry RI	16,000.00	119,680.00	7/08/08-10/23/08	107	1,118.50
Tiogue Avenue Association	1036 Tiogue Avenue, Coventry RI					730.30
Tiogue Veterinary Clinic	916 Tiogue Avenue, Coventry RI	4,000.00	29,920.00	3/27/08-7/06/08	103	290.49
Tom's Fruit and Deli	821 Tiogue Avenue, Coventry RI	11,800.00	88,264.00	3/27/08-7/06/08	103	856.93
U.S. Postal Office	1550 Nooseneck Hill Road, Coventry RI	4,000.00	29,920.00	3/27/08-7/15/08	110	272.00
Wal-Mart Stores, Inc. (Store #228)	650 Centre of New England Blvd	68,501.00	512,387.48	12/27/07-3/24/08	88	5,822.59
Westwood Estates	14 Liena Rose Way, Coventry RI	526,000.00	3,934,480.00	7/10/08-10/1/08	94	6,455.00
VSH Realty (Cumberland Farms)	1600 Nooseneck Hill Road, Coventry RI	2,100.00	15,708.00	7/15/08-10/31/08	108	145.44
Vacant Unit						
Glenwood Park	978 Tiogue Avenue, Coventry RI	83,000.00	620,840.00	7-08/08-10/23/08	107	5,802.24
Kent County Hospital/Coventry Care	1620 Nooseneck Hill Road, Coventry RI	1,000.00	7,480.00	3/27/08-7/16/08	111	62.39
Kenyon Oil Company, Inc.	851 Tiogue Avenue, Coventry RI	5,900.00	44,132.00	7/08/08-10/23/08	107	412.45
						100

* KCWA usage information could not be obtained for this connection. In its place, water billing information obtained from Peter Castriotta was used in the calculations.

^{**} Westwood Estates is a large development which contains both individual septic disposal systems and a gravity sewer system which is pumped into the sewer force main. Since all units do not discharge into sewer force main, the average daily flow reading from the sewer pump located at Westwood Estates was used in the calculations.

The usage values for the most recent flow periods were compared to historical data for the largest users and can be considered consistent with the historical data,

2.4 FLOW STUDY CONCLUSION

The difference between the measured flow through the sewer force before it connects to the City of West Warwick Sewer System (73,518 gpd) and the calculated flow entering the system (72,657 gpd) is 861 gpd. This represents a 1.17% difference and can be considered insignificant. It is the conclusion of this study that there are no major leaks or infiltration in the sewer force main.

The sewer force main itself was not inspected in this study. The small difference between the metered flow and calculated flow (1.17%) does not indicate that the line needs to be inspected at this time.



3.0 Summary of Findings and Recommendations

3.1 MAINTENANCE RECOMMENDATIONS

There are several repair and maintenance issues that need to be addressed. These issues are:

The two pumps that are not operating should be brought back online immediately. It is
important to keep all four pumps online because if only one series of pumps is online the pump
station would become non-operational if the remaining pumps failed.

Update: As observed on the December 22, 2008 site inspection, all four pumps are now operational. This is no longer and issue.

- The pumps should be cleaned to remove accumulated debris to allow for pressure testing of the pumps.
- 3. The wet well should be cleaned to remove all accumulated solids and debris.
- 4. The automatic level control system has been removed and the pumps are setup to be activated by a float system in the holding tank. The float system is powered by an extension cord run from the floor of the pump station, up the stairs, out the door, across the ground to a manhole in the holding tank. The manhole cover is propped up with a stick and a shelf is laid across it to prevent anyone from disturbing it. This is not only an unreliable system but is a safety concern as the holding tank is open at all times. The automatic control system should be replaced and the float system removed.

Update: As observed on the December 22, 2008 site inspection, the automatic level control system has been repaired. This is no longer an issue.

- The meter does not seem to be reliable and is outdated. Boydco suggests installing a polysonic meter. These meters are more accurate and more cost-effective.
- The casing on Pump 1A should be replaced to match the other three pumps. This would increase the efficiency of the pump station and the life of the pump.
- The air release valve line running out of the pump station is currently split and attached to both series of pumps. An independent air release line should be installed for each series of pumps.
- 8. The motor control center (MCC) needs maintenance. For the most part the electrical components of the system are in good shape and with a minimal amount of repair should be restored optimal functionality. The steel cabinet the MCC is located in is heavily corroded and should be replaced and placed on a raised cement slab to prevent corrosion.
- A system should be installed to lift or hoist the pumps into place for maintenance and for future replacement.
- 10. There are several water leaks inside the pump station. This has resulted in corrosion of most of the metal casings for the various control and electrical panels. The water appears to be running over several electrical components. The water could easily short out electrical components and pose an electrocution risk to anyone working inside the pump station.
- 11. The chemical pipes have several leaks and treatment chemicals have been spilt throughout the pump station. These spills should be cleaned up and the pipes replaced.
- 12. The lighting in the pump station should be increased.
- 13. The pump station's heater and ventilator should be replaced.

- 14. The pump station's sump pumps should be replaced.
- 15. The water service to the building is located at floor level. In the future this should be raised above the level of the door in order to prevent it from being inaccessible if the station were to flood. When it is moved a backflow preventer should be installed.
- 16. If in the future the valves on the pumps discharge pipes are replaced, they should be replaced with plug valves and not the butterfly valves which are in place now.
- No source of backup power was observed, and this should be addressed in the future operation of the pump station.
- 18. In the future, the sewer force main meter located on Tiogue Avenue should be read monthly to monitor any changes in flows.

While this station is now handling the sewage flow, the station is of questionable reliability and may be subject to failure if the above repairs and upgrades are not completed.

Boydco has prepared quotes for the two essential repairs to the station. These repairs should be performed as soon as possible:

- Replace and repair the pump station' lights, sump pumps, ventilator, and heater. Clean all the
 debris out of pump station and store all equipment inside that will be reused in an orderly
 manner. Replace existing G-R control unit with new that will give an indication of wet well level
 with back up float switches to insure redundant control should primary level control fail.
 - Cost for this service including labor and materials not including RI Sales tax is \$13,660.00
- Clean the sewage wet well of accumulated solids and debris to include non hazardous regulated solids like fats, oil, & grease, along with grit and heavy materials in wet well bottom.

This quote covers up to removing and disposing of in an approved facility up to 9 tons of material. If the wet well has not been maintained any better than the station it is good practice to remove this material prior to it's damaging the recently installed pumps.

Cost for this service not including RI sales tax is \$8,000.00

In addition, it is DiPrete Engineering's recommendation that the operators of the Woodland Manor Pump Station contract Boydco for monthly inspections and maintenance of the pump station at the following budget:

Annual budgeted amount for monthly inspections and labor = \$4,704.00 Annual budgeted amount for routine part replacements = \$1,000.00 Total Annual Inspection Budget = \$5,704.00

DiPrete Engineering also anticipates significant repair and replacement obligations along the lines of the currently required repairs will be required every 5 to 10 years. We suggest utilizing the current Boydco repair and replacement quote of \$21,660.00 as a guide for these costs. Therefore, this results in an annual budget for repair and replacement of \$4,332.00 in addition to the annual inspection budget.

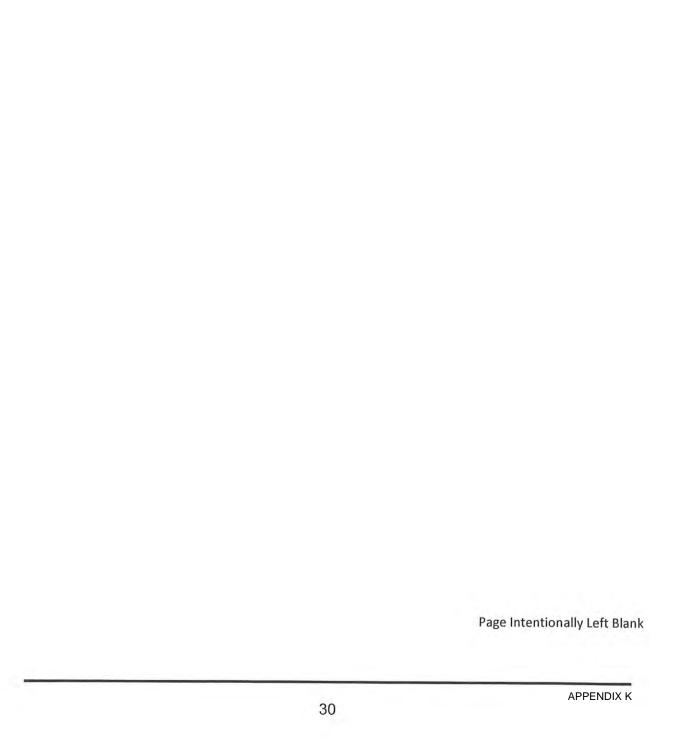
3.2 GENERAL RECOMMENDATIONS

While consulting with James Geremia and Associates it was brought to our attention that future sewer regulations will require that all private sewer line owners provide the sewer authority with an operation and maintenance plan and GIS mapping of all sewer line connections and components. This would involve additional services and could be completed by DiPrete Engineering in the future.

The cost to compile the plan and GIS data of the sewer force main system would range from \$5000-\$8000 depending on the level of effort required to locate the existing connections. We recommend using the operation and maintenance plan included in this report.

3.3 OPERATION AND MAINTENANCE PLAN

Boydco has prepared a proposal for a preventative maintenance plan for the sewer pump station. This can be found on the following pages.



101 Commercial Way East Providence, RI 02914 (401) 438-6900 Fax: (401) 438-6008

DATE:

February 6, 2009

TO:

Woodland Manor

Coventry, RI

RE:

Preventative Maintenance Proposal

Sewage Pump Station

This letter will serve as a quotation to you on a preventative maintenance contract for the above referenced project.

The maintenance performed at this station is on a monthly basis. The work performed at each visit would include:

- In compliance with OSHA'S 29 CFG part 1910 enacted 4/15/93 which dictates the entrance procedures into a confined space area, a pre-entry report and checklist will be performed. Maintain "Safe" job site for non-permit operation and entry.
- 2. Operate, inspect, and verify all electrical control circuits for proper operation.
- 3. Record pump amperage and voltage on all phases of the system, compare with specification, and report variances.
- 4. Check, inspect, and operate all mechanical equipment including manual operation of floats to check for proper alternation.
- 5. Test operation of check valves.
- 6. Check for proper operation of alarm equipment, if applicable.
- 7. Replace burned out light bulbs in control panel.
- 8. Replace corrosion inhibitors in control panel annually.
- 9. Inspect system for loose bolts and correct as required, (where accessible).
- 10. Check all joints and connections for leaks or cracks, (where accessible).
- 11. Treat wetwell with potassium permanganate to reduce accumulation of grease solids which inhibit pump performance.
- 12. Inspect pumps for fractures, corrosion, leaks, etc. where accessible and visually observe for proper operation.
- 13. Perform a draw-down test on both pumps to check pump performance.
- 14. A copy of maintenance report sent to you after each visit.

Sewage Pumping Station Water Booster Systems 101 Commercial Way East Providence, RI 02914 (401) 438-6900 Fax: (401) 438-6008

By having a preventative maintenance contract in effect, your repairs are automatically given a higher priority than if you were strictly on a 'call' basis. Maintenance contracts help to ensure that the expensive mechanical equipment you have in place is inspected, operated, and maintained so there will be a minimum of down-time or unscheduled repairs. These are always inconvenient and quite often more costly than if the problem had been attended to earlier.

BOYDCO recommends that this station be serviced on a monthly basis to ensure that it is maintained in proper operating efficiency. The cost for this service would be \$392.00 per visit.

This preventative maintenance contract does not include any parts or labor not specifically mentioned above. Any other parts could be furnished to you at a discounted price. Any labor not covered in the contract would be billed at a rate of \$90.00 per hour during normal working hours of 7:30 AM through 4:00 PM Monday through Friday. Any labor beyond these hours would be billed 1 1/2 times the normal rate. Any additional trips to your site would also be subject to a charge of \$1.25 per mile.

If you wish to accept this proposal, please sign and return a copy indicating acceptance. Please also provide the names and phone numbers of three (3) contact people on your staff so that if there is an emergency, problem, or a decision has to be made while servicing is going on, there would be a contact person available.

If I can provide any further help or clarify any of the matters outlined above, please do not hesitate to contact me.

Very truly yours,			
BOYDCO, INC.			
Jeffrey A. Fox			
Controller			
		Accepted by:	
		For:	
		Date:	
Contacts and phone numbers			
Name:	Number:		
Name:	Number:		
Name:	Number:		



33



INSTALLATION, OPERATION, AND MAINTENANCE MANUAL

WITH PARTS LIST



T SERIES PUMPS

MODELS

T6A3-B

INCLUDING: /F

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www.grpumps.com

GORMAN-RUPP OF CANADA LIMITED ● ST. THOMAS, ONTARIO, CANADA

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RECORD YOUR PUMP MODEL AND SERIAL NUMBER

Please	recora you	ir pump	mode	and	serial nur	mber in the
						distributo
needs th	nis informa	tion whe	en you	requir	e parts or	service.
Pump M	lodel:					
Serial N	umber:					

TABLE OF CONTENTS

INTRODUCTION	PAGE I – 1
SAFETY – SECTION A	PAGE A - 1
INSTALLATION – SECTION B	PAGE B - 1
Pump Dimensions	PAGE B - 1
PREINSTALLATION INSPECTION	
POSITIONING PUMP	
Lifting	
Mounting	
Clearance	
SUCTION AND DISCHARGE PIPING	
Materials	
Line Configuration	
Connections to Pump	
Gauges	PAGE B - 3
SUCTION LINES	PAGE B = 3
Fittings	PAGE B = 3
Strainers	PAGE B = 3
Sealing	PAGE B = 3
Suction Lines In Sumps	PAGE B - 3
Suction Line Positioning	PAGE B – 4
DISCHARGE LINES	PAGE B – 4
Siphoning	PAGE B = 4
Valves	PAGE B – 4
Bypass Lines	PAGE B - 5
AUTOMATIC AIR RELEASE VALVE	
Theory of Operation	PAGE B - 6
Air Release Valve Installation	
ALIGNMENT	PAGE B - 6 PAGE B - 7
Coupled Drives	PAGE B - 8
V-Belt Drives	PAGE B — 8
OPERATION – SECTION C	PAGE C - 1
PRIMING	PAGE C - 1
STARTING	PAGE C - 1
Rotation	PAGE C - 1
OPERATION	PAGE C - 2
Lines With a Bypass	PAGE C - 2
Lines Without a Bypass	PAGE C - 2
Leakage	PAGE C - 2
Liquid Temperature And Overheating	PAGE C - 2
Strainer Check	PAGE C - 3
Pump Vacuum Check	PAGE C - 3
STOPPING	PAGE C - 3
Cold Weather Preservation	PAGE C = 3
BEARING TEMPERATURE CHECK	PAGE C = 3

TABLE OF CONTENTS (continued)

TROUBLESHOOTING - SECTION D	PAGE D - 1
PREVENTIVE MAINTENANCE SCHEDULE	PAGE D - 3
PUMP MAINTENANCE AND REPAIR - SECTION E	PAGE E - 1
PERFORMANCE CURVE	PAGE E - 1
Pump Model	PAGE E - 3
Repair Rotating Assembly	PAGE E - 5
PUMP AND SEAL DISASSEMBLY AND REASSEMBLY	PAGE E - 6
Back Cover And Wear Plate Removal	PAGE E - 6
Suction Check Valve Removal	PAGE E - 6
Rotating Assembly Removal	PAGE E - 7
Impeller Removal	PAGE E - 7
Seal Removal	PAGE E - 8
Shaft and Bearing Removal and Disassembly	PAGE E - 8
Shaft and Bearing Reassembly and Installation	PAGE E - 9
Seal Installation	PAGE E - 10
Impeller Installation	PAGE E - 13
Rotating Assembly Installation	PAGE E - 13
Suction Check Valve Installation	PAGE E - 14
Back Cover Installation	PAGE E - 14
PRESSURE RELIEF VALVE MAINTENANCE	PAGE E - 14
Final Pump Assembly	PAGE E - 14
LUBRICATION	PAGE E - 15
Seal Assembly	PAGE E - 15
Bearings	PAGE E - 15
Power Source	PAGE E - 15

T SERIES OM-01046

INTRODUCTION

Thank You for purchasing a Gorman-Rupp pump. Read this manual carefully to learn how to safely install and operate your pump. Failure to do so could result in personal injury or damage to the pump. This Installation, Operation, and Maintenance manual is designed to help you achieve the best performance and longest life from your Gorman-Rupp pump.

This pump is a T Series, semi-open impeller, selfpriming centrifugal model with a suction check valve. The pump is designed for handling liquids containing large entrained solids and slurries. The basic material of construction is gray iron, with ductile iron impeller and steel wearing parts.

Because pump installations are seldom identical. this manual cannot possibly provide detailed instructions and precautions for every aspect of each specific application. Therefore, it is the responsibility of the owner/installer of the pump to ensure that applications not addressed in this manual are performed only after establishing that neither operator safety nor pump integrity are compromised by the installation. Pumps and related equipment must be installed and operated according to all national, local and industry standards.

If there are any questions regarding the pump or its application which are not covered in this manual or in other literature accompanying this unit, please contact your Gorman-Rupp distributor, or:

> The Gorman-Rupp Company P.O. Box 1217 Mansfield, Ohio 44901-1217 Phone: (419) 755-1011 or:

Gorman-Rupp of Canada Limited 70 Burwell Road St. Thomas, Ontario N5P 3R7 Phone: (519) 631-2870

For information or technical assistance on the power source, contact the power source manufacturer's local dealer or representative.

The following are used to alert maintenance personnel to procedures which require special attention, to those which could damage equipment, and to those which could be dangerous to personnel:



Immediate hazards which WILL result in severe personal injury or death. These instructions describe the procedure required and the injury which will result from failure to follow the procedure.



Hazards or unsafe practices which COULD result in severe personal injury or death. These instructions describe the procedure required and the injury which could result from failure to follow the procedure.



Hazards or unsafe practices which COULD result in minor personal injury or product or property damage. These instructions describe the requirements and the possible damage which could result from failure to follow the procedure.

NOTE

Instructions to aid in installation, operation, and maintenance or which clarify a procedure.

INTRODUCTION PAGE I - 1 39

SAFETY - SECTION A

This information applies to T Series basic pumps. Gorman-Rupp has no control over or particular knowledge of the power source which will be used. Refer to the manual accompanying the power source before attempting to begin operation.

Because pump installations are seldom identical, this manual cannot possibly provide detailed instructions and precautions for each specific application. Therefore, it is the owner/installer's responsibility to ensure that applications not addressed in this manual are performed only after establishing that neither operator safety nor pump integrity are compromised by the installation.



Before attempting to open or service the pump:

- Familiarize yourself with this manual.
- Disconnect or lock out the power source to ensure that the pump will remain inoperative.
- Allow the pump to completely cool if overheated.
- Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- Vent the pump slowly and cautiously.
- 7. Drain the pump.



This pump is designed to handle liquids

containing large entrained solids or slurries. Do not attempt to pump volatile, corrosive, or flammable materials which may damage the pump or endanger personnel as a result of pump failure.



After the pump has been positioned, make certain that the pump and all piping connections are tight, properly supported and secure before operation.



Do not operate the pump without the guards in place over the rotating parts. Exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

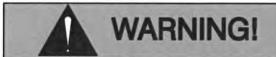


Do not remove plates, covers, gauges, pipe plugs, or fittings from an overheated pump. Vapor pressure within the pump can cause parts being disengaged to be ejected with great force. Allow the pump to completely completely cool before servicing.



Do not operate the pump against a closed discharge valve for long periods of time. If operated against a closed discharge valve, pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

OM-01046 T SERIES



Use lifting and moving equipment in good repair and with adequate capacity to prevent injuries to personnel or damage to equipment. Suction and discharge hoses and piping must be removed from the pump before lifting.



Do not attempt to disengage any part of an overheated pump unit. Vapor pressure within the pump casing can eject these parts with great force when they are disengaged. Allow the pump to completely cool before servicing it.



Pumps and related equipment must be installed and operated according to all national, local and industry standards.



Overheated pumps can cause severe burns and injury. If overheating of the pump occurs:

- 1. Stop the pump immediately.
- 2. Allow the pump to completely cool.
- 3. Refer to instructions in this manual before restarting the pump.

PAGE A - 2 SAFETY 41

INSTALLATION - SECTION B

Review all SAFETY information in Section A.

Since pump installations are seldom identical, this section offers only general recommendations and practices required to inspect, position, and arrange the pump and piping.

Most of the information pertains to a standard static lift application where the pump is positioned above the free level of liquid to be pumped.

If installed in a **flooded suction application** where the liquid is supplied to the pump under pressure, some of the information such as mounting, line configuration, and priming must be tailored to the specific application. Since the pressure supplied to the pump is critical to performance and safety, be sure to limit the incoming pressure to 50% of the maximum permissible operating pressure as shown on the pump performance curve.

For further assistance, contact your Gorman-Rupp distributor or the Gorman-Rupp Company.

Pump Dimensions

See Figure 1 for the approximate physical dimensions of this pump.

OUTLINE DRAWING

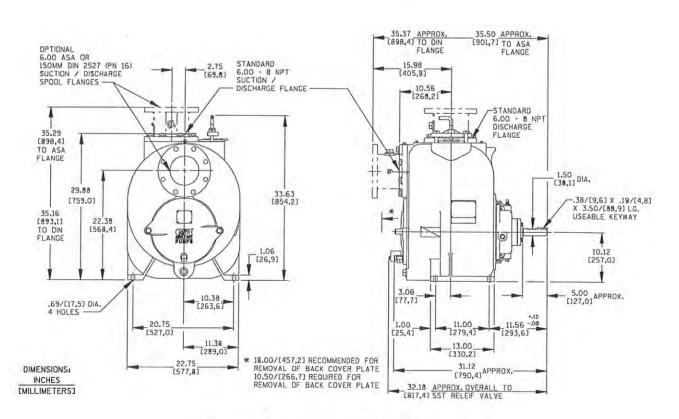


Figure 1. Pump Model T6A3-B, Including /F

OM-01046 T SERIES

PREINSTALLATION INSPECTION

The pump assembly was inspected and tested before shipment from the factory. Before installation, inspect the pump for damage which may have occurred during shipment. Check as follows:

- a. Inspect the pump for cracks, dents, damaged threads, and other obvious damage.
- b. Check for and tighten loose attaching hardware. Since gaskets tend to shrink after drying, check for loose hardware at mating surfaces.
- c. Carefully read all warnings and cautions contained in this manual or affixed to the pump, and perform all duties indicated. Note the direction of rotation indicated on the pump. Check that the pump shaft rotates counterclockwise when facing the impeller.



Only operate this pump in the direction indicated by the arrow on the pump body and on the accompanying decal. Refer to ROTATION in OPERATION, Section C.

- d. Check levels and lubricate as necessary. Refer to LUBRICATION in the MAINTENANCE AND REPAIR section of this manual and perform duties as instructed.
- e. If the pump and power source have been stored for more than 12 months, some of the components or lubricants may have exceeded their maximum shelf life. These must be inspected or replaced to ensure maximum pump service.

If the maximum shelf life has been exceeded, or if anything appears to be abnormal, contact your Gorman-Rupp distributor or the factory to determine the repair or updating policy. Do not put the pump into service until appropriate action has been taken.

POSITIONING PUMP

Lifting

Pump unit weights will vary depending on the mounting and drive provided. Check the shipping tag on the unit packaging for the actual weight, and use lifting equipment with appropriate capacity. Drain the pump and remove all customer-installed equipment such as suction and discharge hoses or piping before attempting to lift existing, installed units.



The pump assembly can be seriously damaged if the cables or chains used to lift and move the unit are improperly wrapped around the pump.

Mounting

Locate the pump in an accessible place as close as practical to the liquid being pumped. Level mounting is essential for proper operation.

The pump may have to be supported or shimmed to provide for level operation or to eliminate vibration.

Clearance

When positioning the pump, allow a minimum clearance of 18 inches (457 mm) in front of the back cover to permit removal of the cover and easy access to the pump interior.

SUCTION AND DISCHARGE PIPING

Pump performance is adversely effected by increased suction lift, discharge elevation, and friction losses. See the performance curve and operating range shown on Page E-1 to be sure your overall application allows pump to operate within the safe operation range.

Materials

Either pipe or hose maybe used for suction and discharge lines; however, the materials must be

PAGE B - 2 INSTALLATION 43

compatible with the liquid being pumped. If hose is used in suction lines, it must be the rigid-wall, reinforced type to prevent collapse under suction. Using piping couplings in suction lines is not recommended.

Line Configuration

Keep suction and discharge lines as straight as possible to minimize friction losses. Make minimum use of elbows and fittings, which substantially increase friction loss. If elbows are necessary, use the long-radius type to minimize friction loss.

Connections to Pump

Before tightening a connecting flange, align it exactly with the pump port. Never pull a pipe line into place by tightening the flange bolts and/or couplings.

Lines near the pump must be independently supported to avoid strain on the pump which could cause excessive vibration, decreased bearing life, and increased shaft and seal wear. If hose-type lines are used, they should have adequate support to secure them when filled with liquid and under pressure.

Gauges

Most pumps are drilled and tapped for installing discharge pressure and vacuum suction gauges. If these gauges are desired for pumps that are not tapped, drill and tap the suction and discharge lines not less than 18 inches (457,2 mm) from the suction and discharge ports and install the lines. Installation closer to the pump may result in erratic readings.

SUCTION LINES

To avoid air pockets which could affect pump priming, the suction line must be as short and direct as possible. When operation involves a suction lift, the line must always slope upward to the pump from the source of the liquid being pumped; if the line slopes down to the pump at any point along the suction run, air pockets will be created.

Fittings

Suction lines should be the same size as the pump inlet. If reducers are used in suction lines, they should be the eccentric type, and should be installed with the flat part of the reducers uppermost to avoid creating air pockets. Valves are not normally used in suction lines, but if a valve is used, install it with the stem horizontal to avoid air pockets.

Strainers

If a strainer is furnished with the pump, be certain to use it; any spherical solids which pass through a strainer furnished with the pump will also pass through the pump itself.

If a strainer is not furnished with the pump, but is installed by the pump user, make certain that the total area of the openings in the strainer is at least three or four times the cross section of the suction line, and that the openings will not permit passage of solids larger than the solids handling capability of the pump.

This pump is designed to handle up to 3-inch (76,2 mm) diameter spherical solids.

Sealing

Since even a slight leak will affect priming, head, and capacity, especially when operating with a high suction lift, all connections in the suction line should be sealed with pipe dope to ensure an airtight seal. Follow the sealant manufacturer's recommendations when selecting and applying the pipe dope. The pipe dope should be compatible with the liquid being pumped.

Suction Lines In Sumps

If a single suction line is installed in a sump, it should be positioned away from the wall of the sump at a distance equal to 1 1/2 times the diameter of the suction line.

If there is a liquid flow from an open pipe into the sump, the flow should be kept away from the suction inlet because the inflow will carry air down into the sump, and air entering the suction line will reduce pump efficiency.

OM-01046 T SERIES

If it is necessary to position inflow close to the suction inlet, install a baffle between the inflow and the suction inlet at a distance 1 1/2 times the diameter of the suction pipe. The baffle will allow entrained air to escape from the liquid before it is drawn into the suction inlet.

If two suction lines are installed in a single sump, the flow paths may interact, reducing the efficiency of one or both pumps. To avoid this, position the suction inlets so that they are separated by a distance equal to at least 3 times the diameter of the suction pipe.

Suction Line Positioning

The depth of submergence of the suction line is critical to efficient pump operation. Figure 2 shows recommended minimum submergence vs. velocity.

NOTE

The pipe submergence required may be reduced by installing a standard pipe increaser fitting at the end of the suction line. The larger opening size will reduce the inlet velocity. Calculate the required submergence using the following formula based on the increased opening size (area or diameter).

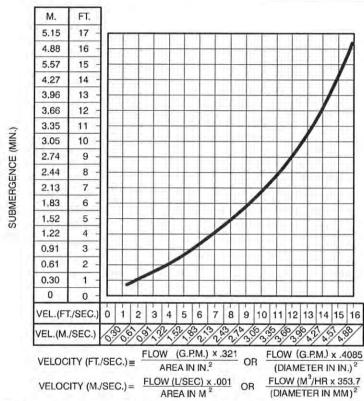


Figure 2. Recommended Minimum Suction Line Submergence vs. Velocity

DISCHARGE LINES

Valves

Siphoning

Do not terminate the discharge line at a level lower than that of the liquid being pumped unless a siphon breaker is used in the line. Otherwise, a siphoning action causing damage to the pump could result.

If a throttling valve is desired in the discharge line, use a valve as large as the largest pipe to minimize friction losses. Never install a throttling valve in a suction line.

With high discharge heads, it is recommended that a throttling valve and a system check valve be installed in the discharge line to protect the pump from excessive shock pressure and reverse rotation when it is stopped.

PAGE B – 4 INSTALLATION



If the application involves a high discharge head, gradually close the discharge throttling valve before stopping the pump.

Bypass Lines

Self-priming pumps are not air compressors. During the priming cycle, air from the suction line must be vented to atmosphere on the discharge side. If the discharge line is open, this air will be vented through the discharge. However, if a check valve has been installed in the discharge line, the discharge side of the pump must be opened to atmospheric pressure through a bypass line installed between the pump discharge and the check valve. A self-priming centrifugal pump will not prime if there is sufficient static liquid head to hold the discharge check valve closed.

NOTE

The bypass line should be sized so that it does not affect pump discharge capacity; however, the bypass line should be at least 1 inch in diameter to minimize the chance of plugging.

In low discharge head applications (less than 30 feet or 9 meters), it is recommended that the bypass line be run back to the wet well, and located 6 inches below the water level or cut-off point of the low level pump. In some installations, this bypass line may be terminated with a six-to-eight foot length of 1 1/4 inch I.D. smooth-bore hose; air and liquid vented during the priming process will then agitate the hose and break up any solids, grease, or other substances likely to cause clogging.



A bypass line that is returned to a wet well must be secured against being drawn into the pump suction inlet.

It is also recommended that pipe unions be installed at each 90° elbow in a bypass line to ease disassembly and maintenance.

In high discharge head applications (more than 30 feet), an excessive amount of liquid may be bypassed and forced back to the wet well under the full working pressure of the pump; this will reduce overall pumping efficiency. Therefore, it is recommended that a Gorman-Rupp Automatic Air Release Valve be installed in the bypass line.

Gorman-Rupp Automatic Air Release Valves are reliable, and require minimum maintenance. See AUTOMATIC AIR RELEASE VALVE in this section for installation and theory of operation of the Automatic Air Release Valve. Consult your Gorman-Rupp distributor, or contact the Gorman-Rupp Company for selection of an Automatic Air Release Valve to fit your application.

If the installation involves a flooded suction such as a below-ground lift station. A pipe union and manual shut-off valve may be installed in the bleed line to allow service of the valve without shutting down the station, and to eliminate the possibility of flooding. If a manual shut-off valve is installed **anywhere** in the air release piping, it **must** be a full-opening **ball type** valve to prevent plugging by solids.



If a manual shut-off valve is installed in a bypass line, it must not be left closed during operation. A closed manual shut-off valve may cause a pump which has lost prime to continue to operate without reaching prime, causing dangerous overheating and possible explosive rupture of the pump casing. Personnel could be severely injured.

Allow an over-heated pump to cool before servicing. Do not remove plates, covers, gauges, or fittings from an overheated pump. Liquid within the pump can reach boiling temperatures, and vapor pressure within the pump can cause parts being disengaged to be ejected with great force. After the pump cools, drain the liquid from the pump by removing the casing drain plug. Use cauOM-01046 T SERIES

tion when removing the plug to prevent injury to personnel from hot liquid.

AUTOMATIC AIR RELEASE VALVE

When properly installed, a Gorman-Rupp Automatic Air Release Valve will permit air to escape through the bypass line and then close automatically when the pump is fully primed and pumping at full capacity.



Some leakage (1 to 5 gallons [3.8 to 19

liters] per minute) will occur when the valve is fully closed. Be sure the bypass line is directed back to the wet well or tank to prevent hazardous spills.

Consult the manual accompanying the Air Release Valve for additional information on valve installation and performance.

Air Release Valve Installation

The Automatic Air Release Valve must be independently mounted in a horizontal position between the pump discharge port and the inlet side of the discharge check valve (see Figure 3). The inlet opening in the Air Release Valve is equipped with standard 1-inch NPT pipe threads.

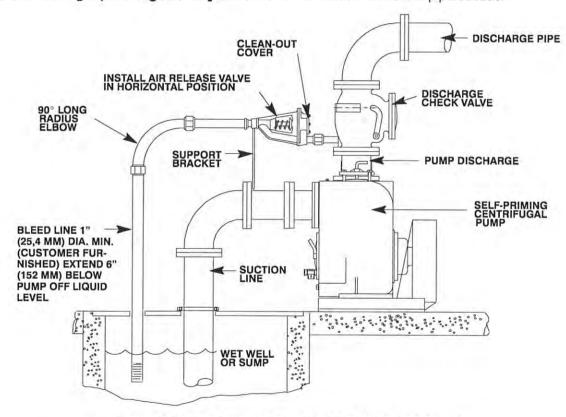


Figure 3. Typical Automatic Air Release Valve Installation

Connect the valve outlet to a bleed line which slopes back to the wet well or sump. The bleed line must be the same size as the outlet opening or larger, depending on which Air Release Valve is being used. If piping is used for the bleed line, avoid the use of elbows whenever possible.

NOTE

For multiple pump installations, it is recommended

that each Air Release Valve be fitted with an independent bleeder line directed back to the wet well. If multiple Air Release Valves are installed in a system, do not direct bleeder lines to a common manifold pipe. Contact your Gorman-Rupp distributor or the Gorman-Rupp Company for information about installation of an Automatic Air Release Valve for your specific application.

APPENDIX K

PAGE B - 6 INSTALLATION 47

ALIGNMENT

The alignment of the pump and its power source is critical for trouble-free mechanical operation. In either a flexible coupling or V-belt driven system, the driver and pump must be mounted so that their shafts are aligned with and parallel to each other. It is imperative that alignment be checked after the pump and piping are installed, and before operation.

NOTE

Check Rotation, Section C, before final alignment of the pump.

When mounted at the Gorman-Rupp factory, driver and pump are aligned before shipment. Misalignment will occur in transit and handling. Pumps must be checked and realigned before operation. Before checking alignment, tighten the foundation bolts. The pump casing feet and/or pedestal feet, and the driver mounting bolts should also be tightly secured.



When checking alignment, disconnect the power source to ensure that the pump will remain inoperative.



Adjusting the alignment in one direction may alter the alignment in another direction. check each procedure after altering alignment.

Coupled Drives

When using couplings, the axis of the power source must be aligned to the axis of the pump shaft in both the horizontal and vertical planes. Most couplings require a specific gap or clearance between the driving and the driven shafts. Refer to the coupling manufacturer's service literature.

Align spider insert type couplings by using calipers to measure the dimensions on the circumference of the outer ends of the coupling hub every 90°.

The coupling is in alignment when the hub ends are the same distance apart at all points (see Figure 4A).

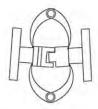


Figure 4A. Aligning Spider-Type Couplings

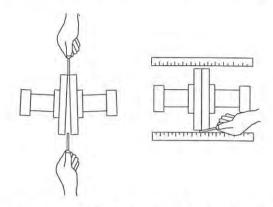


Figure 4B. Aligning Non-Spider Type Couplings

Align non-spider type couplings by using a feeler gauge or taper gauge between the coupling halves every 90°. The coupling is in alignment when the hubs are the same distance apart at all points (see Figure 4B).

Check parallel adjustment by laying a straightedge across both coupling rims at the top, bottom, and side. When the straightedge rests evenly on both halves of the coupling, the coupling is in horizontal parallel alignment. If the coupling is misaligned, use a feeler gauge between the coupling and the straightedge to measure the amount of misalignment.

V-Belt Drives

When using V-belt drives, the power source and the pump must be parallel. Use a straightedge along the sides of the pulleys to ensure that the pulleys are properly aligned (see Figure 4C). In drive systems using two or more belts, make certain that the belts are a matched set; unmatched sets will cause accelerated belt wear.

OM-01046 T SERIES

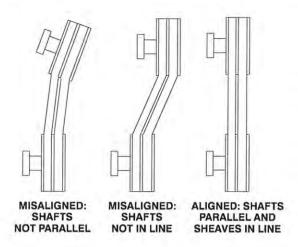


Figure 4C. Alignment of V-Belt Driven Pumps

Tighten the belts in accordance with the belt manufacturer's instructions. If the belts are too loose. they will slip; if the belts are too tight, there will be excessive power loss and possible bearing failure. Select pulleys that will match the proper speed ratio; overspeeding the pump may damage both pump and power source.



Do not operate the pump without the guard in place over the rotating parts. exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

DRIVE BELT TENSIONING

General Rules of Tensioning

For new drive belts, check the tension after 5, 20 and 50 hours of operation and re-tension as required (see the following procedure for measuring belt tension). Thereafter, check and re-tension if required monthly or at 500 hour intervals, whichever comes first.

Ideal drive belt tension is the lowest tension at which the belt will not slip under peak load conditions. Do not over-tension drive belts. Over-tensioning will shorten both drive belt and bearing life. Under-tensioning will cause belt slippage. Always keep belts free from dirt, grease, oil and other foreign material which may cause slippage.

PAGE B - 8 INSTALLATION 49

OPERATION - SECTION C

Review all SAFETY information in Section A.

Follow the instructions on all tags, labels and decals attached to the pump.



This pump is designed to handle liquids containing large entrained solids and slurries. Do not attempt to pump volatile, corrosive, or flammable liquids which may damage the pump or endanger personnel as a result of pump failure.



Pump speed and operating conditions must be within the performance range shown on page E-1.

PRIMING

Install the pump and piping as described in IN-STALLATION. Make sure that the piping connections are tight, and that the pump is securely mounted. Check that the pump is properly lubricated (see LUBRICATION in MAINTENANCE AND REPAIR).

This pump is self-priming, but the pump should never be operated unless there is liquid in the pump casing.



Never operate this pump unless there is liquid in the pump casing. The pump will not prime when dry. extended operation of a dry pump will destroy the seal assembly.

Add liquid to the pump casing when:

- The pump is being put into service for the first time.
- The pump has not been used for a considerable length of time.
- The liquid in the pump casing has evaporated.

Once the pump casing has been filled, the pump will prime and reprime as necessary.



After filling the pump casing, reinstall and tighten the fill plug. Do not attempt to operate the pump unless all connecting piping is securely installed. Otherwise, liquid in the pump forced out under pressure could cause injury to personnel.

To fill the pump, remove the pump casing fill cover or fill plug in the top of the casing, and add clean liquid until the casing is filled. Replace the fill cover or fill plug before operating the pump.

STARTING

Consult the operations manual furnished with the power source.

Rotation

The correct direction of pump rotation is counterclockwise when facing the impeller. The pump could be damaged and performance adversely affected by incorrect rotation. If pump performance is not within the specified limits (see the curve on page E-1), check the direction of power source rotation before further troubleshooting.

If an electric motor is used to drive the pump, remove V-belts, couplings, or otherwise disconnect the pump from the motor before checking motor rotation. Operate the motor independently while observing the direction of the motor shaft, or cooling fan. If rotation is incorrect on a three-phase motor, have a qualified electrician interchange any two of the three phase wires to change direction. If rotation is incorrect on a single-phase motor, consult the literature supplied with the motor for specific instructions.

OPERATION

Lines With a Bypass

If a Gorman-Rupp Automatic Air Release Valve has been installed, the valve will automatically open to allow the pump to prime, and automatically close after priming is complete (see **INSTALLATION** for Air Release Valve operation).

If the bypass line is open, air from the suction line will be discharged through the bypass line back to the wet well during the priming cycle. Liquid will then continue to circulate through the bypass line while the pump is in operation.

Lines Without a Bypass

Open all valves in the discharge line and start the power source. Priming is indicated by a positive reading on the discharge pressure gauge or by a quieter operation. The pump may not prime immediately because the suction line must first fill with liquid. If the pump fails to prime within five minutes, stop it and check the suction line for leaks.

After the pump has been primed, partially close the discharge line throttling valve in order to fill the line slowly and guard against excessive shock pressure which could damage pipe ends, gaskets, sprinkler heads, and any other fixtures connected to the line. When the discharge line is completely filled, adjust the throttling valve to the required flow rate.



Do not operate the pump against a closed discharge throttling valve for long periods of time. If operated against a closed discharge throttling valve,

pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

Leakage

No leakage should be visible at pump mating surfaces, or at pump connections or fittings. Keep all line connections and fittings tight to maintain maximum pump efficiency.

Liquid Temperature And Overheating

The **maximum** liquid temperature for this pump is 160° F (71° C). Do not apply it at a higher operating temperature.

Overheating can occur if operated with the valves in the suction or discharge lines closed. Operating against closed valves could bring the liquid to a boil, build pressure, and cause the pump to rupture or explode. If overheating occurs, stop the pump and allow it to cool before servicing it. Refill the pump casing with cool liquid.



Allow an over-heated pump to cool before servicing. Do not remove plates, covers, gauges, or fittings from an overheated pump. Liquid within the pump can reach boiling temperatures, and vapor pressure within the pump can cause parts being disengaged to be ejected with great force. After the pump cools, drain the liquid from the pump by removing the casing drain plug. Use caution when removing the plug to prevent injury to personnel from hot liquid.

As a safeguard against rupture or explosion due to heat, this pump is equipped with a pressure relief valve which will open if vapor pressure within the pump casing reaches a critical point. If overheating does occur, stop the pump immediately and allow it to cool before servicing it. Approach any overheated pump cautiously. It is recommended that

the pressure relief valve assembly be replaced at each overhaul, or any time the pump casing overheats and activates the valve. **Never** replace this valve with a substitute which has not been specified or provided by the Gorman-Rupp Company.

Strainer Check

If a suction strainer has been shipped with the pump or installed by the user, check the strainer regularly, and clean it as necessary. The strainer should also be checked if pump flow rate begins to drop. If a vacuum suction gauge has been installed, monitor and record the readings regularly to detect strainer blockage.

Never introduce air or steam pressure into the pump casing or piping to remove a blockage. This could result in personal injury or damage to the equipment. If backflushing is absolutely necessary, liquid pressure **must** be limited to 50% of the maximum permissible operating pressure shown on the pump performance curve.

Pump Vacuum Check

With the pump inoperative, install a vacuum gauge in the system, using pipe dope on the threads. Block the suction line and start the pump. At operating speed the pump should pull a vacuum of 20 inches (508,0 mm) or more of mercury. If it does not, check for air leaks in the seal, gasket, or discharge valve.

Open the suction line, and read the vacuum gauge with the pump primed and at operation speed. Shut off the pump. The vacuum gauge reading will immediately drop proportionate to static suction lift, and should then stabilize. If the vacuum reading falls off rapidly after stabilization, an air leak exists. Before checking for the source of the leak, check the point of installation of the vacuum gauge.

STOPPING

Never halt the flow of liquid suddenly. If the liquid being pumped is stopped abruptly, damaging shock waves can be transmitted to the pump and piping system. Close all connecting valves slowly.

On engine driven pumps, reduce the throttle speed slowly and allow the engine to idle briefly before stopping.



If the application involves a high discharge head, gradually close the discharge throttling valve before stopping the pump.

After stopping the pump, lock out or disconnect the power source to ensure that the pump will remain inoperative.



Do not operate the pump against a closed discharge throttling valve for long periods of time. If operated against a closed discharge throttling valve, pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

Cold Weather Preservation

In below freezing conditions, drain the pump to prevent damage from freezing. Also, clean out any solids by flushing with a hose. Operate the pump for approximately one minute; this will remove any remaining liquid that could freeze the pump rotating parts. If the pump will be idle for more than a few hours, or if it has been pumping liquids containing a large amount of solids, drain the pump, and flush it thoroughly with clean water. To prevent large solids from clogging the drain port and preventing the pump from completely draining, insert a rod or stiff wire in the drain port, and agitate the liquid during the draining process. Clean out any remaining solids by flushing with a hose.

BEARING TEMPERATURE CHECK

Bearings normally run at higher than ambient temperatures because of heat generated by friction. Temperatures up to 160°F (71° C) are considered normal for bearings, and they can operate safely to at least 180°F (82° C).

Checking bearing temperatures by hand is inaccurate. Bearing temperatures can be measured accurately by placing a contact-type thermometer against the housing. Record this temperature for future reference.

A sudden increase in bearing temperature is a warning that the bearings are at the point of failing

to operate properly. Make certain that the bearing lubricant is of the proper viscosity and at the correct level (see **LUBRICATION** in **MAINTENANCE AND REPAIR**). Bearing overheating can also be caused by shaft misalignment and/or excessive vibration.

When pumps are first started, the bearings may seem to run at temperatures above normal. Continued operation should bring the temperatures down to normal levels.

TROUBLESHOOTING - SECTION D

Review all SAFETY information in Section A.



Before attempting to open or service the pump:

- 1. Familiarize yourself with this manual.
- Lock out or disconnect the power source to ensure that the pump will remain inoperative.
- Allow the pump to completely cool if overheated.
- Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- 6. Vent the pump slowly and cautiously.
- 7. Drain the pump.

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY
PUMP FAILS TO PRIME	Not enough liquid in casing.	Add liquid to casing. See PRIM-ING.
	Suction check valve contaminated or damaged.	Clean or replace check valve.
	Air leak in suction line.	Correct leak.
	Lining of suction hose collapsed.	Replace suction hose.
	Leaking or worn seal or pump gasket.	Check pump vacuum. Replace leaking or worn seal or gasket.
	Suction lift or discharge head too high.	Check piping installation and install bypass line if needed. See INSTALLATION.
	Strainer clogged.	Check strainer and clean if necessary.
PUMP STOPS OR FAILS TO DELIVER RATED FLOW OR PRESSURE	Air leak in suction line.	Correct leak.
	Lining of suction hose collapsed.	Replace suction hose.
	Leaking or worn seal or pump gasket.	Check pump vacuum. Replace leaking or worn seal or gasket.

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY	
PUMP STOPS OR FAILS TO DELIVER RATED FLOW OR	Strainer clogged.	Check strainer and clean if necessary.	
PRESSURE	Suction intake not submerged at proper level or sump too small.	Check installation and correct sub mergence as needed.	
	Impeller or other wearing parts worn or damaged.	Replace worn or damaged parts. Check that impeller is properly centered and rotates freely.	
	Impeller clogged.	Free impeller of debris.	
	Pump speed too slow.	Check driver output; check belts or couplings for slippage.	
	Discharge head too high.	Install bypass line.	
	Suction lift too high.	Measure lift w/vacuum gauge. Reduce lift and/or friction losses in suction line.	
PUMP REQUIRES TOO MUCH POWER	Pump speed too high.	Check driver output; check that sheaves or couplings are correctly sized.	
	Discharge head too low.	Adjust discharge valve.	
	Liquid solution too thick.	Dilute if possible.	
	Bearing(s) frozen.	Disassemble pump and check bearing(s).	
PUMP CLOGS	Liquid solution too thick.	Dilute if possible.	
FREQUENTLY	Discharge flow too slow.	Open discharge valve fully to increase flow rate, and run power source at maximum governed speed.	
	Suction check valve or foot valve clogged or binding.	Clean valve.	
EXCESSIVE NOISE	Cavitation in pump.	Reduce suction lift and/or friction losses in suction line. Record vacuum and pressure gauge readings and consult local representative or factory.	
	Pumping entrained air.	Locate and eliminate source of air bubble.	
	Pump or drive not securely mounted.	Secure mounting hardware.	
	Impeller clogged or damaged.	Clean out debris; replace damaged parts.	

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY		
BEARINGS RUN TOO HOT	Bearing temperature is high, but within limits.	Check bearing temperature regularly to monitor any increase.		
	Low or incorrect lubricant.	Check for proper type and level of lubricant.		
	Suction and discharge lines not properly supported.	Check piping installation for proper support.		
	Drive misaligned.	Align drive properly.		

PREVENTIVE MAINTENANCE

Since pump applications are seldom identical, and pump wear is directly affected by such things as the abrasive qualities, pressure and temperature of the liquid being pumped, this section is intended only to provide general recommendations and practices for preventive maintenance. Regardless of the application however, following a routine preventive maintenance schedule will help assure trouble-free performance and long life from your Gorman-Rupp pump. For specific questions concerning your application, contact your Gorman-Rupp distributor or the Gorman-Rupp Company.

Record keeping is an essential component of a good preventive maintenance program. Changes in suction and discharge gauge readings (if so equipped) between regularly scheduled inspections can indicate problems that can be corrected before system damage or catastrophic failure occurs. The appearance of wearing parts should also be documented at each inspection for comparison as well. Also, if records indicate that a certain part (such as the seal) fails at approximately the same duty cycle, the part can be checked and replaced before failure occurs, reducing unscheduled down time.

For new applications, a first inspection of wearing parts at 250 hours will give insight into the wear rate for your particular application. Subsequent inspections should be performed at the intervals shown on the chart below. Critical applications should be inspected more frequently.

56

Preventive Maintenance Schedule							
Section 1	Service Interval*						
Item	Daily	Weekly	Monthly	Semi- Annually	Annually		
General Condition (Temperature, Unusual Noises or Vibrations, Cracks, Leaks, Loose Hardware, Etc.) Pump Performance (Gauges, Speed, Flow) Bearing Lubrication Seal Lubrication (And Packing Adjustment, If So Equipped) V-Belts (If So Equipped) Air Release Valve Plunger Rod (If So Equipped) Front Impeller Clearance (Wear Plate) Rear Impeller Clearance (Seal Plate) Check Valve Pressure Relief Valve (If So Equipped) Pump and Driver Alignment Shaft Deflection Bearings Bearing Housing Piping Driver Lubrication — See Mfgr's Literature	I.	i i		C	R R I C I I I I I I I I I I I I I I I I		

Legend:

I = Inspect, Clean, Adjust, Repair or Replace as Necessary

C = Clean

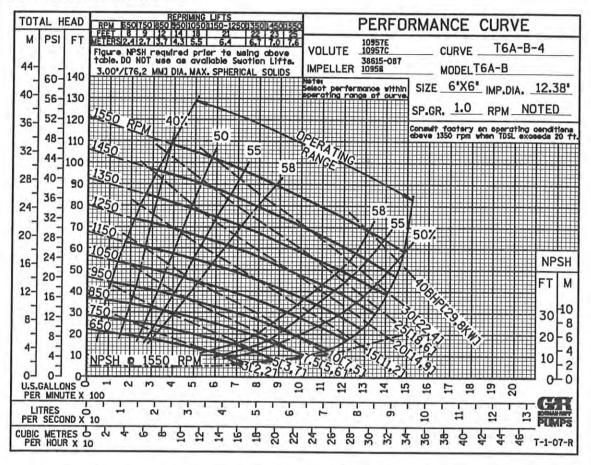
R = Replace

* Service interval based on an intermittent duty cycle equal to approximately 4000 hours annually. Adjust schedule as required for lower or higher duty cycles or extreme operating conditions.

PAGE D - 4 **TROUBLESHOOTING** 57

PUMP MAINTENANCE AND REPAIR - SECTION E

MAINTENANCE AND REPAIR OF THE WEARING PARTS OF THE PUMP WILL MAINTAIN PEAK OPERATING PERFORMANCE.



* STANDARD PERFORMANCE FOR PUMP MODEL T6A3-B, Including /F

*Based on 70° F (21° C) clear water at sea level with minimum suction lift. Since pump installations are seldom identical, your performance may be difference due to such factors as viscosity, specific gravity, elevation, temperature, and impeller trim.

If your pump serial number is followed by an "N", your pump is **NOT** a standard production model.

Contact the Gorman-Rupp Company to verify performance or part numbers.



Pump speed and operating condition points must be within the continuous performance range shown on the curve. OM-01046 T SERIES

SECTION DRAWING

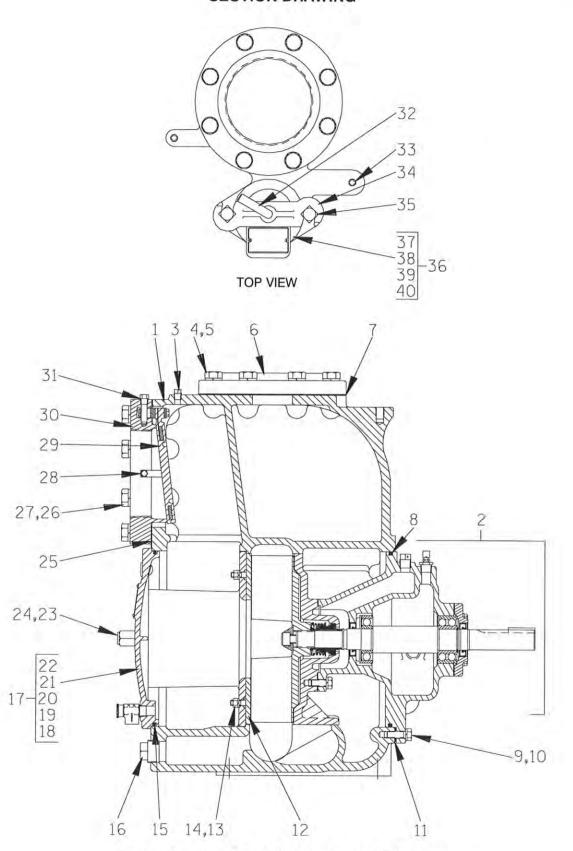


Figure 1. Pump Model T6A3-B, Including /F

PARTS LIST Pump Model T6A3-B, Including /F

(From S/N 740693 Up)

If your pump serial number is followed by an "N", your pump is NOT a standard production model. Contact the Gorman-Rupp Company to verify part numbers.

NO.	PART NAME	PART NUMBER	MAT'L CODE	QTY	NO.	PART NAME	PART NUMBER	MAT'L CODE	QTY
1	PUMP CASING	100570	10010			OUGTION OTIONED			
		10957C	10010	1		SUCTION STICKER	6588AG		1
	REPAIR ROTATING ASSY			1		DISCHARGE STICKER	6588BJ		1
*	REPAIR ROTATING ASSY	44163-243		1		PRIMING STICKER	6588AH		1
10	(WW MODEL ONLY)					WARNING DECAL	2613FE		1
*	REPAIR ROTATING ASSY	44163-202		1	OPTIO	ROTATON DECAL	2613M		1
3	(WWS MODEL ONLY) PIPE PLUG	P04	15070	4		DISASSEMBLY TOOL	48711-020		1
4	HEX HD CAPSCREW	B1208	15079 15991	1			,0,,,		•
5	LOCKWASHER	J12	15991	8		/F FLANGE KIT	48213-041		1
6	DISCHARGE FLANGE	1758	10010	1		-SUCTION	11402A	10010	1
	DISCH FLANGE GSKT					-DISCHARGE	11402B	10010	1
	그는 경기 기가 되었다고 보이지를 그리고 하는 것으로	25113-036		1			100 1000	155	
	ROTATING ASSY O-RING			1		/FM METRIC FLANGE KIT	48213-078		1
9	HEX HD CAPSCREW	B0806	15991	4	1/	-SUCTION	38642-502	10000	1
10	LOCKWASHER	J08	15991	4		-DISCHARGE	38642-503	10000	1
	ROT ASSY SHIM SET	13131	17040	4	1			100000	-
	WEAR PLATE ASSY	46451-723	24150	1	1	WEAR PLATES:			
13	LOCKWASHER	J06	15991	4		-SPA ALLOY	46451-729	24160	1.1
14	HEX NUT	D06	15991	4		-TUNGSTEN CARBIDE	46451-726	2415D	1
15 *	BACK COVER O-RING	S1676		1		-STAINLESS STEEL	46451-723	1718H	1
16	CASING DRAIN PLUG	P20	10009	1					
17	BACK CVR PLATE ASSY	42111-905		1		CASING HEATERS:			
18	-DRIVE SCREW	BM#04-03	17000	4		-120V	47811-004		1
19	-WARNING PLATE	2613EV	13990	1		-240V	47811-005		1
20	-PRESS RELIEF VALVE	26662-005		1					
21	-BACK COVER PLATE	NOT AVAILA		1		CHECK VALVE ASSYS:			
22	-WARNING DECAL	38816-302	-	1		-NEO SOLID TYPE	46411-019		1
23	STUD	C1211	15991	2	V	-VITON SOLID	46411-078		1
24	BACK COVER NUT	31871-073	15000	2	1	-VITON BLOW-OUT	46411-088		1
	GASKET	11402G	19370	1					
26	HEX HD CAPSCREW	B1211	15991	8		PRESS RELIEF VALVES:			
27	LOCKWASHER	J12	15991	8		-SEWAGE TYPE	46431-628		1
28	PIPE PLUG	P04	15079	1		-STAINLESS STEEL	46431-629		1
29 *	SUCT CHK VALVE ASSY	46411-064		1		AND			
30	SUCTION FLANGE	11402	10010	1		HI TEMP SHUT-DOWN K			
31	CHECK VALVE PIN	11645	17010	1		-145°F	48313-186		1
32	CLAMP BAR SCREW	31912-009	15000	1		-130°F	48313-256		1
33	PIPE PLUG	P04	15079	1		-120°F	48313-257		1
34	CLAMP BAR	38111-004	11010	1		HI TEMP SHUT-DOWN	48313-172		1
35	MACHINE BOLT	A1014	15991	2		THERMOSTAT KIT 145°F			
36	FILL COVER ASSY	42111-344		1					
37	-DRIVE SCREW	BM#04-03	17000	2		AIR RELEASE VALVES:			
	-FILL COVER PLATE	NOT AVAILA		1		-10# COMP SPRING	GRP33-07A		1
39	-WARNING PLATE	38816-097	13990	1		-25# COMP SPRING	GRP33-07		1
	-GASKET	50G	19210	1		-80# COMP SPRING	GRP33-07B		1
OT SH	IOWN:			. II		A/R VALVE MTG KIT	46331-515		1
	NAME PLATE	38818-040	13990	1					
	DRIVE SCREW	BM#04-03	17000	4		ROTATING ASSY AND BA	CK COVER O-	RING	
	LUBE DECAL	11421		1	1	-VITON	25154-454		1

^{*} INDICATES PARTS RECOMMENDED FOR STOCK

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OM-01046 T SERIES

SECTION DRAWING

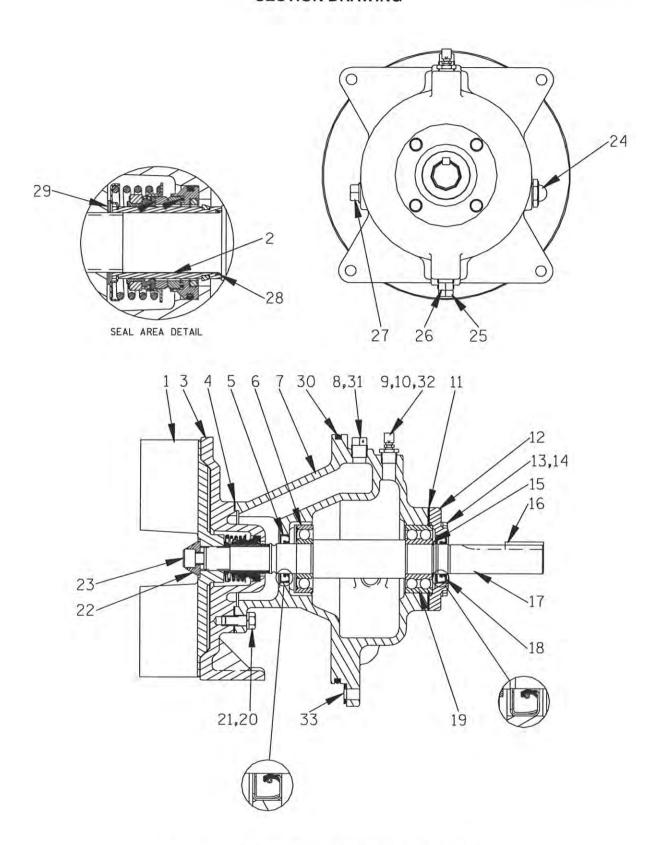


Figure 2. 10956F Repair Rotating Assembly

PARTS LIST 10956F Repair Rotating Assembly

NO.	I PART NAME	PART NUMBER	MAT'L CODE	QTY	ITEM NO.	PART NAME	PART NUMBER	MAT'L CODE	QTY
1 *	MPELLER	10958	11010	1		INSTRUCTION TAG	6588U	>	1
2 *	SEAL ASSEMBLY	46513-150		1					
3	SEAL PLATE	11837E	10010	1	OPTIO	NAL:			
4 *	SEAL PLATE GASKET	10959G	20000	1		IMP CLEAN-OUT KIT	48783-003		1
5 *	BEARING CAP OIL SEAL	S1352		1					
6 *	INBOARD BALL BEARING	23276-009		1		STAINLESS STEEL PARTS			
7	BEARING HOUSING	10959B	10010	1		IMP SHAFT LESS SLEEVE	10529B	1706H	1
8	VENTED PLUG	4823A	15079	1		SPACER WASHER			
9	AIR VENT	S1530		1		(FOR SST SHAFT)	38329-040	17130	1
10	RED PIPE BUSHING	AP0802	15079	1		SEAL ASSY	112364D		1
11 *	*BEARING CAP GASKET	38683-248	18000	1					
12	BEARING CAP	38322-215	10010	1		IMPELLERS:			
13	HEX HD CAPSCREW	B0605	15991	4		-ADI	10958	1102H	1
14	LOCKWASHER	J06	15991	4		-TUNG CARB COATED	10958A	11000	1
15	BRG RETAINING RING	S244		1		Zalir No Caral			
16 *	SHAFT KEY	N0612	15990	1		SEAL PLATES:			
17 *	IMPELLER SHAFT	10529	16040	1		-(TUNG CARB COATED)	11837F	10010	1
18 *	INBOARD OIL SEAL	S1352		1		-ADI	11837E	1102H	1
19 *	OUTBRD BALL BEARING	S1040		1	0.4	0541 40054545			
20	HEX HD CAPSCREW	B0805 1/2	15991	4		SEAL ASSEMBLIES	522202		
21	LOCKWASHER	J08	15991	4	Ţ	-STD MECHANICAL	12364A		1
22	IMPELLER WASHER	10278	15030	1	T	-PERMALON COATED	46512-150		1
23	SOCKET HD CAPSCREW	DM1004S	15991	1	-	METAL DELLOWS MESSUS	CAL ADOM		
24	SIGHT GAUGE	S1471		1		METAL BELLOWS MECH S			0.
25	SEAL CAV DRAIN PLUG	P08	15079	1		SEAL PLATE	38272-242	10010	1
26	BRG HSG DRAIN PLUG	P08	15079	1		SEAL SLEEVE ASTL	11876B	16000	1
27	PIPE PLUG	P12	15079	1	1.2	SPACER WASHER	38329-040	17130	1
28 *	O-RING	25154-022		REF		-(VITON OR EQUAL)	46512-147		1
29 *	IMPELLER ADJ SHIM SET	37J	17090	REF	-	-(KALREZ)	46512-142		1
	ROTATING ASSY O-RING			1	+	MECHANICAL SEAL			
31	SHIPPING PLUG	11495B	15079	1		SHAFT SLEEVE	110704	10000	
32	SHIPPING PLUG	11495B	15079	1	+ +	AFLAS SEAL (W/SST SLEE	11876A	16000	1
33 *	ROT ASSY ADJ SHIM SET		17040	4		[1] 보고 : # 12 House Hou	46512-194		1
IOT SI	HOWN:					ROTATING ASSEMBLY ANI	D BACK COVE	ER O-RINI	GS:
	ROTATION DECAL	2613M		1		-VITON			1

^{*} INDICATES PARTS RECOMMENDED FOR STOCK

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^{***} FOR PUMPS WITH SERIAL NUMBERS **BELOW** 864836, ORDER 10530G/18000 BEARING CAP GASKET. IF **BOTH** BEARING CAP AND GASKET MUST BE REPLACED, ORDER PARTS LISTED ABOVE.

[†] OPTIONAL MECHANICAL SEAL(S) MUST BE USED WITH MECHANICAL SEAL SHAFT SLEEVE OR SOLID SST SHAFT.

OM-01046 T SERIES

PUMP AND SEAL DISASSEMBLY AND REASSEMBLY

Review all SAFETY information in Section A.

Follow the instructions on all tags, label and decals attached to the pump.

This pump requires little service due to its rugged, minimum-maintenance design. However, if it becomes necessary to inspect or replace the wearing parts, follow these instructions which are keyed to the sectional views (see Figures 1 and 2) and the accompanying parts lists.

As described on the following pages, this manual will alert personnel to known procedures which require special attention, to those which could damage equipment, and to those which could be dangerous to personnel. However, this manual cannot possibly anticipate and provide detailed precautions for every situation that might occur during maintenance of the unit. Therefore, it is the responsibility of the owner/maintenance personnel to ensure that only safe, established maintenance procedures are used, and that any procedures not addressed in this manual are performed only after establishing that neither personal safety nor pump integrity are compromised by such practices.

Many service functions may be performed by draining the pump and removing the back cover assembly. If major repair is required, the piping and/or power source must be disconnected. The following instructions assume complete disassembly is required.

Before attempting to service the pump, disconnect or lock out the power source and take precautions to ensure that it will remain inoperative. Close all valves in the suction and discharge lines.

For power source disassembly and repair, consult the literature supplied with the power source, or contact your local power source representative.



Before attempting to open or service the pump:

 Familiarize yourself with this manual.

- Disconnect or lock out the power source to ensure that the pump will remain inoperative.
- Allow the pump to completely cool if overheated.
- Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- Vent the pump slowly and cautiously.
- 7. Drain the pump.



Use lifting and moving equipment in good repair and with adequate capacity to prevent injuries to personnel or damage to equipment.

Back Cover And Wear Plate Removal

(Figure 1)

The wear plate (12) is easily accessible and may be serviced by removing the back cover assembly (17). Before attempting to service the pump, remove the pump casing drain plug (16) and drain the pump. Clean and reinstall the drain plug.

Remove the back cover nuts (24) and pull the back cover and assembled wear plate from the pump casing (1). Inspect the wear plate, and replace it if badly scored or worn. To remove the wear plate, disengage the hardware (13 and 14).

Inspect the back cover O-ring (15) and replace it if damaged or worn.

Suction Check Valve Removal

(Figure 1)

If the check valve assembly (29) is to be serviced, remove the check valve pin (31), reach through the back cover opening and pull the complete assembly from the suction flange (30).

NOTE

Further disassembly of the check valve is not required since it must be replaced as a complete unit. Individual parts are not sold separately.

Rotating Assembly Removal

(Figure 2)

The rotating assembly may be serviced without disconnecting the suction or discharge piping; however, the power source must be removed to provide clearance.

The impeller (1) should be loosened while the rotating assembly is still secured to the pump casing. Before loosening the impeller, remove the seal cavity drain plug (25) and drain the seal lubricant. This will prevent the oil in the seal cavity from escaping when the impeller is loosened. Clean and reinstall the seal cavity drain plug.

Immobilize the impeller by wedging a block wood between the vanes and the pump casing, and remove the impeller capscrew and washer (22 and 23).

Install a lathe dog on the drive end of the shaft (17) with the "V" notch positioned over the shaft keyway.

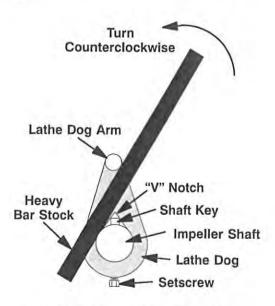


Figure 3. Loosening Impeller

With the impeller rotation still blocked, see Figure 3 and use a long piece of heavy bar stock to pry against the arm of the lathe dog in a counterclockwise direction (when facing the drive end of the shaft). **Use caution** not to damage the shaft or key-

way. When the impeller breaks loose, remove the lathe dog and wood block.

NOTE

Do not remove the impeller until the rotating assembly has been removed from the pump casing.

(Figure 1)

Remove the hardware (9 and 10) securing the rotating assembly to the pump casing. Separate the rotating assembly by pulling straight away from the pump casing.

NOTE

An optional disassembly tool is available from the factory. If the tool is used, follow the instructions packed with it. A similar tool may be assembled using 1/2-inch pipe (schedule 80 steel or malleable iron) and a standard tee (see Figure 4). All threads are 1/2-inch NPT. Do not pre-assemble the tool.

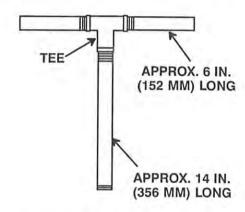


Figure 4. Rotating Assembly Tool

To install the tool, remove the air vent (9, Figure 2) from the bearing housing, and screw the longest length of pipe into the vent hole until fully engaged. Install the tee, and screw the handles into the tee. Use caution when lifting the rotating assembly to avoid injury to personnel or damage to the assembly.

Remove the bearing housing O-ring (8).

Impeller Removal

(Figure 2)

With the rotating assembly removed from the pump casing, unscrew the impeller from the shaft.

OM-01046 T SERIES

Use caution when unscrewing the impeller; tension on the shaft seal spring will be released as the impeller is removed. Inspect the impeller and replace if cracked or badly worn.

Remove the impeller adjusting shims (29); tie and tag the shims, or measure and record their thickness for ease of reassembly.

Seal Removal

(Figure 2)

Slide the integral shaft sleeve and rotating portion of the seal off the shaft as a unit.

Use a pair of stiff wires with hooked ends to remove the stationary element and seat.

An alternate method of removing the stationary seal components is to remove the hardware (20 and 21) and separate the seal plate (3) and gasket (4) from the bearing housing (7). Position the seal plate on a flat surface with the impeller side down. Use a wooden dowel or other suitable tool to press on the back side of the stationary seat until the seat, O-rings, and stationary element can be removed.

Remove the shaft sleeve O-ring (28).

If no further disassembly is required, refer to **Seal Installation**.

Shaft and Bearing Removal and Disassembly (Figure 2)

When the pump is properly operated and maintained, the bearing housing should not require disassembly. Disassemble the shaft and bearings only when there is evidence of wear or damage.



Shaft and bearing disassembly in the field is not recommended. These operations should be performed only in a properlyequipped shop by qualified personnel.

Remove the bearing housing drain plug (26) and drain the lubricant. Clean and reinstall the drain plug.

Disengage the hardware (13 and 14) and slide the bearing cap (12) and oil seal (18) off the shaft.Remove the bearing cap gasket (11), and press the oil seal from the bearing cap.

Place a block of wood against the impeller end of the shaft and tap the shaft and assembled bearings (6 and 19) from the bearing housing.

After removing the shaft and bearings, clean and inspect the bearings in place as follows.



To prevent damage during removal from the shaft, it is recommended that bearings be cleaned and inspected **in place**. It is **strongly** recommended that the bearings be replaced **any** time the shaft and bearings are removed.

Clean the bearing housing, shaft and all component parts (except the bearings) with a soft cloth soaked in cleaning solvent. Inspect the parts for wear or damage and replace as necessary.



Most cleaning solvents are toxic and flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Clean the bearings thoroughly in **fresh** cleaning solvent. Dry the bearings with filtered compressed air and coat with light oil.



Bearings must be kept free of all dirt and foreign material. Failure to do so will greatly shorten bearing life. **DO NOT** spin dry bearings. This may scratch the balls or races and cause premature bearing failure.

Rotate the bearings by hand to check for roughness or binding and inspect the bearing balls. If ro-

tation is rough or the bearing balls are discolored, replace the bearings.

The bearing tolerances provide a tight press fit onto the shaft and a snug slip fit into the bearing housing. Replace the bearings, shaft, or bearing housing if the proper bearing fit is not achieved.

If bearing replacement is required, remove the outboard bearing retaining ring (15), and use a bearing puller to remove the bearings from the shaft.

Press the inboard oil seal (5) from the bearing housing.

Shaft and Bearing Reassembly and Installation (Figure 2)

Clean the bearing housing, shaft and all component parts (except the bearings) with a soft cloth soaked in cleaning solvent. Inspect the parts for wear or damage as necessary.



Most cleaning solvents are toxic and flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Inspect the shaft for distortion, nicks or scratches, or for thread damage on the impeller end. Dress small nicks and burrs with a fine file or emery cloth. Replace the shaft if defective.

Position the inboard oil seal (5) in the bearing housing bore with the lip positioned as shown in Figure 2. Press the oil seal into the housing until the face is **just flush** with the machined surface on the housing.



To prevent damage during removal from the shaft, it is recommended that bearings be cleaned and inspected **in place**. It is **strongly** recommended that the bearings be replaced **any** time the shaft and bearings are removed.

NOTE

Position the inboard bearing (6) on the shaft with the shielded side toward the impeller end of the shaft. Position the outboard bearing (19) on the shaft with the integral retaining ring on the bearing O.D. toward the drive end of the shaft.

The bearings may be heated to ease installation. An induction heater, hot oil bath, electric oven, or hot plate may be used to heat the bearings. Bearings should **never** be heated with a direct flame or directly on a hot plate.

NOTE

If a hot oil bath is used to heat the bearings, both the oil and the container must be **absolutely** clean. If the oil has been previously used, it must be **thoroughly** filtered.

Heat the bearings to a uniform temperature **no higher than** 250°F (120°C), and slide the bearings onto the shaft, one at a time, until they are fully seated. This should be done quickly, in one continuous motion, to prevent the bearings from cooling and sticking on the shaft.

After the bearings have been installed and allowed to cool, check to ensure that they have not moved away from the shaft shoulders in shrinking. If movement has occurred, use a suitable sized sleeve and a press to reposition the bearings against the shaft shoulders.

If heating the bearings is not practical, use a suitable sized sleeve, and an arbor (or hydraulic) press to install the bearings on the shaft.



When installing the bearings onto the shaft, **never** press or hit against the outer race, balls, or ball cage. Press **only** on the inner race.

Secure the outboard bearing on the shaft with the bearing retaining ring (15).

Slide the shaft and assembled bearings into the bearing housing until the retaining ring on the outboard bearing seats against the bearing housing.



When installing the shaft and bearings into the bearing bore, push against the outer race. **Never** hit the balls or ball cage.

Press the outboard oil seal (18) into the bearing cap (12) with the lip positioned as shown in Figure 2. Replace the bearing cap gasket (11), and secure the bearing cap with the hardware (13 and 14). **Be careful** not to damage the oil seal lip on the shaft keyway.

Install the bearing housing O-ring (30).

Lubricate the bearing housing as indicated in **LU-BRICATION**.

Seal Installation

(Figures 2, 5, 6 and 7)



Most cleaning solvents are toxic and

flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Clean the seal cavity and shaft with a cloth soaked in fresh cleaning solvent. Inspect the stationary seat bore in the seal plate for dirt, nicks and burrs, and remove any that exist. The stationary seat bore **must** be completely clean before installing the seal.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

To ease installation of the seal, lubricate the shaft sleeve O-ring and the external stationary seat O-ring with a very **small** amount of light lubricating oil. See Figure 5 for seal part identification.

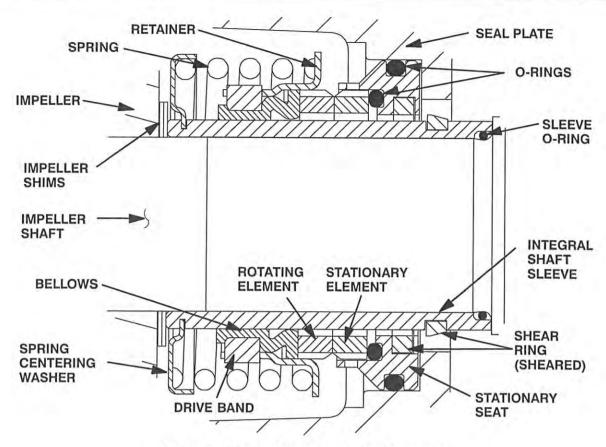


Figure 5. 46513-150 Cartridge Seal Assembly



This seal is not designed for operation at temperatures above 160°F (71°C). Do not use at higher operating temperatures.

If the seal plate was removed, install the seal plate gasket (4). Position the seal plate over the shaft and secure it to the intermediate with the hardware (20 and 21).

To prevent damaging the shaft sleeve O-ring (28) on the shaft threads, stretch the O-ring over a piece of tubing 1-1/4 I.D. x 1-1/2 O.D. x 2-inches long (32 mm x 38 mm x 51 mm). Slide the tube over the shaft threads, then slide the O-ring off the tube and onto the shaft. Remove the tube, and continue to slide the O-ring down the shaft until it seats against the shaft shoulder.

When installing a new cartridge seal assembly, remove the seal from the container, and remove the mylar storage tabs, if so equipped, from between the seal faces.



New cartridge seal assemblies may be equipped with mylar storage tabs between the seal faces. If so equipped, these storage tabs **must** be removed before installing the seal.

Lubricate the external stationary seat O-ring with light oil. Slide the seal assembly onto the shaft until the external stationary seat O-ring engages the bore in the seal plate.

Clean and inspect the impeller as described in Impeller Installation and Adjustment. Install the full set of impeller shims (29) provided with the seal, and screw the impeller onto the shaft until it is seated against the seal (see Figure 6).

Continue to screw the impeller onto the shaft. This will press the stationary seat into the seal plate bore.

OM-01046 T SERIES

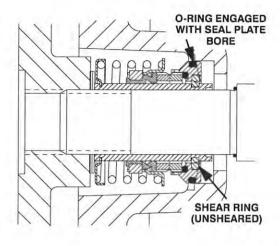


Figure 6. Seal Partially Installed

NOTE

A firm resistance will be felt as the impeller presses the stationary seat into the seal plate bore.

As the stationary seat becomes fully seated, the seal spring compresses, and the shaft sleeve will break the nylon shear ring. This allows the sleeve to slide down the shaft until seated against the shaft shoulder. Continue to screw the impeller onto the shaft until the impeller, shims, and sleeve are fully seated against the shaft shoulder (see Figure 7).

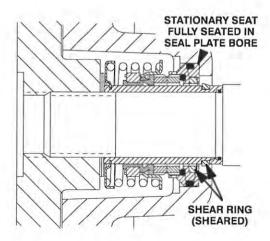


Figure 7. Seal Fully Installed

Measure the impeller-to-seal plate clearance, and remove impeller adjusting shims to obtain the proper clearance as described in **Impeller Installation and Adjustment**.

If necessary to reuse an old seal in an emergency, carefully separate the rotating and stationary seal faces from the bellows retainer and stationary seat.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

Handle the seal parts with extreme care to prevent damage. Be careful not to contaminate precision finished faces; even fingerprints on the faces can shorten seal life. If necessary, clean the faces with a non-oil based solvent and a clean, lint-free tissue. Wipe **lightly** in a concentric pattern to avoid scratching the faces.

Carefully wash all metallic parts in fresh cleaning solvent and allow to dry thoroughly.



Do not attempt to separate the rotating portion of the seal from the shaft sleeve when reusing an old seal. The rubber bellows will adhere to the sleeve during use, and attempting to separate them could damage the bellows.

Inspect the seal components for wear, scoring, grooves, and other damage that might cause leakage. Inspect the integral shaft sleeve for nicks or cuts on either end. If any components are worn, or the sleeve is damaged, replace the complete seal; never mix old and new seal parts.

Install the stationary seal element in the stationary seat. Press this stationary subassembly into the seal plate bore until it seats squarely against the bore shoulder. A push tube made from a piece of plastic pipe would aid this installation. The I.D. of

the pipe should be slightly larger than the O.D. of the shaft sleeve.

Slide the rotating portion of the seal (consisting of the integral shaft sleeve, spring centering washer, spring, bellows and retainer, and rotating element) onto the shaft until the seal faces contact.

Proceed with Impeller Installation and Adjustment.

Impeller Installation

(Figure 2)

Inspect the impeller, and replace it if cracked or badly worn. Inspect the impeller and shaft threads for dirt or damage, and clean or dress the threads as required.



The shaft and impeller threads **must** be completely clean before reinstalling the impeller. Even the slightest amount of dirt on the threads can cause the impeller to seize to the shaft, making future removal difficult or impossible without damage to the impeller or shaft.

Install the same thickness of impeller adjusting shims (29) as previously removed. Apply 'Never-Seez' or equivalent to the shaft threads and screw the impeller onto the shaft until tight.

NOTE

At the slightest sign of binding, immediately back the impeller off, and check the threads for dirt. **Do not** try to force the impeller onto the shaft.

A clearance of .025 to .040 inch (0,64 to 1,02 mm) between the impeller and the seal plate is recommended for maximum pump efficiency. Measure this clearance, and add or remove impeller adjusting shims as required.

NOTE

If the rotating assembly has been installed in the pump casing, this clearance may be measured by reaching through the priming port with a feeler gauge.

NOTE

Proceed with Rotating Assembly Installation before installing the impeller capscrew and washer (22 and 23). The rotating assembly must be installed in the pump casing in order to torque the impeller capscrew.

After the rotating assembly is installed in the pump casing, coat the threads of the impeller capscrew (23) with 'Never-Seez' or equivalent compound, and install the impeller washer (22) and capscrew; torque the capscrew to 90 ft. lbs. (1080 in. lbs. or 12,4 m. kg.).

Rotating Assembly Installation

(Figure 1)

NOTE

If the pump has been completely disassembled, it is recommended that the suction check valve and back cover assembly be reinstalled at this point. The back cover assembly must be in place to adjust the impeller face clearance.

Install the bearing housing and lubricate it with light grease. Ease the rotating assembly into the pump casing using the installation tool. **Be careful** not to damage the O-ring.

Install the four sets of rotating assembly adjusting shims (11) using the same thickness as previously removed. Secure the rotating assembly to the pump casing with the hardware (9 and 10). **Do not** fully tighten the capscrews until the back cover has been reinstalled and the impeller face clearance has been set.

A clearance of .010 to .020 inch (0,25 to 0,51 mm) between the impeller and the wear plate is also recommended for maximum pump efficiency. This clearance can be obtained by removing an equal amount of shims from each rotating assembly shim set until the impeller scrapes against the wear plate when the shaft is turned. After the impeller scrapes, add approximately .015 inch (0,4 mm) of shims to each shim set.

NOTE

An alternate method of adjusting this clearance is to

APPENDIX K

OM-01046 T SERIES

reach through the suction port with a feeler gauge and measure the gap. Add or subtract rotating assembly shims accordingly.

Suction Check Valve Installation

(Figure 1)

Inspect the check valve assembly (29), and replace it if badly worn.

NOTE

The check valve assembly must be replaced as a complete unit. Individual parts are not sold separately.

Reach through the back cover opening with the check valve (29), and position the check valve adaptor in the mounting slot in the suction flange (30). Align the adaptor with the flange hole, and secure the assembly with the check valve pin (31).

NOTE

If the suction or discharge flanges were removed, replace the respective gaskets, apply 'Permatex Aviation No. 3 Form-A-Gasket' or equivalent compound to the mating surfaces, and secure them to the pump casing with the attaching hardware.

Back Cover Installation

(Figure 1)

If the wear plate (12) was removed for replacement, carefully center it on the back cover and secure it with the hardware (13 and 14). The wear plate **must** be concentric to prevent binding when the back cover is installed.

Replace the back cover O-ring (15), and lubricate it with a generous amount of No. 2 grease. Clean any scale or debris from the contacting surfaces in the pump casing that might interfere or prevent a good seal with the back cover. Slide the back cover assembly into the pump casing. Be sure the wear plate does not bind against the impeller.

NOTE

To ease future disassembly, apply a film of grease or 'Never-Seez' on the back cover shoulder, or any

surface which contacts the pump casing. This action will reduce rust and scale build-up.

Secure the back cover assembly by tightening the back cover nuts (24) evenly. **Do not** over-tighten the hand nuts; they should be just tight enough to ensure a good seal at the back cover shoulder. Be sure the wear plate does not bind against the casing.

PRESSURE RELIEF VALVE MAINTENANCE

(Figure 1)

The back cover is equipped with a pressure relief valve (20) to provide additional safety for the pump and operator (refer to **Liquid Temperature And Overheating** in **OPERATION**).

It is recommended that the pressure relief valve assembly be replaced at each overhaul, or any time the pump overheats and activates the valve. **Never** replace this valve with a substitute which has not been specified or provided by the Gorman-Rupp Company.

Periodically, the valve should be removed for inspection and cleaning. When reinstalling the relief valve, apply 'Loctite Pipe Sealant With Teflon No. 592', or equivalent compound, on the relief valve threads. Position the valve as shown in Figure 1 with the discharge port pointing down.

Final Pump Assembly

(Figure 1)

71

Install the shaft key (16, Figure 2) and reconnect the power source. Be sure to install any guards used over the rotating members.



Do not operate the pump without the guards in place over the rotating parts. Exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

Install the suction and discharge lines and open all valves. Make certain that all piping connections are tight, properly supported and secure.

Be sure the pump and power source have been properly lubricated, see LUBRICATION.

Remove the fill cover assembly (36) and fill the pump casing with clean liquid. Reinstall the fill cover and tighten it. Refer to **OPERATION**, Section C, before putting the pump back into service.

LUBRICATION

Seal Assembly

(Figure 2)

Before starting the pump, remove the vented plug (8) and fill the seal cavity with approximately 40 ounces (1,4 liters) of SAE No. 30 non-detergent oil, or to a level just below the tapped vented plug hole. Clean and reinstall the vented plug. Maintain the oil at this level.

Bearings

(Figure 2)

The bearing housing was fully lubricated when shipped from the factory. Check the oil level regularly through the sight gauge (24) and maintain it at the middle of the gauge. When lubrication is required, add SAE No. 30 non-detergent oil through the hole for the air vent (9). **Do not** over-lubricate.

Over-lubrication can cause the bearings to overheat, resulting in premature bearing failure.

NOTE

The white reflector in the sight gauge must be positioned horizontally to provide proper drainage.

Under normal conditions, drain the bearing housing once each year and refill with approximately 32 ounces (1 liter) clean oil. Change the oil more frequently if the pump is operated continuously or installed in an environment with rapid temperature change.



Monitor the condition of the bearing lubricant regularly for evidence of rust or moisture condensation. This is especially important in areas where variable hot and cold temperatures are common.

For cold weather operation, consult the factory or a lubricant supplier for the recommended grade of oil.

Power Source

Consult the literature supplied with the power source, or contact your local power source representative.

THE GORMAN-RUPP COMPANY AND GORMAN-RUPP OF CANADA LIMITED 12 MONTH LIMITED WARRANTY

EXTENT AND DURATION OF WARRANTY

Coverage: The Gorman-Rupp Company or Gorman-Rupp of Canada Limited (herein individually referred to as "GR") each individually warrant that its products and parts shall be free from defects in material and workmanship for twelve (12) months from the date of purchase by the original end user.

Exceptions: This Limited Warranty shall not apply to the following products and parts: engines, motors, trade accessories and other products, components or materials not manufactured by GR. With respect to submersible pumps, the pump and motor are an integral unit and are therefore warranted as a unit. However, with respect to the electrical components in submersible pumps, this warranty is valid **only** when electrical controls for the pump have been specified and/or provided by GR. Wear and tear on any product resulting from normal use is not covered by this Limited Warranty.

LIMITATIONS

GR'S SOLE AND EXCLUSIVE WARRANTY WITH RESPECT TO ITS PRODUCTS AND PARTS IS THIS LIMITED WARRANTY. THIS LIMITED WARRANTY IS IN LIEU OF ALL OTHER EXPRESS AND/OR IMPLIED WARRANTIES, INCLUDING IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR PARTICULAR PURPOSE.

EXCLUSIVE REMEDY AND DAMAGES

The sole and exclusive remedy for breach of this Limited Warranty by GR, and the entire extent of its liability for such breach or for damages arising and/or resulting from the use of the products and parts covered by this Limited Warranty shall be as follows:

1. Repair or replacement: If inspection shows that any GR product or part covered under this LimitedWarranty is defective in materials or workmanship, GR shall repair or replace the defective product or part at its option, without charge. You must have properly installed, maintained and used the product or part claimed to be defective in accordance with the maintenance schedule and/or manual which comes with the product. No allowance will be made for labor, transportation or other charges incurred by you in connection with such repair or replacement.

2. To obtain the above remedy:

- a) Immediately notify GR at the address below of the claimed defect in materials or workmanship and provide the serial number or date code of the product and/or part and provide a copy of the invoice or bill of sale referencing the product and/or part by no later than the expiration date of the Limited Warranty period.
- b) GR will advise whether inspection of the product and/or part will be necessary and whether and how repair or replacement will be effected. If inspection by GR is necessary, the product or part must be sent freight prepaid to GR at the address stated below. Return shipment of the repaired product or part will be F.O.B. the address stated below.
- 3. Damages: GR's liability for damages for breach of this Limited Warranty shall not exceed the amount of the purchase price of the product or part in respect to which damages are claimed. IN NO EVENT SHALL GR BE LIABLE FOR INCIDENTAL, CONSEQUENTIAL OR SPECIAL DAMAGES FOR BREACH OF THIS LIMITED WARRANTY OTHER THAN AS STATED HEREIN.

Some states do not allow the exclusion or limitation of incidental or consequential damages. Accordingly, the above may not apply to you. This Limited Warranty gives you specific legal rights, and you may also have other rights which vary from state to state and province to province.

THE GORMAN-RUPP COMPANY P.O. BOX 1217 MANSFIELD, OH 44901-1217 Phone: (419) 755-1011 GORMAN-RUPP OF CANADA LIMITED 70 Burwell Road St. Thomas, Ontario N5P 3R7 Phone: (519) 631–2870



INSTALLATION, OPERATION, AND MAINTENANCE MANUAL

WITH PARTS LIST



T SERIES PUMPS

MODELS

T6A60-B

INCLUDING: /F, /FM

THE GORMAN-RUPP COMPANY . MANSFIELD, OHIO

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TABLE OF CONTENTS

INTRODUCTION	PAGE I – 1
SAFETY - SECTION A	PAGE A - 1
INSTALLATION – SECTION B	PAGE B - 1
Pump Dimensions	PAGE B - 1
PREINSTALLATION INSPECTION	PAGE B - 2
POSITIONING PUMP	PAGE B - 2
Lifting	PAGE B - 2
Mounting	
Clearance	PAGE B - 2
SUCTION AND DISCHARGE PIPING	PAGE B - 2
Materials	PAGE B - 2
Line Configuration	PAGE B - 3
Connections to Pump	PAGE B - 3
Gauges	PAGE B - 3
SUCTION LINES	PAGE B - 3
Fittings	PAGE B - 3
Strainers	PAGE B - 3
Sealing	PAGE B - 3
Suction Lines In Sumps	PAGE B - 3
Suction Line Positioning	PAGE B - 4
DISCHARGE LINES	PAGE B - 4
Siphoning	PAGE B - 4
Valves	PAGE B - 4
Bypass Lines	PAGE B - 5
AUTOMATIC AIR RELEASE VALVE	PAGE B - 6
Theory of Operation	PAGE B - 6
Air Release Valve Installation	PAGE B - 6
ALIGNMENT	PAGE B - 7
Coupled Drives	PAGE B - 8
V-Belt Drives	PAGE B - 8
OPERATION - SECTION C	PAGE C - 1
PRIMING	PAGE C - 1
STARTING	PAGE C - 1
Rotation	PAGE C - 1
OPERATION	PAGE C - 2
Lines With a Bypass	PAGE C - 2
Lines Without a Bypass	PAGE C - 2
Leakage	PAGE C – 2
Liquid Temperature And Overheating	PAGE C - 2
Strainer Check	PAGE C = 2
Pump Vacuum Check	PAGE C = 3
STOPPING	PAGE C = 3
Cold Weather Preservation	PAGE C - 3
BEARING TEMPERATURE CHECK	PAGE C = 3

7¹7 APPENDIX K

TABLE OF CONTENTS (continued)

TI	ROUBLESHOOTING — SECTION D	PAGE D - 1
	PREVENTIVE MAINTENANCE SCHEDULE	PAGE D - 3
PI	UMP MAINTENANCE AND REPAIR - SECTION E	PAGE E - 1
	PERFORMANCE CURVE	PAGE E - 1
	Pump Model	PAGE E - 3
	Repair Rotating Assembly	PAGE E - 5
	PUMP AND SEAL DISASSEMBLY AND REASSEMBLY	PAGE E - 6
	Back Cover And Wear Plate Removal	PAGE E - 6
	Suction Check Valve Removal	PAGE E - 6
	Rotating Assembly Removal	PAGE E - 7
	Impeller Removal	PAGE E - 7
	Seal Removal	PAGE E - 8
	Shaft and Bearing Removal and Disassembly	PAGE E - 8
	Shaft and Bearing Reassembly and Installation	PAGE E - 9
	Seal Installation	PAGE E - 10
	Impeller Installation	PAGE E - 13
	Rotating Assembly Installation	PAGE E - 13
	Suction Check Valve Installation	PAGE E - 14
	Back Cover Installation	PAGE E - 14
	PRESSURE RELIEF VALVE MAINTENANCE	PAGE E - 14
	Final Pump Assembly	PAGE E - 14
	LUBRICATION	PAGE E - 15
	Seal Assembly	PAGE E - 15
	Bearings	PAGE E - 15
	Power Source	PAGE E - 15

T SERIES OM-01929

INTRODUCTION

Thank You for purchasing a Gorman-Rupp pump. Read this manual carefully to learn how to safely install and operate your pump. Failure to do so could result in personal injury or damage to the pump. This Installation, Operation, and Maintenance manual is designed to help you achieve the best performance and longest life from your Gorman-Rupp pump.

This pump is a T Series, semi-open impeller, self-priming centrifugal model with a suction check valve. The pump is designed for handling liquids containing large entrained solids and slurries. The basic material of construction is gray iron, with ductile iron impeller and steel wearing parts.

Because pump installations are seldom identical, this manual cannot possibly provide detailed instructions and precautions for every aspect of each specific application. Therefore, it is the responsibility of the owner/installer of the pump to ensure that applications not addressed in this manual are performed **only** after establishing that neither operator safety nor pump integrity are compromised by the installation. Pumps and related equipment **must** be installed and operated according to all national, local and industry standards.

If there are any questions regarding the pump or its application which are not covered in this manual or in other literature accompanying this unit, please contact your Gorman-Rupp distributor, or:

> The Gorman-Rupp Company P.O. Box 1217 Mansfield, Ohio 44901–1217 Phone: (419) 755–1011

Gorman-Rupp of Canada Limited 70 Burwell Road St. Thomas, Ontario N5P 3R7 Phone: (519) 631–2870

For information or technical assistance on the power source, contact the power source manufacturer's local dealer or representative.

The following are used to alert maintenance personnel to procedures which require special attention, to those which could damage equipment, and to those which could be dangerous to personnel:



Immediate hazards which WILL result in severe personal injury or death. These instructions describe the procedure required and the injury which will result from failure to follow the procedure.



Hazards or unsafe practices which COULD result in severe personal injury or death. These instructions describe the procedure required and the injury which could result from failure to follow the procedure.



Hazards or unsafe practices which COULD result in minor personal injury or product or property damage. These instructions describe the requirements and the possible damage which could result from failure to follow the procedure.

NOTE

Instructions to aid in installation, operation, and maintenance or which clarify a procedure.

INTRODUCTION PAGE I – 1

79 APPENDIX K

SAFETY - SECTION A

This information applies to T Series basic pumps. Gorman-Rupp has no control over or particular knowledge of the power source which will be used. Refer to the manual accompanying the power source before attempting to begin operation.

Because pump installations are seldom identical, this manual cannot possibly provide detailed instructions and precautions for each specific application. Therefore, it is the owner/installer's responsibility to ensure that applications not addressed in this manual are performed only after establishing that neither operator safety nor pump integrity are compromised by the installation.



Before attempting to open or service the pump:

- Familiarize yourself with this manual.
- Disconnect or lock out the power source to ensure that the pump will remain inoperative.
- 3. Allow the pump to completely cool if overheated.
- Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- Vent the pump slowly and cautiously.
- 7. Drain the pump.



This pump is designed to handle liquids

containing large entrained solids or slurries. Do not attempt to pump volatile, corrosive, or flammable materials which may damage the pump or endanger personnel as a result of pump failure.



After the pump has been positioned, make certain that the pump and all piping connections are tight, properly supported and secure before operation.



Do not operate the pump without the guards in place over the rotating parts. Exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.



Do not remove plates, covers, gauges, pipe plugs, or fittings from an over-heated pump. Vapor pressure within the pump can cause parts being disengaged to be ejected with great force. Allow the pump to completely completely cool before servicing.



Do not operate the pump against a closed discharge valve for long periods of time. If operated against a closed discharge valve, pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

OM-01929 T SERIES



Use lifting and moving equipment in good repair and with adequate capacity to prevent injuries to personnel or damage to equipment. Suction and discharge hoses and piping must be removed from the pump before lifting.



Do not attempt to disengage any part of an overheated pump unit. Vapor pressure within the pump casing can eject these parts with great force when they are disengaged. Allow the pump to completely cool before servicing it.



Pumps and related equipment must be installed and operated according to all national, local and industry standards.



Overheated pumps can cause severe burns and injury. If overheating of the pump occurs:

- 1. Stop the pump immediately.
- 2. Allow the pump to completely cool.
- 3. Refer to instructions in this manual before restarting the pump.

INSTALLATION - SECTION B

Review all SAFETY information in Section A.

Since pump installations are seldom identical, this section offers only general recommendations and practices required to inspect, position, and arrange the pump and piping.

Most of the information pertains to a standard static lift application where the pump is positioned above the free level of liquid to be pumped.

If installed in a **flooded suction application** where the liquid is supplied to the pump under pressure, some of the information such as mounting, line configuration, and priming must be tailored to the specific application. Since the pressure supplied to the pump is critical to performance and safety, **be sure** to limit the incoming pressure to **50%** of the maximum permissible operating pressure as shown on the pump performance curve.

For further assistance, contact your Gorman-Rupp distributor or the Gorman-Rupp Company.

Pump Dimensions

See Figure 1 for the approximate physical dimensions of this pump.

OUTLINE DRAWING

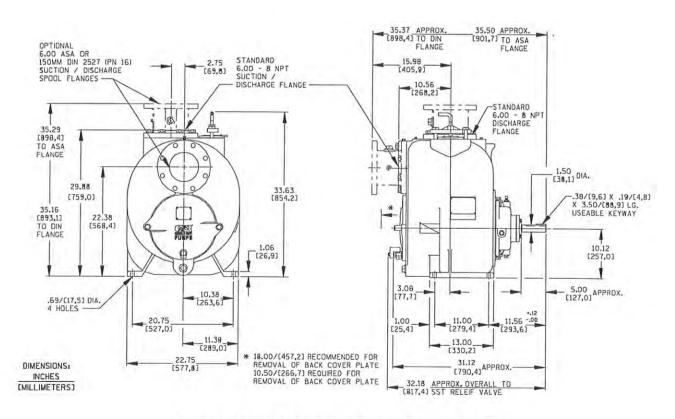


Figure 1. Pump Model T6A60-B, Including /F and /FM

OM-01929 T SERIES

PREINSTALLATION INSPECTION

The pump assembly was inspected and tested before shipment from the factory. Before installation, inspect the pump for damage which may have occurred during shipment. Check as follows:

- Inspect the pump for cracks, dents, damaged threads, and other obvious damage.
- Check for and tighten loose attaching hardware. Since gaskets tend to shrink after drying, check for loose hardware at mating surfaces.
- c. Carefully read all warnings and cautions contained in this manual or affixed to the pump, and perform all duties indicated. Note the direction of rotation indicated on the pump. Check that the pump shaft rotates counterclockwise when facing the impeller.



Only operate this pump in the direction indicated by the arrow on the pump body and on the accompanying decal. Refer to **ROTATION** in **OPERATION**, Section C.

- d. Check levels and lubricate as necessary. Refer to LUBRICATION in the MAINTENANCE AND REPAIR section of this manual and perform duties as instructed.
- e. If the pump and power source have been stored for more than 12 months, some of the components or lubricants may have exceeded their maximum shelf life. These must be inspected or replaced to ensure maximum pump service.

If the maximum shelf life has been exceeded, or if anything appears to be abnormal, contact your Gorman-Rupp distributor or the factory to determine the repair or updating policy. **Do not** put the pump into service until appropriate action has been taken.

POSITIONING PUMP

Lifting

Pump unit weights will vary depending on the mounting and drive provided. Check the shipping tag on the unit packaging for the actual weight, and use lifting equipment with appropriate capacity. Drain the pump and remove all customer-installed equipment such as suction and discharge hoses or piping before attempting to lift existing, installed units.



The pump assembly can be seriously damaged if the cables or chains used to lift and move the unit are improperly wrapped around the pump.

Mounting

Locate the pump in an accessible place as close as practical to the liquid being pumped. Level mounting is essential for proper operation.

The pump may have to be supported or shimmed to provide for level operation or to eliminate vibration.

Clearance

When positioning the pump, allow a minimum clearance of 18 inches (457 mm) in front of the back cover to permit removal of the cover and easy access to the pump interior.

SUCTION AND DISCHARGE PIPING

Pump performance is adversely effected by increased suction lift, discharge elevation, and friction losses. See the performance curve and operating range shown on Page E-1 to be sure your overall application allows pump to operate within the safe operation range.

Materials

Either pipe or hose maybe used for suction and discharge lines; however, the materials must be

PAGE B – 2 INSTALLATION

83 APPENDIX K

compatible with the liquid being pumped. If hose is used in suction lines, it must be the rigid-wall, reinforced type to prevent collapse under suction. Using piping couplings in suction lines is not recommended.

Line Configuration

Keep suction and discharge lines as straight as possible to minimize friction losses. Make minimum use of elbows and fittings, which substantially increase friction loss. If elbows are necessary, use the long-radius type to minimize friction loss.

Connections to Pump

Before tightening a connecting flange, align it exactly with the pump port. Never pull a pipe line into place by tightening the flange bolts and/or couplings.

Lines near the pump must be independently supported to avoid strain on the pump which could cause excessive vibration, decreased bearing life, and increased shaft and seal wear. If hose-type lines are used, they should have adequate support to secure them when filled with liquid and under pressure.

Gauges

Most pumps are drilled and tapped for installing discharge pressure and vacuum suction gauges. If these gauges are desired for pumps that are not tapped, drill and tap the suction and discharge lines not less than 18 inches (457,2 mm) from the suction and discharge ports and install the lines. Installation closer to the pump may result in erratic readings.

SUCTION LINES

To avoid air pockets which could affect pump priming, the suction line must be as short and direct as possible. When operation involves a suction lift, the line must always slope upward to the pump from the source of the liquid being pumped; if the line slopes down to the pump at any point along the suction run, air pockets will be created.

Fittings

Suction lines should be the same size as the pump inlet. If reducers are used in suction lines, they should be the eccentric type, and should be installed with the flat part of the reducers uppermost to avoid creating air pockets. Valves are not normally used in suction lines, but if a valve is used, install it with the stem horizontal to avoid air pockets.

Strainers

If a strainer is furnished with the pump, be certain to use it; any spherical solids which pass through a strainer furnished with the pump will also pass through the pump itself.

If a strainer is not furnished with the pump, but is installed by the pump user, make certain that the total area of the openings in the strainer is at least three or four times the cross section of the suction line, and that the openings will not permit passage of solids larger than the solids handling capability of the pump.

This pump is designed to handle up to 3-inch (76,2 mm) diameter spherical solids.

Sealing

Since even a slight leak will affect priming, head, and capacity, especially when operating with a high suction lift, all connections in the suction line should be sealed with pipe dope to ensure an airtight seal. Follow the sealant manufacturer's recommendations when selecting and applying the pipe dope. The pipe dope should be compatible with the liquid being pumped.

Suction Lines In Sumps

If a single suction line is installed in a sump, it should be positioned away from the wall of the sump at a distance equal to 1 1/2 times the diameter of the suction line.

If there is a liquid flow from an open pipe into the sump, the flow should be kept away from the suction inlet because the inflow will carry air down into the sump, and air entering the suction line will reduce pump efficiency.

OM-01929 T SERIES

If it is necessary to position inflow close to the suction inlet, install a baffle between the inflow and the suction inlet at a distance 1 1/2 times the diameter of the suction pipe. The baffle will allow entrained air to escape from the liquid before it is drawn into the suction inlet.

If two suction lines are installed in a single sump, the flow paths may interact, reducing the efficiency of one or both pumps. To avoid this, position the suction inlets so that they are separated by a distance equal to at least 3 times the diameter of the suction pipe.

Suction Line Positioning

The depth of submergence of the suction line is critical to efficient pump operation. Figure 2 shows recommended minimum submergence vs. velocity.

NOTE

The pipe submergence required may be reduced by installing a standard pipe increaser fitting at the end of the suction line. The larger opening size will reduce the inlet velocity. Calculate the required submergence using the following formula based on the increased opening size (area or diameter).

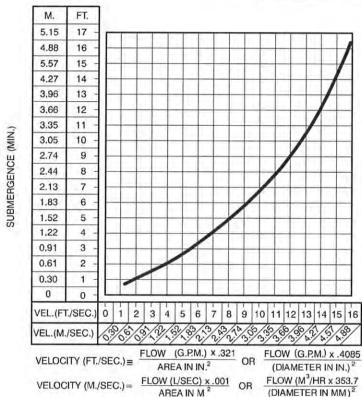


Figure 2. Recommended Minimum Suction Line Submergence vs. Velocity

DISCHARGE LINES

Valves

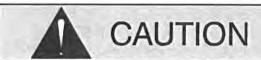
Siphoning

Do not terminate the discharge line at a level lower than that of the liquid being pumped unless a siphon breaker is used in the line. Otherwise, a siphoning action causing damage to the pump could result. If a throttling valve is desired in the discharge line, use a valve as large as the largest pipe to minimize friction losses. Never install a throttling valve in a suction line.

With high discharge heads, it is recommended that a throttling valve and a system check valve be installed in the discharge line to protect the pump from excessive shock pressure and reverse rotation when it is stopped.

PAGE B — 4 INSTALLATION

85 APPENDIX K



If the application involves a high discharge head, gradually close the discharge throttling valve before stopping the pump.

Bypass Lines

Self-priming pumps are not air compressors. During the priming cycle, air from the suction line must be vented to atmosphere on the discharge side. If the discharge line is open, this air will be vented through the discharge. However, if a check valve has been installed in the discharge line, the discharge side of the pump must be opened to atmospheric pressure through a bypass line installed between the pump discharge and the check valve. A self-priming centrifugal pump will not prime if there is sufficient static liquid head to hold the discharge check valve closed.

NOTE

The bypass line should be sized so that it does not affect pump discharge capacity; however, the bypass line should be at least 1 inch in diameter to minimize the chance of plugging.

In low discharge head applications (less than 30 feet or 9 meters), it is recommended that the bypass line be run back to the wet well, and located 6 inches below the water level or cut-off point of the low level pump. In some installations, this bypass line may be terminated with a six-to-eight foot length of 1 1/4 inch I.D. smooth-bore hose; air and liquid vented during the priming process will then agitate the hose and break up any solids, grease, or other substances likely to cause clogging.



A bypass line that is returned to a wet well must be secured against being drawn into the pump suction inlet.

It is also recommended that pipe unions be installed at each 90° elbow in a bypass line to ease disassembly and maintenance.

In high discharge head applications (more than 30 feet), an excessive amount of liquid may be bypassed and forced back to the wet well under the full working pressure of the pump; this will reduce overall pumping efficiency. Therefore, it is recommended that a Gorman-Rupp Automatic Air Release Valve be installed in the bypass line.

Gorman-Rupp Automatic Air Release Valves are reliable, and require minimum maintenance. See AUTOMATIC AIR RELEASE VALVE in this section for installation and theory of operation of the Automatic Air Release Valve. Consult your Gorman-Rupp distributor, or contact the Gorman-Rupp Company for selection of an Automatic Air Release Valve to fit your application.

If the installation involves a flooded suction such as a below-ground lift station. A pipe union and manual shut-off valve may be installed in the bleed line to allow service of the valve without shutting down the station, and to eliminate the possibility of flooding. If a manual shut-off valve is installed **anywhere** in the air release piping, it **must** be a full-opening **ball type** valve to prevent plugging by solids.



If a manual shut-off valve is installed in a bypass line, it must not be left closed during operation. A closed manual shut-off valve may cause a pump which has lost prime to continue to operate without reaching prime, causing dangerous overheating and possible explosive rupture of the pump casing. Personnel could be severely injured.

Allow an over-heated pump to cool before servicing. Do not remove plates, covers, gauges, or fittings from an overheated pump. Liquid within the pump can reach boiling temperatures, and vapor pressure within the pump can cause parts being disengaged to be ejected with great force. After the pump cools, drain the liquid from the pump by removing the casing drain plug. Use cauOM-01929 T SERIES

tion when removing the plug to prevent injury to personnel from hot liquid.

AUTOMATIC AIR RELEASE VALVE

When properly installed, a Gorman-Rupp Automatic Air Release Valve will permit air to escape through the bypass line and then close automatically when the pump is fully primed and pumping at full capacity.



Some leakage (1 to 5 gallons [3.8 to 19

liters] per minute) will occur when the valve is fully closed. <u>Be sure</u> the bypass line is directed back to the wet well or tank to prevent hazardous spills.

Consult the manual accompanying the Air Release Valve for additional information on valve installation and performance.

Air Release Valve Installation

The Automatic Air Release Valve must be independently mounted in a horizontal position between the pump discharge port and the inlet side of the discharge check valve (see Figure 3). The inlet opening in the Air Release Valve is equipped with standard 1-inch NPT pipe threads.

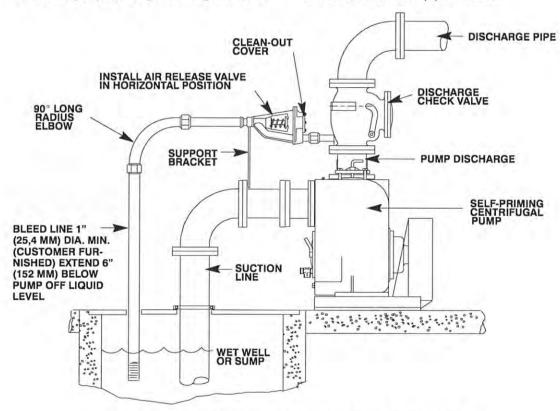


Figure 3. Typical Automatic Air Release Valve Installation

Connect the valve outlet to a bleed line which slopes back to the wet well or sump. The bleed line must be the same size as the outlet opening or larger, depending on which Air Release Valve is being used. If **piping** is used for the bleed line, avoid the use of elbows whenever possible.

NOTE

For multiple pump installations, it is recommended

that each Air Release Valve be fitted with an independent bleeder line directed back to the wet well. If multiple Air Release Valves are installed in a system, do not direct bleeder lines to a common manifold pipe. Contact your Gorman-Rupp distributor or the Gorman-Rupp Company for information about installation of an Automatic Air Release Valve for your specific application.

PAGE B – 6 INSTALLATION

ALIGNMENT

The alignment of the pump and its power source is critical for trouble-free mechanical operation. In either a flexible coupling or V-belt driven system, the driver and pump must be mounted so that their shafts are aligned with and parallel to each other. It is imperative that alignment be checked after the pump and piping are installed, and before operation.

NOTE

Check Rotation, Section C, before final alignment of the pump.

When mounted at the Gorman-Rupp factory, driver and pump are aligned before shipment. Misalignment will occur in transit and handling. Pumps must be checked and realigned before operation. Before checking alignment, tighten the foundation bolts. The pump casing feet and/or pedestal feet, and the driver mounting bolts should also be tightly secured.



When checking alignment, disconnect the power source to ensure that the pump will remain inoperative.



Adjusting the alignment in one direction may alter the alignment in another direction. check each procedure after altering alignment.

Coupled Drives

When using couplings, the axis of the power source must be aligned to the axis of the pump shaft in both the horizontal and vertical planes. Most couplings require a specific gap or clearance between the driving and the driven shafts. Refer to the coupling manufacturer's service literature.

Align spider insert type couplings by using calipers to measure the dimensions on the circumference of the outer ends of the coupling hub every 90°.

The coupling is in alignment when the hub ends are the same distance apart at all points (see Figure 4A).

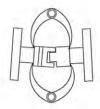


Figure 4A. Aligning Spider-Type Couplings

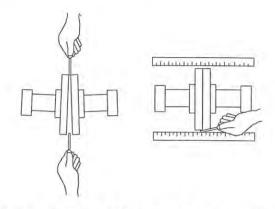


Figure 4B. Aligning Non-Spider Type Couplings

Align non-spider type couplings by using a feeler gauge or taper gauge between the coupling halves every 90°. The coupling is in alignment when the hubs are the same distance apart at all points (see Figure 4B).

Check parallel adjustment by laying a straightedge across both coupling rims at the top, bottom, and side. When the straightedge rests evenly on both halves of the coupling, the coupling is in horizontal parallel alignment. If the coupling is misaligned, use a feeler gauge between the coupling and the straightedge to measure the amount of misalignment.

V-Belt Drives

When using V-belt drives, the power source and the pump must be parallel. Use a straightedge along the sides of the pulleys to ensure that the pulleys are properly aligned (see Figure 4C). In drive systems using two or more belts, make certain that the belts are a matched set; unmatched sets will cause accelerated belt wear.

OM-01929 T SERIES

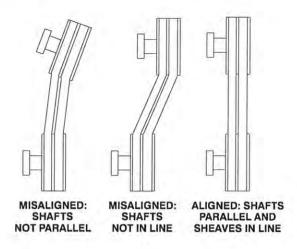


Figure 4C. Alignment of V-Belt Driven Pumps

Tighten the belts in accordance with the belt manufacturer's instructions. If the belts are too loose, they will slip; if the belts are too tight, there will be excessive power loss and possible bearing failure. Select pulleys that will match the proper speed ratio; overspeeding the pump may damage both pump and power source.



Do not operate the pump without the guard in place over the rotating parts. exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

DRIVE BELT TENSIONING

General Rules of Tensioning

For new drive belts, check the tension after 5, 20 and 50 hours of operation and re-tension as required (see the following procedure for measuring belt tension). Thereafter, check and re-tension if required monthly or at 500 hour intervals, whichever comes first.

Ideal drive belt tension is the **lowest** tension at which the belt will not slip under peak load conditions. Do not over-tension drive belts. Over-tensioning will shorten both drive belt and bearing life. Under-tensioning will cause belt slippage. Always keep belts free from dirt, grease, oil and other foreign material which may cause slippage.

PAGE B – 8 INSTALLATION

T SERIES OM-01929

OPERATION - SECTION C

Review all SAFETY information in Section A.

Follow the instructions on all tags, labels and decals attached to the pump.



This pump is designed to handle liquids containing large entrained solids and slurries. Do not attempt to pump volatile, corrosive, or flammable liquids which may damage the pump or endanger personnel as a result of pump failure.



Pump speed and operating conditions must be within the performance range shown on page E-1.

PRIMING

Install the pump and piping as described in IN-STALLATION. Make sure that the piping connections are tight, and that the pump is securely mounted. Check that the pump is properly lubricated (see LUBRICATION in MAINTENANCE AND REPAIR).

This pump is self-priming, but the pump should never be operated unless there is liquid in the pump casing.



Never operate this pump unless there is liquid in the pump casing. The pump will not prime when dry. extended operation of a dry pump will destroy the seal assembly.

Add liquid to the pump casing when:

- The pump is being put into service for the first time.
- 2. The pump has not been used for a considerable length of time.
- The liquid in the pump casing has evaporated.

Once the pump casing has been filled, the pump will prime and reprime as necessary.



After filling the pump casing, reinstall and tighten the fill plug. Do not attempt to operate the pump unless all connecting piping is securely installed. Otherwise, liquid in the pump forced out under pressure could cause injury to personnel.

To fill the pump, remove the pump casing fill cover or fill plug in the top of the casing, and add clean liquid until the casing is filled. Replace the fill cover or fill plug before operating the pump.

STARTING

Consult the operations manual furnished with the power source.

Rotation

The correct direction of pump rotation is counterclockwise when facing the impeller. The pump could be damaged and performance adversely affected by incorrect rotation. If pump performance is not within the specified limits (see the curve on page E-1), check the direction of power source rotation before further troubleshooting.

If an electric motor is used to drive the pump, remove V-belts, couplings, or otherwise disconnect the pump from the motor before checking motor rotation. Operate the motor independently while observing the direction of the motor shaft, or cooling fan. OM-01929 T SERIES

If rotation is incorrect on a three-phase motor, have a qualified electrician interchange any two of the three phase wires to change direction. If rotation is incorrect on a single-phase motor, consult the literature supplied with the motor for specific instructions.

OPERATION

Lines With a Bypass

If a Gorman-Rupp Automatic Air Release Valve has been installed, the valve will automatically open to allow the pump to prime, and automatically close after priming is complete (see INSTALLATION for Air Release Valve operation).

If the bypass line is open, air from the suction line will be discharged through the bypass line back to the wet well during the priming cycle. Liquid will then continue to circulate through the bypass line while the pump is in operation.

Lines Without a Bypass

Open all valves in the discharge line and start the power source. Priming is indicated by a positive reading on the discharge pressure gauge or by a quieter operation. The pump may not prime immediately because the suction line must first fill with liquid. If the pump fails to prime within five minutes, stop it and check the suction line for leaks.

After the pump has been primed, partially close the discharge line throttling valve in order to fill the line slowly and guard against excessive shock pressure which could damage pipe ends, gaskets, sprinkler heads, and any other fixtures connected to the line. When the discharge line is completely filled, adjust the throttling valve to the required flow rate.



Do not operate the pump against a closed discharge throttling valve for long periods of time. If operated against a closed discharge throttling valve,

pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

Leakage

No leakage should be visible at pump mating surfaces, or at pump connections or fittings. Keep all line connections and fittings tight to maintain maximum pump efficiency.

Liquid Temperature And Overheating

The maximum liquid temperature for this pump is 160° F (71° C). Do not apply it at a higher operating temperature.

Overheating can occur if operated with the valves in the suction or discharge lines closed. Operating against closed valves could bring the liquid to a boil, build pressure, and cause the pump to rupture or explode. If overheating occurs, stop the pump and allow it to cool before servicing it. Refill the pump casing with cool liquid.



Allow an over-heated pump to cool before servicing. Do not remove plates, covers, gauges, or fittings from an overheated pump. Liquid within the pump can reach boiling temperatures, and vapor pressure within the pump can cause parts being disengaged to be ejected with great force. After the pump cools. drain the liquid from the pump by removing the casing drain plug. Use caution when removing the plug to prevent injury to personnel from hot liquid.

As a safeguard against rupture or explosion due to heat, this pump is equipped with a pressure relief valve which will open if vapor pressure within the pump casing reaches a critical point. If overheating does occur, stop the pump immediately and allow it to cool before servicing it. Approach any overheated pump cautiously. It is recommended that

PAGE C - 2 **OPERATION** 91

T SERIES OM-01929

the pressure relief valve assembly be replaced at each overhaul, or any time the pump casing overheats and activates the valve. **Never** replace this valve with a substitute which has not been specified or provided by the Gorman-Rupp Company.

Strainer Check

If a suction strainer has been shipped with the pump or installed by the user, check the strainer regularly, and clean it as necessary. The strainer should also be checked if pump flow rate begins to drop. If a vacuum suction gauge has been installed, monitor and record the readings regularly to detect strainer blockage.

Never introduce air or steam pressure into the pump casing or piping to remove a blockage. This could result in personal injury or damage to the equipment. If backflushing is absolutely necessary, liquid pressure **must** be limited to 50% of the maximum permissible operating pressure shown on the pump performance curve.

Pump Vacuum Check

With the pump inoperative, install a vacuum gauge in the system, using pipe dope on the threads. Block the suction line and start the pump. At operating speed the pump should pull a vacuum of 20 inches (508,0 mm) or more of mercury. If it does not, check for air leaks in the seal, gasket, or discharge valve.

Open the suction line, and read the vacuum gauge with the pump primed and at operation speed. Shut off the pump. The vacuum gauge reading will immediately drop proportionate to static suction lift, and should then stabilize. If the vacuum reading falls off rapidly after stabilization, an air leak exists. Before checking for the source of the leak, check the point of installation of the vacuum gauge.

STOPPING

Never halt the flow of liquid suddenly. If the liquid being pumped is stopped abruptly, damaging shock waves can be transmitted to the pump and piping system. Close all connecting valves slowly.

On engine driven pumps, reduce the throttle speed slowly and allow the engine to idle briefly before stopping.



If the application involves a high discharge head, gradually close the discharge throttling valve before stopping the pump.

After stopping the pump, lock out or disconnect the power source to ensure that the pump will remain inoperative.



Do not operate the pump against a closed discharge throttling valve for long periods of time. If operated against a closed discharge throttling valve, pump components will deteriorate, and the liquid could come to a boil, build pressure, and cause the pump casing to rupture or explode.

Cold Weather Preservation

In below freezing conditions, drain the pump to prevent damage from freezing. Also, clean out any solids by flushing with a hose. Operate the pump for approximately one minute; this will remove any remaining liquid that could freeze the pump rotating parts. If the pump will be idle for more than a few hours, or if it has been pumping liquids containing a large amount of solids, drain the pump, and flush it thoroughly with clean water. To prevent large solids from clogging the drain port and preventing the pump from completely draining, insert a rod or stiff wire in the drain port, and agitate the liquid during the draining process. Clean out any remaining solids by flushing with a hose.

BEARING TEMPERATURE CHECK

Bearings normally run at higher than ambient temperatures because of heat generated by friction. Temperatures up to 160°F (71° C) are considered normal for bearings, and they can operate safely to at least 180°F (82° C).

Checking bearing temperatures by hand is inaccurate. Bearing temperatures can be measured accurately by placing a contact-type thermometer against the housing. Record this temperature for future reference.

A sudden increase in bearing temperature is a warning that the bearings are at the point of failing

to operate properly. Make certain that the bearing lubricant is of the proper viscosity and at the correct level (see **LUBRICATION** in **MAINTENANCE AND REPAIR**). Bearing overheating can also be caused by shaft misalignment and/or excessive vibration.

When pumps are first started, the bearings may seem to run at temperatures above normal. Continued operation should bring the temperatures down to normal levels.

TROUBLESHOOTING - SECTION D

Review all SAFETY information in Section A.



Before attempting to open or service the pump:

- 1. Familiarize yourself with this manual.
- Lock out or disconnect the power source to ensure that the pump will remain inoperative.
- Allow the pump to completely cool if overheated.
- 4. Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- 6. Vent the pump slowly and cautiously.
- 7. Drain the pump.

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY		
PUMP FAILS TO PRIME	Not enough liquid in casing.	Add liquid to casing. See PRIM-ING.		
	Suction check valve contaminated or damaged.	Clean or replace check valve.		
	Air leak in suction line.	Correct leak.		
	Lining of suction hose collapsed.	Replace suction hose.		
	Leaking or worn seal or pump gasket.	Check pump vacuum. Replace leaking or worn seal or gasket.		
	Suction lift or discharge head too high.	Check piping installation and install bypass line if needed. See INSTALLATION.		
	Strainer clogged.	Check strainer and clean if necessary.		
PUMP STOPS OR	Air leak in suction line.	Correct leak.		
FAILS TO DELIVER RATED FLOW OR	Lining of suction hose collapsed.	Replace suction hose.		
PRESSURE	Leaking or worn seal or pump gasket.	Check pump vacuum. Replace leaking or worn seal or gasket.		

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY		
PUMP STOPS OR FAILS TO DELIVER RATED FLOW OR	Strainer clogged.	Check strainer and clean if necessary.		
PRESSURE	Suction intake not submerged at proper level or sump too small.	Check installation and correct sub mergence as needed.		
	Impeller or other wearing parts worn or damaged.	Replace worn or damaged parts. Check that impeller is properly centered and rotates freely.		
	Impeller clogged.	Free impeller of debris.		
	Pump speed too slow.	Check driver output; check belts or couplings for slippage.		
	Discharge head too high.	Install bypass line.		
	Suction lift too high.	Measure lift w/vacuum gauge. Reduce lift and/or friction losses in suction line.		
PUMP REQUIRES TOO MUCH POWER	Pump speed too high.	Check driver output; check that sheaves or couplings are cor- rectly sized.		
	Discharge head too low.	Adjust discharge valve.		
	Liquid solution too thick.	Dilute if possible.		
	Bearing(s) frozen.	Disassemble pump and check bearing(s).		
PUMP CLOGS	Liquid solution too thick.	Dilute if possible.		
FREQUENTLY	Discharge flow too slow.	Open discharge valve fully to increase flow rate, and run power source at maximum governed speed.		
	Suction check valve or foot valve clogged or binding.	Clean valve.		
EXCESSIVE NOISE	Cavitation in pump.	Reduce suction lift and/or friction losses in suction line. Record vacuum and pressure gauge readings and consult local representative or factory.		
4	Pumping entrained air.	Locate and eliminate source of air bubble.		
	Pump or drive not securely mounted.	Secure mounting hardware.		
	Impeller clogged or damaged.	Clean out debris; replace damaged parts.		

TROUBLE	POSSIBLE CAUSE	PROBABLE REMEDY		
BEARINGS RUN TOO HOT	Bearing temperature is high, but within limits.	Check bearing temperature regularly to monitor any increase.		
	Low or incorrect lubricant.	Check for proper type and level of lubricant.		
	Suction and discharge lines not properly supported.	Check piping installation for proper support.		
	Drive misaligned.	Align drive properly.		

PREVENTIVE MAINTENANCE

Since pump applications are seldom identical, and pump wear is directly affected by such things as the abrasive qualities, pressure and temperature of the liquid being pumped, this section is intended only to provide general recommendations and practices for preventive maintenance. Regardless of the application however, following a routine preventive maintenance schedule will help assure trouble-free performance and long life from your Gorman-Rupp pump. For specific questions concerning your application, contact your Gorman-Rupp distributor or the Gorman-Rupp Company.

Record keeping is an essential component of a good preventive maintenance program. Changes in suction and discharge gauge readings (if so equipped) between regularly scheduled inspections can indicate problems that can be corrected before system damage or catastrophic failure occurs. The appearance of wearing parts should also be documented at each inspection for comparison as well. Also, if records indicate that a certain part (such as the seal) fails at approximately the same duty cycle, the part can be checked and replaced before failure occurs, reducing unscheduled down time.

For new applications, a first inspection of wearing parts at 250 hours will give insight into the wear rate for your particular application. Subsequent inspections should be performed at the intervals shown on the chart below. Critical applications should be inspected more frequently.

Preventive Maintenance Schedule										
	Service Interval*									
Item	Daily	Weekly	Monthly	Semi- Annually	Annually					
General Condition (Temperature, Unusual Noises or Vibrations, Cracks, Leaks, Loose Hardware, Etc.) Pump Performance (Gauges, Speed, Flow) Bearing Lubrication Seal Lubrication (And Packing Adjustment, If So Equipped) V-Belts (If So Equipped) Air Release Valve Plunger Rod (If So Equipped) Front Impeller Clearance (Wear Plate) Rear Impeller Clearance (Seal Plate) Check Valve Pressure Relief Valve (If So Equipped) Pump and Driver Alignment Shaft Deflection Bearings Bearing Housing Piping Driver Lubrication — See Mfgr's Literature	i i	1	1	C	R					

Legend:

I = Inspect, Clean, Adjust, Repair or Replace as Necessary

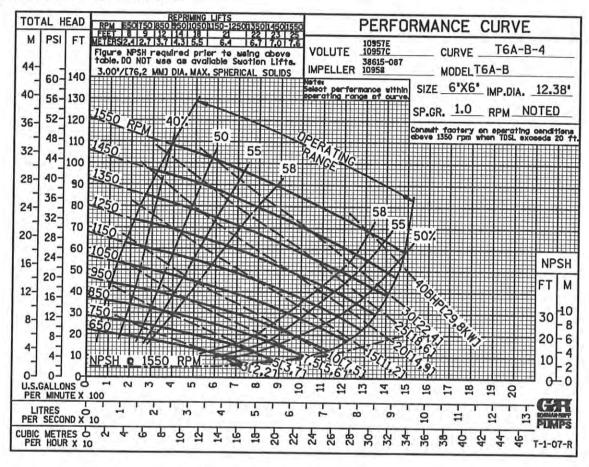
C = Clean

R = Replace

* Service interval based on an intermittent duty cycle equal to approximately 4000 hours annually. Adjust schedule as required for lower or higher duty cycles or extreme operating conditions.

PUMP MAINTENANCE AND REPAIR - SECTION E

MAINTENANCE AND REPAIR OF THE WEARING PARTS OF THE PUMP WILL MAINTAIN PEAK OPERATING PERFORMANCE.



* STANDARD PERFORMANCE FOR PUMP MODEL T6A60-B, Including /F and /FM

*Based on 70° F (21° C) clear water at sea level with minimum suction lift. Since pump installations are seldom identical, your performance may be difference due to such factors as viscosity, specific gravity, elevation, temperature, and impeller trim.

If your pump serial number is followed by an "N", your pump is **NOT** a standard production model.

Contact the Gorman-Rupp Company to verify performance or part numbers.



Pump speed and operating condition points must be within the continuous performance range shown on the curve.

SECTION DRAWING

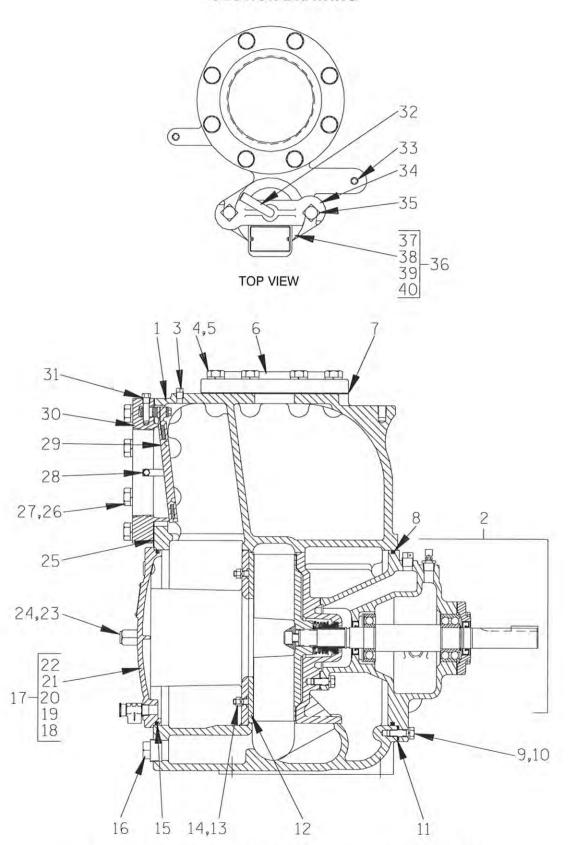


Figure 1. Pump Model T6A60-B, Including /F and /FM

PARTS LIST Pump Model T6A60-B, Including /F and /FM

(From S/N 791258 Up)

If your pump serial number is followed by an "N", your pump is NOT a standard production model. Contact the Gorman-Rupp Company to verify part numbers.

NO.	PART NAME	PART NUMBER	MAT'L CODE	QTY	ITEM F	PART NAME	PART NUMBER	MAT'L CODE	QTY
1	PUMP CASING	10957C	10010	1	1	WARNING DECAL	2613FE		1.
2 *	REPAIR ROTATING ASSY	44163-050		1	3	NAME PLATE	38818-040	13990	1
3	PIPE PLUG	P04	15079	1		SUCTION STICKER	6588AG		1
4	HEX HD CAPSCREW	B1208	15991	8	0	PRIMING STICKER	6588AH		1
5	LOCKWASHER	J12	15991	8	1	DISCHARGE STICKER	6588BJ		1
6	DISCHARGE FLANGE	1758	10010	1					
7*	DISCH FLANGE GSKT	1679G	19370	1	OPTION	AL:			
8 *	ROTATING ASSY O-RING	S1676		1		DISASSEMBLY TOOL	48711-020		1
9	HEX HD CAPSCREW	B0806	15991	4					
10	LOCKWASHER	J08	15991	4		F FLANGE KIT	48213-041		1
11 *	ROT ASSY SHIM SET	13131	17040	4		-SUCTION	11402A	10010	1
8 545	WEAR PLATE ASSY	46451-723	24150	1	7	-DISCHARGE	11402B	10010	1
13	LOCKWASHER	J06	15991	4					
14	HEX NUT	D06	15991	4		FM METRIC FLNG KIT	48213-078		1
6.0	BACK COVER O-RING	S1676	10001			-SUCTION	38642-502	10000	1
16	CASING DRAIN PLUG	P20	10009	1		-DISCHARGE	38642-503	10000	1
17	BACK CVR PLATE ASSY	42111-905	10009	1					
18	-DRIVE SCREW	BM#04-03	17000	4		VEAR PLATES:			
19	-WARNING PLATE	2613EV	13990	1	4	-SPA ALLOY	46451-729	24160	1
20	-PRESS RELIEF VALVE	26662-005	13990	1	-	-TUNGSTEN CARBIDE	46451-726	2415D	1
21	-BACK COVER PLATE	NOT AVAILA		1		valva valoteo.			
3.5	-WARNING DECAL	38816-302	DLC	1		CASING HEATERS:	Collins of the		
	STUD	C1211	15991	2		-120V	47811-004		1
	BACK COVER NUT	31871-073	15000	2	-	-240V	47811-005		1
7.0	SUCTION FLANGE GSKT	11402G	19370	1		CHECK VALVE ASSYS:			
	HEX HD CAPSCREW	B1211	15991	8		-NEO SOLID TYPE	40444 040		4.
22	LOCKWASHER	J12	15991	8		-NEO SOLID TYPE -VITON SOLID	46411-019		1
	PIPE PLUG	P04	15079	1		-VITON SOLID -VITON BLOW-OUT	46411-078		1
	SUCT CHK VALVE ASSY	46411-064		1		-VITON BLOW-OUT	46411-088		1
	SUCTION FLANGE	11402	10010	1	ь	RESS RELIEF VALVES:			
	CHECK VALVE PIN	11645	17010	1		-SEWAGE TYPE	46431-628		-2
5.	CLAMP BAR SCREW	31912-009	15000	1		-STAINLESS STEEL	26662-101		1
	PIPE PLUG	P04	15079	i		-OTAINLEGG GTEEL	20002-101		1
67	CLAMP BAR	38111-004	11010	1	н	II TEMP SHUT-DOWN KI	TQ.		
-	MACHINE BOLT	A1014	15991	2		-145°F	48313-186	-	1
	FILL COVER ASSY	42111-344		1		-130°F	48313-256		1
	-DRIVE SCREW		17000	2		-120°F	48313-257		1
759	-FILL COVER PLATE	NOT AVAILAB	23377	1		I TEMP SHUT-DOWN	48313-172		1
	-WARNING PLATE		13990	1		HERMOSTAT KIT 145°F	10010 172		,
1000	-COVER GASKET	50G		500					
10	-OUVER GAGRET	500	19210	1	A	IR RELEASE VALVES:			
OT SH	OWN:					-10# COMP SPRING	GRP33-07A		1
		BM#04-03	17000	4		-25# COMP SPRING	GRP33-07		-
		11421		1					1
		2613M		1		-80# COMP SPRING	GRP33-07B		1
,	TO IT IT DE OAL	LUTUN		. 1	A	R VLVE MOUNTING KIT	46331-515		1

^{*} INDICATES PARTS RECOMMENDED FOR STOCK

SECTION DRAWING

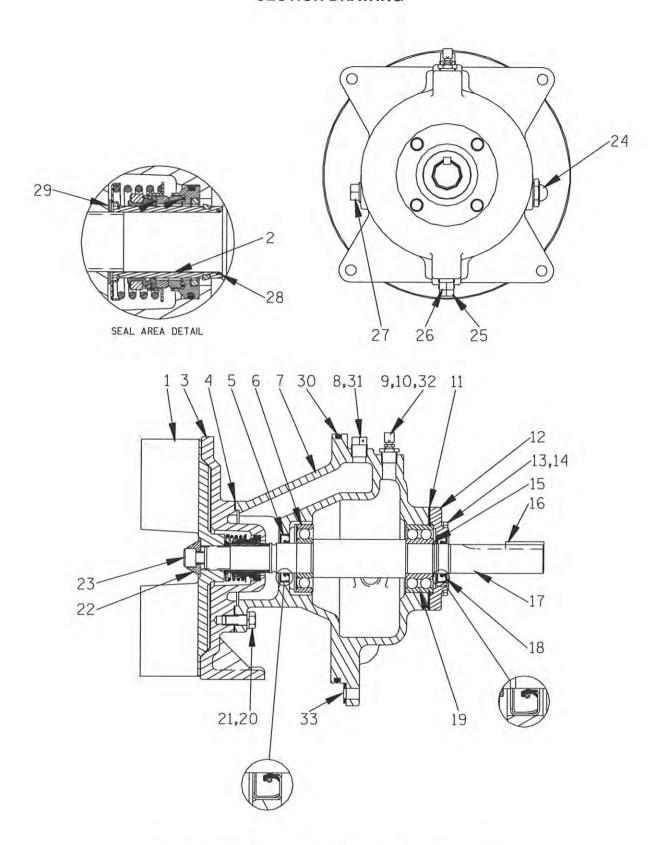


Figure 2. 44163-050 Repair Rotating Assembly

PARTS LIST 44163-050 Repair Rotating Assembly

ITEM PART NAME NO.	PART NUMBER	MAT'L CODE	QTY	ITEM PART NAME NO.	PART NUMBER	MAT'L CODE	QTY
1 * IMPELLER	10958	11010	1	33 * ASSY ADJ SHIM SET	13131	17040	4
2 * SEAL ASSEMBLY	46513-151	444	1				
3 SEAL PLATE	11837E	10010	1	NOT SHOWN			
4 * SEAL PLATE GAS	KET 10959G	20000	1	ROTATION DECAL	2613M		1
5 * INBOARD OIL SEA	AL S1352		1	INSTRUCTION TAG	6588U		1
6 * INBOARD BALL B	EARING 23276-009		1	OPTIONAL:			
7 BEARING HOUSIN		10010	1	STAINLESS STEEL PARTS:			
8 VENTED PLUG	4823A	15079	1	SEAL PLATE	38272-242	10010	1
9 AIR VENT	S1530		1	IMP SHAFT			
10 RED PIPE BUSHIN	IG AP0802	15079	1	(LESS SLEEVE)	10529B	1706H	1
11 ** BEARING CAP G	ASKET 38683-248	18000	1	SPACER WASHER	00000 040		- 0
12 BEARING CAP	38322-215	10010	1	(FOR SST SHAFT) ASTL SEAL SLEEVE	38329-040	17130	1
13 HEX HD CAPSCRI	EW B0605	15991	4	IMPELLERS:	11876B	16000	1
14 LOCKWASHER	J06	15991	4	ADI	10958	1102H	1
15 RETAINING RING	S244		1	-TUNGS CARB COATED		1102H	1
16 * SHAFT KEY	N0612	15990	1	IMP CLEAN-OUT KIT	48783-003		1
17 * IMPELLER SHAFT	10529	16040	1	SEAL PLATE	10700 000		
18 * BEARING CAP OIL			1	-TUNG CARB COATED	11837F	1001D	1
19 * OUTBD BALL BEA			1	-ADI	11837E	1102H	1
20 HEX HD CAPSCRE		15991	4	† ★ AFLAS SEAL(W/SST SLEE	VE		
21 LOCKWASHER	J08	15991	4	OR SOLID SST SHAFT)	46512-194		1
22 IMPELLER WASHE		15030	1	† PERMALON COATED			
23 SOCKET HD CAPS		15991	1	MECH SEAL ASSY	46512-150		1
24 SIGHT GAUGE	S1471		1	† STD MECHANICAL			
25 SEAL CVTY DRAIN		15079	1	SEAL ASSEMBLY	46512-047		1
26 BEARING DRAIN P		15079	1	† MECH SEAL			
27 PIPE PLUG	P12	15079	1	SHAFT SLEEVE	11876A	16000	1
8 * SEAL SLEEVE O-R	ING 25154-022	225	REF	† METAL BELLOWS MECH S			
9 * IMPELLER ADJ SH		17090	REF	✓ (VITON OR EQUAL	46512-147		1
30 * ROTATING ASSY O	market are		1	† METAL BELLOWS MECH S			1
31 SHIPPING PLUG	11495B	15079	1		46512-142		1
32 SHIPPING PLUG	11495B	15079	1	► VITON	25154-454		1
- Jim i mar 200	113000	10013	,	- VIION	20104-404		A.

^{*} INDICATES PARTS RECOMMENDED FOR STOCK

- ✓ KALREZ® AND VITON™ ARE PRODUCTS OF THE DUPONT CORP.
- ★ AFLAS® IS A PRODUCT OF THE 3M CORP.

^{**} FOR PUMPS WITH SERIAL NUMBERS **BELOW** 864836, ORDER 10530G/18000 BEARING CAP GASKET. IF **BOTH** BEARING CAP AND GASKET MUST BE REPLACED, ORDER PARTS LISTED ABOVE.

[†] OPTIONAL MECHANICAL SEAL(S) MUST BE USED WITH MECHANICAL SEAL SHAFT SLEEVE OR SOLID SST SHAFT.

PUMP AND SEAL DISASSEMBLY AND REASSEMBLY

Review all SAFETY information in Section A.

Follow the instructions on all tags, label and decals attached to the pump.

This pump requires little service due to its rugged, minimum-maintenance design. However, if it becomes necessary to inspect or replace the wearing parts, follow these instructions which are keyed to the sectional views (see Figures 1 and 2) and the accompanying parts lists.

This manual will alert personnel to known procedures which require special attention, to those which could damage equipment, and to those which could be dangerous to personnel. However, this manual cannot possibly anticipate and provide detailed precautions for every situation that might occur during maintenance of the unit. Therefore, it is the responsibility of the owner/maintenance personnel to ensure that **only** safe, established maintenance procedures are used, and that any procedures not addressed in this manual are performed **only** after establishing that neither personal safety nor pump integrity are compromised by such practices.

Many service functions may be performed by draining the pump and removing the back cover assembly. If major repair is required, the piping and/or power source must be disconnected. The following instructions assume complete disassembly is required.

Before attempting to service the pump, disconnect or lock out the power source and take precautions to ensure that it will remain inoperative. Close all valves in the suction and discharge lines.

For power source disassembly and repair, consult the literature supplied with the power source, or contact your local power source representative.



Before attempting to open or service the pump:

 Familiarize yourself with this manual.

- Disconnect or lock out the power source to ensure that the pump will remain inoperative.
- Allow the pump to completely cool if overheated.
- Check the temperature before opening any covers, plates, or plugs.
- Close the suction and discharge valves.
- Vent the pump slowly and cautiously.
- 7. Drain the pump.



Use lifting and moving equipment in good repair and with adequate capacity to prevent injuries to personnel or damage to equipment.

Back Cover And Wear Plate Removal

(Figure 1)

The wear plate (12) is easily accessible and may be serviced by removing the back cover assembly (17). Before attempting to service the pump, remove the pump casing drain plug (16) and drain the pump. Clean and reinstall the drain plug.

Remove the back cover nuts (24) and pull the back cover and assembled wear plate from the pump casing (1). Inspect the wear plate, and replace it if badly scored or worn. To remove the wear plate, disengage the hardware (13 and 14).

Inspect the back cover O-ring (15) and replace it if damaged or worn.

Suction Check Valve Removal

(Figure 1)

If the check valve assembly (29) is to be serviced, remove the check valve pin (31), reach through the back cover opening and pull the complete assembly from the suction flange (30).

NOTE

Further disassembly of the check valve is not required since it must be replaced as a complete unit.

PAGE E - 6

MAINTENANCE & REPAIR

Individual parts are not sold separately.

Rotating Assembly Removal

(Figure 2)

The rotating assembly may be serviced without disconnecting the suction or discharge piping; however, the power source must be removed to provide clearance.

The impeller (1) should be loosened while the rotating assembly is still secured to the pump casing. Before loosening the impeller, remove the seal cavity drain plug (25) and drain the seal lubricant. This will prevent the oil in the seal cavity from escaping when the impeller is loosened. Clean and reinstall the seal cavity drain plug.

Immobilize the impeller by wedging a block wood between the vanes and the pump casing, and remove the impeller capscrew and washer (22 and 23).

Install a lathe dog on the drive end of the shaft (17) with the "V" notch positioned over the shaft keyway.

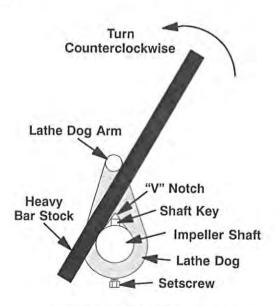


Figure 3. Loosening Impeller

With the impeller rotation still blocked, see Figure 3 and use a long piece of heavy bar stock to pry against the arm of the lathe dog in a counterclockwise direction (when facing the drive end of the shaft). **Use caution** not to damage the shaft or key-

way. When the impeller breaks loose, remove the lathe dog and wood block.

NOTE

Do not remove the impeller until the rotating assembly has been removed from the pump casing.

(Figure 1)

Remove the hardware (9 and 10) securing the rotating assembly to the pump casing. Separate the rotating assembly by pulling straight away from the pump casing.

NOTE

An optional disassembly tool is available from the factory. If the tool is used, follow the instructions packed with it. A similar tool may be assembled using 1/2-inch pipe (schedule 80 steel or malleable iron) and a standard tee (see Figure 4). All threads are 1/2-inch NPT. Do not pre-assemble the tool.

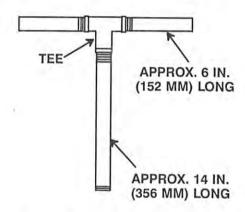


Figure 4. Rotating Assembly Tool

To install the tool, remove the air vent (9, Figure 2) from the bearing housing, and screw the longest length of pipe into the vent hole until fully engaged. Install the tee, and screw the handles into the tee. Use caution when lifting the rotating assembly to avoid injury to personnel or damage to the assembly.

Remove the bearing housing O-ring (8).

Impeller Removal

(Figure 2)

With the rotating assembly removed from the pump casing, unscrew the impeller from the shaft.

Use caution when unscrewing the impeller; tension on the shaft seal spring will be released as the impeller is removed. Inspect the impeller and replace if cracked or badly worn.

Remove the impeller adjusting shims (29); tie and tag the shims, or measure and record their thickness for ease of reassembly.

Seal Removal

(Figure 2)

Slide the integral shaft sleeve and rotating portion of the seal off the shaft as a unit.

Use a pair of stiff wires with hooked ends to remove the stationary element and seat.

An alternate method of removing the stationary seal components is to remove the hardware (20 and 21) and separate the seal plate (3) and gasket (4) from the bearing housing (7). Position the seal plate on a flat surface with the impeller side down. Use a wooden dowel or other suitable tool to press on the back side of the stationary seat until the seat, O-rings, and stationary element can be removed.

Remove the shaft sleeve O-ring (28).

If no further disassembly is required, refer to **Seal Installation**.

Shaft and Bearing Removal and Disassembly (Figure 2)

When the pump is properly operated and maintained, the bearing housing should not require disassembly. Disassemble the shaft and bearings **only** when there is evidence of wear or damage.



Shaft and bearing disassembly in the field is not recommended. These operations should be performed only in a properlyequipped shop by qualified personnel.

Remove the bearing housing drain plug (26) and drain the lubricant. Clean and reinstall the drain plug.

Disengage the hardware (13 and 14) and slide the bearing cap (12) and oil seal (18) off the shaft.Remove the bearing cap gasket (11), and press the oil seal from the bearing cap.

Place a block of wood against the impeller end of the shaft and tap the shaft and assembled bearings (6 and 19) from the bearing housing.

After removing the shaft and bearings, clean and inspect the bearings in place as follows.



To prevent damage during removal from the shaft, it is recommended that bearings be cleaned and inspected **in place**. It is **strongly** recommended that the bearings be replaced **any** time the shaft and bearings are removed.

Clean the bearing housing, shaft and all component parts (except the bearings) with a soft cloth soaked in cleaning solvent. Inspect the parts for wear or damage and replace as necessary.



Most cleaning solvents are toxic and flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Clean the bearings thoroughly in **fresh** cleaning solvent. Dry the bearings with filtered compressed air and coat with light oil.



Bearings must be kept free of all dirt and foreign material. Failure to do so will greatly shorten bearing life. **DO NOT** spin dry bearings. This may scratch the balls or races and cause premature bearing failure.

Rotate the bearings by hand to check for roughness or binding and inspect the bearing balls. If ro-

PAGE E - 8

MAINTENANCE & REPAIR

tation is rough or the bearing balls are discolored, replace the bearings.

The bearing tolerances provide a tight press fit onto the shaft and a snug slip fit into the bearing housing. Replace the bearings, shaft, or bearing housing if the proper bearing fit is not achieved.

If bearing replacement is required, remove the outboard bearing retaining ring (15), and use a bearing puller to remove the bearings from the shaft.

Press the inboard oil seal (5) from the bearing housing.

Shaft and Bearing Reassembly and Installation (Figure 2)

Clean the bearing housing, shaft and all component parts (except the bearings) with a soft cloth soaked in cleaning solvent. Inspect the parts for wear or damage as necessary.



Most cleaning solvents are toxic and flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Inspect the shaft for distortion, nicks or scratches, or for thread damage on the impeller end. Dress small nicks and burrs with a fine file or emery cloth. Replace the shaft if defective.

Position the inboard oil seal (5) in the bearing housing bore with the lip positioned as shown in Figure 2. Press the oil seal into the housing until the face is **just flush** with the machined surface on the housing.



To prevent damage during removal from the shaft, it is recommended that bearings be cleaned and inspected in place. It is strongly recommended that the bearings be replaced **any** time the shaft and bearings are removed.

NOTE

Position the inboard bearing (6) on the shaft with the shielded side toward the impeller end of the shaft. Position the outboard bearing (19) on the shaft with the integral retaining ring on the bearing O.D. toward the drive end of the shaft.

The bearings may be heated to ease installation. An induction heater, hot oil bath, electric oven, or hot plate may be used to heat the bearings. Bearings should **never** be heated with a direct flame or directly on a hot plate.

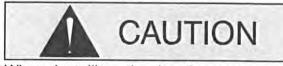
NOTE

If a hot oil bath is used to heat the bearings, both the oil and the container must be **absolutely** clean. If the oil has been previously used, it must be **thoroughly** filtered.

Heat the bearings to a uniform temperature **no higher than** 250°F (120°C), and slide the bearings onto the shaft, one at a time, until they are fully seated. This should be done quickly, in one continuous motion, to prevent the bearings from cooling and sticking on the shaft.

After the bearings have been installed and allowed to cool, check to ensure that they have not moved away from the shaft shoulders in shrinking. If movement has occurred, use a suitable sized sleeve and a press to reposition the bearings against the shaft shoulders.

If heating the bearings is not practical, use a suitable sized sleeve, and an arbor (or hydraulic) press to install the bearings on the shaft.



When installing the bearings onto the shaft, **never** press or hit against the outer race, balls, or ball cage. Press **only** on the inner race.

Secure the outboard bearing on the shaft with the bearing retaining ring (15).

Slide the shaft and assembled bearings into the bearing housing until the retaining ring on the outboard bearing seats against the bearing housing.



When installing the shaft and bearings into the bearing bore, push against the outer race. **Never** hit the balls or ball cage.

Press the outboard oil seal (18) into the bearing cap (12) with the lip positioned as shown in Figure 2. Replace the bearing cap gasket (11), and secure the bearing cap with the hardware (13 and 14). **Be careful** not to damage the oil seal lip on the shaft keyway.

Install the bearing housing O-ring (30).

Lubricate the bearing housing as indicated in **LU-BRICATION**.

Seal Installation

(Figures 2, 5, 6 and 7)



Most cleaning solvents are toxic and

flammable. Use them only in a well ventilated area free from excessive heat, sparks, and flame. Read and follow all precautions printed on solvent containers.

Clean the seal cavity and shaft with a cloth soaked in fresh cleaning solvent. Inspect the stationary seat bore in the seal plate for dirt, nicks and burrs, and remove any that exist. The stationary seat bore **must** be completely clean before installing the seal.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

To ease installation of the seal, lubricate the shaft sleeve O-ring and the external stationary seat O-ring with a very **small** amount of light lubricating oil. See Figure 5 for seal part identification.

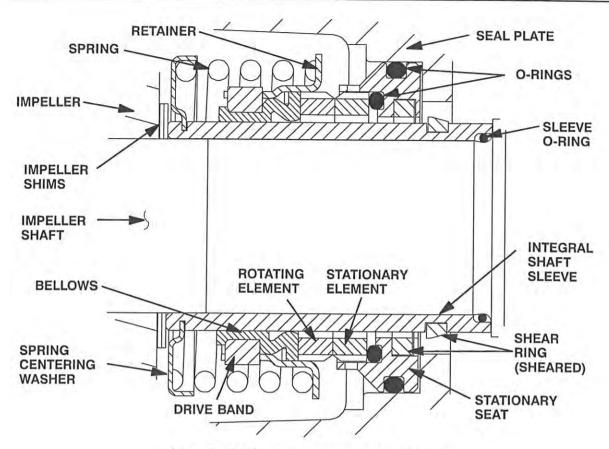


Figure 5. 46513-151 Cartridge Seal Assembly



This seal is not designed for operation at temperatures above 160°F (71°C). Do not use at higher operating temperatures.

If the seal plate was removed, install the seal plate gasket (4). Position the seal plate over the shaft and secure it to the intermediate with the hardware (20 and 21).

To prevent damaging the shaft sleeve O-ring (28) on the shaft threads, stretch the O-ring over a piece of tubing 1-1/4 I.D. x 1-1/2 O.D. x 2-inches long (32 mm x 38 mm x 51 mm). Slide the tube over the shaft threads, then slide the O-ring off the tube and onto the shaft. Remove the tube, and continue to slide the O-ring down the shaft until it seats against the shaft shoulder.

When installing a new cartridge seal assembly, remove the seal from the container, and remove the mylar storage tabs, if so equipped, from between the seal faces.



New cartridge seal assemblies may be equipped with mylar storage tabs between the seal faces. If so equipped, these storage tabs **must** be removed before installing the seal.

Lubricate the external stationary seat O-ring with light oil. Slide the seal assembly onto the shaft until the external stationary seat O-ring engages the bore in the seal plate.

Clean and inspect the impeller as described in Impeller Installation and Adjustment. Install the full set of impeller shims (29) provided with the seal, and screw the impeller onto the shaft until it is seated against the seal (see Figure 6).

Continue to screw the impeller onto the shaft. This will press the stationary seat into the seal plate bore.

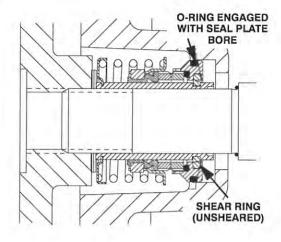


Figure 6. Seal Partially Installed

NOTE

A firm resistance will be felt as the impeller presses the stationary seat into the seal plate bore.

As the stationary seat becomes fully seated, the seal spring compresses, and the shaft sleeve will break the nylon shear ring. This allows the sleeve to slide down the shaft until seated against the shaft shoulder. Continue to screw the impeller onto the shaft until the impeller, shims, and sleeve are fully seated against the shaft shoulder (see Figure 7).

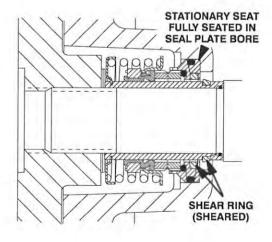


Figure 7. Seal Fully Installed

Measure the impeller-to-seal plate clearance, and remove impeller adjusting shims to obtain the proper clearance as described in **Impeller Installation and Adjustment**.

If necessary to reuse an old seal in an emergency, carefully separate the rotating and stationary seal faces from the bellows retainer and stationary seat.



A new seal assembly should be installed any time the old seal is removed from the pump. Wear patterns on the finished faces cannot be realigned during reassembly. Reusing an old seal could result in premature failure.

Handle the seal parts with extreme care to prevent damage. Be careful not to contaminate precision finished faces; even fingerprints on the faces can shorten seal life. If necessary, clean the faces with a non-oil based solvent and a clean, lint-free tissue. Wipe **lightly** in a concentric pattern to avoid scratching the faces.

Carefully wash all metallic parts in fresh cleaning solvent and allow to dry thoroughly.



Do not attempt to separate the rotating portion of the seal from the shaft sleeve when reusing an old seal. The rubber bellows will adhere to the sleeve during use, and attempting to separate them could damage the bellows.

Inspect the seal components for wear, scoring, grooves, and other damage that might cause leakage. Inspect the integral shaft sleeve for nicks or cuts on either end. If any components are worn, or the sleeve is damaged, replace the complete seal; never mix old and new seal parts.

Install the stationary seal element in the stationary seat. Press this stationary subassembly into the seal plate bore until it seats squarely against the bore shoulder. A push tube made from a piece of plastic pipe would aid this installation. The I.D. of

PAGE E - 12

MAINTENANCE & REPAIR

the pipe should be slightly larger than the O.D. of the shaft sleeve.

Slide the rotating portion of the seal (consisting of the integral shaft sleeve, spring centering washer, spring, bellows and retainer, and rotating element) onto the shaft until the seal faces contact.

Proceed with Impeller Installation and Adjustment.

Impeller Installation

(Figure 2)

Inspect the impeller, and replace it if cracked or badly worn. Inspect the impeller and shaft threads for dirt or damage, and clean or dress the threads as required.



The shaft and impeller threads **must** be completely clean before reinstalling the impeller. Even the slightest amount of dirt on the threads can cause the impeller to seize to the shaft, making future removal difficult or impossible without damage to the impeller or shaft.

Install the same thickness of impeller adjusting shims (29) as previously removed. Apply 'Never-Seez' or equivalent to the shaft threads and screw the impeller onto the shaft until tight.

NOTE

At the slightest sign of binding, immediately back the impeller off, and check the threads for dirt. **Do not** try to force the impeller onto the shaft.

A clearance of .025 to .040 inch (0,64 to 1,02 mm) between the impeller and the seal plate is recommended for maximum pump efficiency. Measure this clearance, and add or remove impeller adjusting shims as required.

NOTE

If the rotating assembly has been installed in the pump casing, this clearance may be measured by reaching through the priming port with a feeler gauge.

NOTE

Proceed with Rotating Assembly Installation before installing the impeller capscrew and washer (22 and 23). The rotating assembly must be installed in the pump casing in order to torque the impeller capscrew.

After the rotating assembly is installed in the pump casing, coat the threads of the impeller capscrew (23) with 'Never-Seez' or equivalent compound, and install the impeller washer (22) and capscrew; torque the capscrew to 90 ft. lbs. (1080 in. lbs. or 12,4 m. kg.).

Rotating Assembly Installation

(Figure 1)

NOTE

If the pump has been completely disassembled, it is recommended that the suction check valve and back cover assembly be reinstalled at this point. The back cover assembly must be in place to adjust the impeller face clearance.

Install the bearing housing and lubricate it with light grease. Ease the rotating assembly into the pump casing using the installation tool. **Be careful** not to damage the O-ring.

Install the four sets of rotating assembly adjusting shims (11) using the same thickness as previously removed. Secure the rotating assembly to the pump casing with the hardware (9 and 10). **Do not** fully tighten the capscrews until the back cover has been reinstalled and the impeller face clearance has been set.

A clearance of .010 to .020 inch (0,25 to 0,51 mm) between the impeller and the wear plate is also recommended for maximum pump efficiency. This clearance can be obtained by removing an equal amount of shims from each rotating assembly shim set until the impeller scrapes against the wear plate when the shaft is turned. After the impeller scrapes, add approximately .015 inch (0,4 mm) of shims to each shim set.

NOTE

An alternate method of adjusting this clearance is to

reach through the suction port with a feeler gauge and measure the gap. Add or subtract rotating assembly shims accordingly.

Suction Check Valve Installation

(Figure 1)

Inspect the check valve assembly (29), and replace it if badly worn.

NOTE

The check valve assembly must be replaced as a complete unit. Individual parts are not sold separately.

Reach through the back cover opening with the check valve (29), and position the check valve adaptor in the mounting slot in the suction flange (30). Align the adaptor with the flange hole, and secure the assembly with the check valve pin (31).

NOTE

If the suction or discharge flanges were removed, replace the respective gaskets, apply 'Permatex Aviation No. 3 Form-A-Gasket' or equivalent compound to the mating surfaces, and secure them to the pump casing with the attaching hardware.

Back Cover Installation

(Figure 1)

If the wear plate (12) was removed for replacement, carefully center it on the back cover and secure it with the hardware (13 and 14). The wear plate **must** be concentric to prevent binding when the back cover is installed.

Replace the back cover O-ring (15), and lubricate it with a generous amount of No. 2 grease. Clean any scale or debris from the contacting surfaces in the pump casing that might interfere or prevent a good seal with the back cover. Slide the back cover assembly into the pump casing. Be sure the wear plate does not bind against the impeller.

NOTE

To ease future disassembly, apply a film of grease or 'Never-Seez' on the back cover shoulder, or any

surface which contacts the pump casing. This action will reduce rust and scale build-up.

Secure the back cover assembly by tightening the back cover nuts (24) evenly. **Do not** over-tighten the hand nuts; they should be just tight enough to ensure a good seal at the back cover shoulder. Be sure the wear plate does not bind against the casing.

PRESSURE RELIEF VALVE MAINTENANCE

(Figure 1)

The back cover is equipped with a pressure relief valve (20) to provide additional safety for the pump and operator (refer to Liquid Temperature And Overheating in OPERATION).

It is recommended that the pressure relief valve assembly be replaced at each overhaul, or any time the pump overheats and activates the valve. **Never** replace this valve with a substitute which has not been specified or provided by the Gorman-Rupp Company.

Periodically, the valve should be removed for inspection and cleaning. When reinstalling the relief valve, apply 'Loctite Pipe Sealant With Teflon No. 592', or equivalent compound, on the relief valve threads. Position the valve as shown in Figure 1 with the discharge port pointing down.

Final Pump Assembly

(Figure 1)

Install the shaft key (16, Figure 2) and reconnect the power source. Be sure to install any guards used over the rotating members.



Do not operate the pump without the guards in place over the rotating parts. Exposed rotating parts can catch clothing, fingers, or tools, causing severe injury to personnel.

Install the suction and discharge lines and open all valves. Make certain that all piping connections are tight, properly supported and secure.

Be sure the pump and power source have been properly lubricated, see LUBRICATION.

Remove the fill cover assembly (36) and fill the pump casing with clean liquid. Reinstall the fill cover and tighten it. Refer to **OPERATION**, Section C, before putting the pump back into service.

LUBRICATION

Seal Assembly

(Figure 2)

Before starting the pump, remove the vented plug (8) and fill the seal cavity with approximately 40 ounces (1,4 liters) of SAE No. 30 non-detergent oil, or to a level just below the tapped vented plug hole. Clean and reinstall the vented plug. Maintain the oil at this level.

Bearings

(Figure 2)

The bearing housing was fully lubricated when shipped from the factory. Check the oil level regularly through the sight gauge (24) and maintain it at the middle of the gauge. When lubrication is required, add SAE No. 30 non-detergent oil through the hole for the air vent (9). **Do not** over-lubricate.

Over-lubrication can cause the bearings to overheat, resulting in premature bearing failure.

NOTE

The white reflector in the sight gauge must be positioned horizontally to provide proper drainage.

Under normal conditions, drain the bearing housing once each year and refill with approximately 32 ounces (1 liter) clean oil. Change the oil more frequently if the pump is operated continuously or installed in an environment with rapid temperature change.



Monitor the condition of the bearing lubricant regularly for evidence of rust or moisture condensation. This is especially important in areas where variable hot and cold temperatures are common.

For cold weather operation, consult the factory or a lubricant supplier for the recommended grade of oil.

Power Source

Consult the literature supplied with the power source, or contact your local power source representative.

THE GORMAN-RUPP COMPANY AND GORMAN-RUPP OF CANADA LIMITED 12 MONTH LIMITED WARRANTY

EXTENT AND DURATION OF WARRANTY

Coverage: The Gorman-Rupp Company or Gorman-Rupp of Canada Limited (herein individually referred to as "GR") each individually warrant that its products and parts shall be free from defects in material and workmanship for twelve (12) months from the date of purchase by the original end user.

Exceptions: This Limited Warranty shall not apply to the following products and parts: engines, motors, trade accessories and other products, components or materials not manufactured by GR. With respect to submersible pumps, the pump and motor are an integral unit and are therefore warranted as a unit. However, with respect to the electrical components in submersible pumps, this warranty is valid **only** when electrical controls for the pump have been specified and/or provided by GR. Wear and tear on any product resulting from normal use is not covered by this Limited Warranty.

LIMITATIONS

GR'S SOLE AND EXCLUSIVE WARRANTY WITH RESPECT TO ITS PRODUCTS AND PARTS IS THIS LIMITED WARRANTY. THIS LIMITED WARRANTY IS IN LIEU OF ALL OTHER EXPRESS AND/OR IMPLIED WARRANTIES, INCLUDING IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR PARTICULAR PURPOSE.

EXCLUSIVE REMEDY AND DAMAGES

The sole and exclusive remedy for breach of this Limited Warranty by GR, and the entire extent of its liability for such breach or for damages arising and/or resulting from the use of the products and parts covered by this Limited Warranty shall be as follows:

- 1. Repair or replacement: If inspection shows that any GR product or part covered under this LimitedWarranty is defective in materials or workmanship, GR shall repair or replace the defective product or part at its option, without charge. You must have properly installed, maintained and used the product or part claimed to be defective in accordance with the maintenance schedule and/or manual which comes with the product. No allowance will be made for labor, transportation or other charges incurred by you in connection with such repair or replacement.
- 2. To obtain the above remedy:
 - a) Immediately notify GR at the address below of the claimed defect in materials or workmanship and provide the serial number or date code of the product and/or part and provide a copy of the invoice or bill of sale referencing the product and/or part by no later than the expiration date of the Limited Warranty period.
 - b) GR will advise whether inspection of the product and/or part will be necessary and whether and how repair or replacement will be effected. If inspection by GR is necessary, the product or part must be sent freight prepaid to GR at the address stated below. Return shipment of the repaired product or part will be F.O.B. the address stated below.
- Damages: GR's liability for damages for breach of this Limited Warranty shall not exceed the amount of the purchase
 price of the product or part in respect to which damages are claimed. IN NO EVENT SHALL GR BE
 LIABLE FOR INCIDENTAL, CONSEQUENTIAL OR SPECIAL DAMAGES FOR
 BREACH OF THIS LIMITED WARRANTY OTHER THAN AS STATED HEREIN.

Some states do not allow the exclusion or limitation of incidental or consequential damages. Accordingly, the above may not apply to you. This Limited Warranty gives you specific legal rights, and you may also have other rights which vary from state to state and province to province.

THE GORMAN-RUPP COMPANY P.O. BOX 1217 MANSFIELD, OH 44901-1217 Phone: (419) 755-1011 GORMAN-RUPP OF CANADA LIMITED 70 Burwell Road St. Thomas, Ontario N5P 3R7 Phone: (519) 631–2870

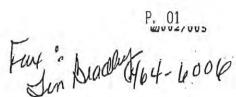






4.1 Sewer Connection Information





CUSTOMER NAME	CUSTOMER ID NUMBER	SERVICE LOCATION	METER ID NUMBE
Borrelli's Pastry Shop	107136	765 Tiogue Ave.	39539596 \
Boston Neck Realty	116473	1650 Nooseneck Hill Rd.	
Coventry Credit Union	114468	1584 Nooseneck Hill Rd.	60106589 \
Cumberland Farms	111938	1600 Nooseneck Hill Rd.	31599205 V
CVS Store #00621-01	105876	743 Tioque Ave.	39597778 V
Glenwood Park	110981	978 Tiogue Ave.	47624300 V
HallKeen Management Inc.	113021	100 Woodland Dr.	31918077 V
HallKeen Management Inc	113019	207 Goldfinch Dr.	60106571 V
HallKeen Management Inc.	113020	309 Woodland Dr.	60106564 V
HallKeen Management Inc.	113018	400 Goldfinch Dr.	60105584 V
HallKeen Management Inc.	112973	110 Coldenst Dr.	60107146 V
fallKeen Management Inc.	112972	110 Goldfinch Dr.	60106590 V
fallKeen Management Inc	112974	310 Goldfinch Dr.	60106566 V
fallKeen Management Inc.	113230	Goldfinch Dr.	23717273 V
fallKeen Management Inc.	113022	1 Viero Ln,	33825338 V
lallKeen Management Inc.	113206	20 Woodland Dr.	60106557 W
lallKeen Management Inc.	113023	20 Woodland Dr.	70174067 W
lallKeen Management Inc	113111	200 Woodland Dr.	60106562 W
aven Eldercare of New England	113312	100 Viero Ln.	60108561 W
ent County Hospital / Cov. Care	113623	11 Woodland Dr.	66302032 W
enyon Oil Company, Inc.	107955	1620 Nooseneck Hill Rd.	39539501 W
eisure Village	113353	851 Tioque Ave.	39749439 VV
ockwood McKinnon Taco Venture		1620 Nooseneck Hill Road	1155706 W
OCO / Leisure Condo's	115274	784 Tiogue Ave.	37272428 W
John & Paul Parish Church	116734	1700 Nooseneck Hill Rd.	
arther John V Doyle School	106734	341 South Main St.	51006475 W
ar Brite Car Wash	109438 :	343 South Main St.	
ar Brite Laundromat	113709	1620 Nooseneck Hill Rd.	31947081 W
op & Shop	113315	1602 Nooseneck Hill Rd.	31947084 W
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gue Veterinary Clinic	114013	1036 Tiogue Ave.	31166858 W
n's Fruit & Deli Inc.	105287	916 Tiogue Ave.	34944727 W
B. Post Office	107959	821 Tiogue Ave.	39117010 W
S Realty	114758	1550 Nooseneck Hill Rd.	31923991 W
S Realty	113545	1600 Nooseneck Hill Rd.	39597727 W
	112452	785 Tiogue Ave.	37517545 W
-Mart Stores, Inc.	115603	1173 Tiogue Ave.	31988583A W
-Mart Stores, Inc.	115662	1173 Tiogue Ave.	31988583
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Total Account 108662-1420.03 - Equipment - Surveilla	3,720.50	.00*	.00*	3,720.50*	
108662-1420.04 Equipment - General	3/100.30	.00	.00	3,720.50-	
Total Account 108662-1420.04 - Equipment - General	2,100.00*	.00*	.00*	2,100.00*	
108662-1420.05 Equipment - Neters	2,200.00	.00	.00	2,100.00-	
Total Account 108662-1420.05 - Equipment - Meters	34,630.46*	.00*	.00*	34,630.46*	
108662-1430.00 Leasehold Improvements	5.7.5.5.15	.00	.00	31,030.10	
Total Account 109662-1430.00 - Leasehold Improvement	27,446.75*	.00*	.00*	27,446.75*	
108662-1440.00 Building Equipment (Fortable)		100	100	27,110.75	
Total Account 108662-1440.00 - Building Equipment (F	9,920.99*	.00*	.00*	9,920.99+	
108662-1450.00 Furniture for Project	2,244,12		,,,,	2,220.32	
Total Account 108662-1450.00 - Furniture for Project	11,083.92*	.00*	.00*	11,083.92*	
108662-1460.00 Furnishings	234243455	723/	10.0	*******	
Total Account 108662-1460.00 - Furnishings	1,787.20*	.00*	.004	1,707.204	
108662-1495.00 Reserve for Depreciation	24417 (220)		4,432	4.000.00	
Total Account 108662-1495.00 - Reserve for Depreciat	204,912.00-*	.00*	.00*	204,912.00-*	
108662-1495.01 Accum Depr Improvement				0.00	
Total Account 108662-1495.01 - Accum Depr Improvemen	65,933.01-	.00*	.00*	65,933.00-*	
108662-1495.02 Acum Depr Chlorine Pumps					
Total Account 108662-1495.02 - Acum Depr Chlorine Pu	33,703.38-*	.00*	.00*	33,703.38-+	
108662-1495.03 Accom Depr Tank					
Total Account 108662-1495.03 - Accum Depr Tank	2,220.00-	.00*	.00*	2,220.00-	
108662-1495.05 Accum Depr Furn & Fixture					
Total Account 108662-1495.05 - Accum Depr Furn & Pix	14,668.00-4	.00*	.00*	14,668,00-	
108662-1495.12 Accum Depr General Equipment					
Total Account 108662-1495.12 - Accum Depr General Eq	18,191.00-*	.00*	.00*	18,191.00-*	
108662-6516.00 Repairs & Maintenance 1-24-2008 API Mult 3689 69785 Monitoring svc.	1 (00 0 101 100	2.2			
1-24-2008 API Mult 3689 59785 Monitoring svc. 1-24-2008 API Siem 8828 69785 Bioxide 1-24-2008 API Siem 8828 69785 Bioxide	1/08-3/31/08	52.50 588.50			
1-31-2008 JE jf 33297 reclass Monitor	ing fee per bu	588.50	52.50-		
1-31-2008 JS jf 33297 reclass Dig Saf Total 1-31-08	se per budget a to 6516	2,965.00 173.00	22.22.7	5 5.0 0.5	
2-20-2008 API Siem 8828 70433 Bioxide	.004	4,367.50*	52.50-4	4,315.004	
2-20-2008 API Siem 8828 70433 Bioxide 2-20-2008 API Prem 3678 70451 Jan svc 2-20-2008 API Siem 8829 70451 Bioxide		588.50 588.50			
2-20-2008 API Siem 8829 70451 Bioxide 2-20-2008 API Siem 8829 70451 Bioxide		1,450.00 588.50			
Total 2-29-08	4,315.00*	588.50 3,804.00*	.00*	8,119.00*	
3-18-2008 API Siem 8829 71122 Bioxide WMIA 3-18-2008 API Siem 8829 71122 Bioxide WMIA		765.05			
3-24-2008 API Siem 8829 71235 Bloxide WMIA		765.05 588.50			
3-24-2008 API Siem 8829 71235 Bioxide WMIA 3-31-2008 API Siem 8829 71545 Bioxide WMIA 3-31-2008 API Siem 8829 71545 Bioxide WMIA	in Mar in error	588.50	52.50-		
3-31-2006 API Siem 8829 71545 Bioxide WMTA		588.50 588.50			
3-31-2008 API Mult 3749 71756 • Monitoring servi	8,119.00*	52.50 3,936.60*	52.50-*	12,003.104	
4-01-2008 JE jf 34387 Premium locating 4-10-2008 API Mult 3749 71756 (Rev)Monitoring 4-10-2008 API Mult 3749 71756 Monitoring servi	Inv per budge	2,900.00			
4-10-2008 'API Mult 3749 71756 (Rev)Monitoring 4-10-2008 API Mult 3749 71756 Monitoring servi	C0 SELATCO	52.50- 52.50			
4-23-2008 API Siem 8829 72048 Bioxide 4-23-2008 API Siem 8829 72048 Bioxide		589.50 588.50			

HallKeen Management Inc			0		Year-	to-date Ledger - Acc	10-07-2008 Page		
Date	Jrn	Ref	Ref	Batch	Transaction Des	Beginning Balance	Debit	Credit	Ending Balance
0662 6516	00	onn I'w		- Company Color	Continued				
1002-0310.		eparr	5 6 17	atification	e - Continued Total 4-30-08	12,003.10*	4,077.00*	.00*	16,080.10*
5-12-2008	API	Siem	8829	72506	Bioxide		588.50		
-12-2008					Bioxide		588.50 588.50		
-19-2008	API	Prem	3882	72681	Locate & mark out	AIMW	1,450.00		
5-27-2008	API	Siem	8930	72900	Bioxide		663.40		
5-27-2008	API	Siem	8830	72900	Bioxide		663.40		
5-27-2008					Bioxide		588.50		
5-27-2008	API	Siem	8830	72900	Bioxide Bioxide Bioxide Bioxide		588.50	247	
					Total 5-31-08	16,080.10*	5,130.804	.00*	21,210.90*
5-17-2008				73445	Bioxide		588.50		
5-17-2008	API			73445	Bioxida		588.50		
5-30-2008	JE	jf	200	35069	reclass Utility 1	ocat	1,450.00		
5-30-2008	API	Siem	8830	73783	Bioxide reclass Utility 1 Bioxide		588.50		
5-30-2008	API	Siem	8830	73783	Bioxide		588.50 3,804.00*	00*	25,014.90
						21,210.90*		(00-	25/024.50
7-09-2008	API	Mult	3808	73973	7/1-9/30/08 Monit	or ave pump	52.50		
7-16-2008	API	Prem	4046	74105	Locate & mark out		1,450.00		
7-21-2008	API	Siem	8830	74217	Bloxide		588.50		
-21-2008	API	Siem	8830	74217	Bioxide		588.50		
7-21-2008	API	Siem	8830	74217	Bioxide		588.50		
7-21-2009	API	Siem	8830	74217	Bioxide		588.50		
7-29-2008	API	Mejp	815	74376	Cleaned out sewer	pump station	3,940,00		
7-31-2008	JE	jŧ		35431	reclass Monitorin	g fees		52.50-	
7-31-2008	API	Siem	8830	74565	Bioxide		612.04		
7-31-2008	API	Siem	8830	74565	Bioxide	25,014.90*	589.50	52.50-*	33, 959, 44
								32,30	357555,14
8-19-2008	API	Siem	8830	74906	Bioxide-WMIA Bioxide-WMIA		588.50		
3-19-2008		Siem	8830	74906	Bioxide-WMIA		588.50		
3-31-2008	J£	jf		35475	reclass Premium M	arking fees	1,580.00		
3-31-2008	API	Siem	8830	75171	Bloxide		588.50		
3-31-2008	API	Siem	8883	75171	Bioxide	33,959.4	411.95 3,757.45*	.00*	37,716.89
					Total 8-31-08	33,959.4	3,737.43*	,00-	31,110.05
-17-2008	API	Siem	8831	75473	Bloxide		588.50		
3-17-2008	API	Siem	8831	75473	Bioxide		588.50		
9-23-2008					Locate & mark out	AIMW	1,580.00		
9-23-2008	API	Siem	8831	75628	Bioxide		588.50		
9-23-2008	API	Siem	8931	75628	Bioxide	25 25 C 25 co	588.50	***	41 550 00
						37,716.89*		.00*	41,650.89
10-06-2008	API	Mult	3869	75908	Otrly monitoring Total 10-30-08	service	52.50 52.50*	.00*	41.703.39
otal Acco	unt 1	08662-	6516	.00 - Rep	airs & Maintenance	.00*	41,860.89*	157,50-*	41,703.39
otal Prop	erty	108662	2 - W	oodland F	anor Improv Associ	2,415,195.51*	41,860.894	157.50-*	2,456,898.90

				-		
Hal'ikeen Managemen	t Inc	Year-t	o-date Ledger - Ac	crual		10-07-2008 Page 1
Date Jrn 1	Ref Ref Batch	Tennesettes Dec	Beginning	2000	45567	Ending
7.55		Transaction Das at (1-01-2007 - 12-3)	Balance	Debit	Credit	Balance
108662-1415.00 Es			-2007)			
		avation and Piping	103,000.004	204	.00*	107 000 004
108662-1420.00 Set	Wer Pump System	a la saon and tapang	103,000,00	.004	.00-	103,000.00*
3-15-2007 API :	Siem 8825 62057	install meter/ pum	p	6,018.75		
		Sewer Pump System	2,500,000.00*	6,018.75*	.00*	2,506,018.75*
108662-1420.01 Bu						
		lding Improvements	4,200.00*	.00*	.00*	4,200.00*
108662-1420.02 Equ		and it is	a anic			
108662-1420.03 Eq.		Equipment - Pumps	50, 914.32*	.00*	.00*	50,914.32
		ipment - Surveilla	3 500 1 1	440	ata	4 170 40
108662-1420.04 Equ		rpment - surveilla	3,7211,1	.004	.00*	3,720.50*
		quipment - General	2,100.00*	200	741	200000
108662-1420.05 Equ		darbuenc - peneral	2,100.00	.00*	.00*	2,100.00*
		Equipment - Meters	34,630.46*	.00*	.00*	24 622 464
108662-1430.00 Lea			34,030.40	.00	.00-	34,630.46*
		sehold Improvement	27,446.75*	.00*	.00*	27 446 764
109662-1440.00 Bul			an in its	.00	.00	27,446.75*
Total Account 108			9,920.99*	.00*	,00*	9,920.99*
108662-1450.00 Fur			0.00000	7.5	1.00	3/260133
Total Account 108	662-1450.00 - Furi	iture for Project	11,083.92*	.00*	.00*	11,083.92*
109662-1460.00 Fur					100	20,000,00
Total A	ccount 108662-1460	.00 - Furnishings	1,787.20*	.00+	.00*	1,787.20*
108662-1495.00 Res 12-31-2007 JE	erve for Deprecia AJE #17 35673				300 020 00	
Total Account 108		record Depreciation			105,177.00-	427 332 337
108662-1495.01 Acc		and the first of the state of t	99,735.00-*	-00*	105,177.00-+	204,912.00-*
	AJE #17 35673	record Depreciation	r .		1,319.00-	
Total Account 1086			64, 614.60-*	.00*	1,319.00-4	65,933.00-
108662-1495.02 Acur 12-31-2007 JE I	m Depr Chlorine Po AJE #17 35673	mps record Depreciation	in the second		4,066.00~	
Total Account 1086			29,637,38-*	.00*	4,066.00-	33,703.38-*
108662-1495.03 Acci	um Depr Tank		207.021.120	.00	4,000.00	33,703,302
	AJE #17 35673	record Depreciation			97.00-	
	nt 108662-1495.03		2,123.00-	.00*	97.00-*	2,220.00-*
108662-1495.05 Acci						
Total Account 1086			14,668.00-*	.00*	.00*	14,668.00-*
108662-1495.12 Acct 12-31-2007 JE A	M Depr General Eq NJE #17 35673	uipment record Depreciation			4,947.00-	7
Total Account 1086	62-1495.12 - Accu	m Depr General Eq	13,244.00-+	.00*	4,947.00-	18,191.00-
108662-6516.00 Repa 1-31-2007 JE				disco-si		
1-31-2007 08	j£ 29065	reclass chem treatm Total 1-31-07	*00.	1,177.00	.00+	1,177.00*
2-20-2007 API Pr	em B262 61332	Locating Utilities Total 2-28-07	1 177 004	1,450.00	200	
3-15-2007 API Pr	rem 8265 62057	locate & mark out s	1,177.00*	1,450.00*	.00*	2,627.00+
3-15-2007 API Pr 3-15-2007 API Si 3-20-2007 API Si	em 8825 62057	500 gal Bioxide Bioxide	ewet 2/01	1,450.00		
3-20-2007 API SI	em 8825 62933	Bioxide Total 3-31-07	2,627.1*	588.50 588.50 3,804.00*	.00*	£ 431 00#
4-18-2007 API PO	we 2377 62933	Generator rental 10		6,959.90	.00-	6,431.00*
4-30-2007 API Si 4-30-2007 API Si	em 8825 63373 em 8025 63373	Bioxide Bioxide		588.50 588.50		
4-30-2007 API Si	em 8825 63373 em 8825 63373	Bioxide Bioxide		223.63 580.50		
4.72.224		Total 4-30-07	6,431.00*	8,949.03*	.00*	15,380.034
5-31-2007 JE	jf 30718	reclass to R & M Total 5-31-07	15,380.03*	1,450.00	.00*	16,830.034
	em 8826 64274	Bioxide	n. · bed. cd	588.50		-21 222.00
6-06-2007 API Si	em 8826 64274	Bioxide		588.50		

									10-07-2008 Page
Date 3	Irn	Ref	Ref	Batch	Transaction Dea	Beginning Balance	Debit	Credit	Ending Balance
08662-6516.00). R	epalr	s & M	aintenan	ce - Continued				
6-06-2007 P 6-06-2007 P	MPI.	SLem	8826	64274	Bioxide		588.50		
0-00-2007 P	Te.	STEM	6826	692/9	Bioxide	. 22 'esla (a.)	588.50	100	
					Total 6-30-07	16,830.0.3	2,354.00*	*00*	19,184.03*
7-16-2007 A	PI	Siem	8826	65089	Bioxide		588.50		
7-16-2007 A	PI		8826	65089	Bioxide		EOD EO		
7-31-2007 J	8	jf		31207	reclass repairs	to 6516	14,719.27		
					Total 7-31-07	19,184.03*	15,896.27*	.00*	35,080.30*
8-09-2007 A	PI	Stem	8826	65733	Bioxide				01.400,032.50
8-09-2007 A	PI	Siem	8826	65733	Pinylda		588,50 588,50		
					Total 8-31-07	35,080.30*	1,177.00*	004	25 055 001
0_11.2007 *	DT	~1 +	000-	*****		55,000.50	1,177.00	.00*	36,257.30*
9-11-2007 A 9-11-2007 A	DT.	Siem	8827	66484 66484	bioxide		470.80		
9-11-2007 A	DI	Siem	0027	66484	bioxide		470.80		
5-11-5001 W	61	216W	0821	66484	bioxide	100000000000000000000000000000000000000	941.60		
					Total 9-30-07	36, 257.30*	1,883.20*	.00*	38,140.50*
10-22-2007 A	PI	Powe	2543	67408	maint agreement	2/07-12/08	265.00		
10-22-2007 A	δI	Prem	3397	67408	locate m/o avc 9	30/07	1,450.00		
10-22-2007 A	PI	Siem	8827	67408	Dioxide	1.00	588.50		
0-22-2007 A 0-31-2007 A	14	Siem	8827	67408	bioxíde		588,50		
10-31-2007 A	DT.	Nacı	1991	67690	Quarterly insp Ar	nual	150.00		
0-31-2007 A	Dr	Stom	8227	67690	Bioxide Bioxide		588.50		
10-31-2007 A	Pr	Siem	8827	67690	Bioxide		588.50		
10-31-2007 A	PI	Siem	8827	67690	Bioxide		580.50		
			7720	0,020	Total 10-31-07	38,140.50*	588.50 5,396.00*	200	22,312,511
1 12 2007 1				45753	100	30/140.30	3,396.00	.00*	43,536.50*
1-12-2007 A	21	Siem	8828	67975	Bioxide		588,50		
1-19-2007 A	71	Dine	6451	60171	Bioxide		588.50		
1-14-2007 AT	37	Dinn	CCCC	60171	SEWER SEWER		527.30		
1~26~2007 A	21	Siem	8828	68256	Bioxide		1,273.75		
1-26-2007 AL	I	Siem	8828	68256	Bioxide		508.50		
				52504	Total 11-30-07	43,536,50+	588.50 4,155.05*	204	
2 21 2007		25		272.04		45,530.5	4,155.05	.00*	47,691.55*
2-31-2007 AF 2-31-2007 AF	'I	Siem	8828	69246	BIOXIDE		588.50		
2-31-2007 AF	1	Siem	8828	69246	BIOXIDE		588.50		
2-31-2007 A	7	wood !	1 100	69246	Repair Pence at S	ewer Station	587.00		
2-31-2007 AF	T	Stem	0020	60554	Bioxide		589.50		
x 01 1007 710		Diem	0020	09334	Bioxide Total 12-31-07	10 111 122 122 1	588.50		
						120 8 2 2 2 2 2 2 2 2	2,941.00*	.00*	50,632.55*
Total Account 108662-6516.00 - Repairs & Maintenance						-00*	50,632.55*	.00*	50,632.55*
otal Propert	y 10	08662	- Woo	dland M	anor Improv Associ	2,524,782.76*	56,651.30*	115,606.00-*	2,465,828.06*
ND TOTALS						2,524,782.76*	56,651.30*	115,606.00-*	2,465,828.06*

Hall-Keen Management Inc	Year	-to-date Ledger -	Accrual		10-07-2008 Page 1
		Beginning	Accidat		Ending
Date Jrn Ref Ref Batch	Transaction Des	Balance	Debit	Credit	Balance
108662 Woodland Manor Improv Associa		31-2006)			
108662-1415.00 Escavation and Piping			G.V.		Name and San
Total Account 108662-1415.00 - Esca 108662-1420.00 Sewer Pump System	vation and Piping	103,000.00*	.004	.00*	103,000.00*
1-26-2006 JE jf 25267 1-31-2006 JE jf 25288	Record Sewer lin record Note Paybl Total 1-31-06	Prom Note CSA te to CSA 2,500,000.00*	2,500,000.00 4,520,000.00 7,020,000.00*	.00*	2,500,000.00* 11
12-31-2006 JE AJE 8 31919	record Conting no Total 12-31-06	ote CSA 2,512,037.50*		4,520,000.00-	2 222 22 22 1
Total Account 108662-1420.00 -	and the second second second second	2,500,000.00*	7,020,000.00*	4,520,000.00-4	2,007,962.50-4
108662-1420.01 Building Improvements	The state of the s	2,300,000.00	7,020,000.00-	9,520,000,00-	2,007,962.50-*!!
Total Account 108662-1420.01 - Buil		4,200.00*	.004	.00*	4,200.00*
108662-1420.02 Equipment - Pumps 1-27-2006 APX fgle 1017 52646 1-31-2006 JE jf 25256	Plumbing avc Rec Pick-up & re	To a late to the same of	9,916.76	199	7,500
Total Account 108662-1420.02 -		50,914.32*	13,390.40 23,307.16*	.00*	50,914.32* 11
108662-1420.03 Equipment - Surveilla		30,521102	25,507.10	.00	30,314.32-11
Total Account 108662-1420.03 - Equi		3,720.50*	.00*	.00*	3,720,504
108662-1420.04 Equipment - General		51.353.351	734		7,120,20
Total Account 108662-1420.04 - Eq	ipment - General	2,100.00+	.00+	.00*	2,100.00*
108662-1420.05 Equipment - Meters					
Total Account 108662-1420.05 - Ed	quipment - Meters	34,630.46*	.00*	.00*	34,630.46*
108662-1430.00 Leasehold Improvement 2-01-2006 JE jf 25256 2-09-2006 API FGLe 1082 51471 2-09-2006 API FGLe 1091 51471	Rev Pick-up & re pick-up reassembl ck valve , rebuil	e pipe	4,980.76 8,409.64	13,390.40-	
Total Account 108662-1430.00 - Lease		27,446.75*	13,390.40*	13,390.40-*	27,446.75*
108662-1440.00 Building Equipment (Po		277110110	107000110	23/330.30	21,140.75
Total Account 188662-1440.00 - Build	ling Equipment (P	9,920.99*	.00*	.00*	9,920.99*
108662-1450.00 Furniture for Project					120114020
Total Account 108662-1450.00 - Furni 108662-1460.00 Furnishings	ture for Project	11,083.92*	.00*	.00*	11,083.92*
Total Account 108662-1460.	00 - Furnishings	1,787.20+	.00*	.00*	1,787.20*
108662-1495.00 Reserve for Depreciat	ion				0.000.00
Total Account 108662-1495.00 - Reser	ve for Depreciat	99,735.00-	.00+	.00*	99,735.00-4
108662-1495.01 Accum Depr Improvement 12-31-2006 JE AJE 7 31919				41 141 41	
12-31-2006 JE AJE 7 31919 Total Account 108662-1495.01 - Account	Depreciation	C4 C11 00 4		53,402.00-	no sives a
108662-1495.02 Acum Depr Chlorine Pun	College of Section (College)	64,614.00-*	.00*	53,402.00-*	118,016.00-#
12-31-2006 JE AJE 7 31919	Depreciation			2,402.00-	
Total Account 108662-1495.02 - Acum	Depr Chlorine Pu	29,637.38-*	.00*	2,402.00-*	32,039.38-*
108662-1495.03 Accum Depr Tank 12-31-2006 JE AJE 7 31919	Depreciation		141	97.00-	
Total Account 108662-1495.03 -		2,123.00-*	.08*	97.00-*	2,220.00-+
108662-1495.05 Accum Depr Furn & Flat					00,000133
12-31-2006 JE AJE 7 31919	Depreciation	10 11 11 11	7.5	4,872.00-	SE-600 FE 7
Total Account 108662-1495.05 - Accum 108662-1495.12 Accum Depr General Equ		14,668.00-4	*00	4,872.00-*	19,540.00-
12-31-2006 JE AJE 7 31919	Depreciation			4,947.00~	
Total Account 108662-1495.12 - Accum	Depr General Eq	13,244.00-*	.00*	4,947.80-	18,191.00-4
108662-6516.00 Repairs & Maintenance 2-09-2006 API EGLe 8792 51471 2-09-2006 API EGLe 9644 51471 2-09-2006 API EGLe 1067 51471 2-09-2006 API EGLe 8792 51471 2-09-2006 API EGLe 9644 51471 2-09-2006 API EGLe 9644 51471 2-09-2006 API EGLe 1067 51471	svc wet well pump repair sump pump repair sump pump (Rev)svc wet well (Rev)repair sump p (Rev)repair sump p Total 2-28-06	quiuq	1,902.07 541.56 402.16 1,902.07- 541.56- 402.16- .00*	.00+	20,412.684
7-25-2006 API Mann 1468 56088 7-31-2006 API FGLe 1195 56385 7-31-2006 API FGLe 1211 56385 7-31-2006 API Sani 3147 56385 7-31-2006 API FGLe 1195 56385 7-31-2006 API FGLe 1195 56385	pump station chlor repair ck valves p wet well at pump s bleach & chlorine (Rev)repair ck val repair ck valves p	ool house tation ves pool hou	667.00 910.00 1,838.00 312.37 910.00- 910.00		

HallKeen Management Inc					Year-to-date Ledger - Accryal				10-07-2008 Page 2	
Date	Jrn	Ref	Ref	Batch	Transaction Des	Beginning Balance	Debit	Credit	Ending Balance	
108662-6516.	00 I	Repair	3 6 M	aintenan	ce - Continued					
					Total 7-31-06	71,045.231	3,727.37*	,00*	109,185.73* !!	
8-17-2006 8-31-2006	API			56788 57092	request and member chem for pump stat Total 8-31-06		178.00 667.00 845.00*	.00*	150,994.12* !!	
9-21-2006 9-21-2006 9-21-2006 9-21-2006	API API API API	FG1e Powe	1227 6516	57709 57709 57709 57709	replace solenoid chlorine system emrgency generator mercury for pump a Total 9-30-06		677.86 610.00 922.34 266.43 2,476.634	.00*	150,994,12* 11	
10-19-2006 10-31-2006 10-31-2006 10-31-2006	API	Powe	2331	58401 58884 58884 58884	service pump generator rental repair generator sanitary sewer/ pu Total 10-31-06	ump station 150,994.12*	807.50 6,892.00 1,069.60 1,850.00 10,619.10*	.00*	161,613.22*	
11-15-2006 11-15-2006		RHod		59085 59085	replace curcuit br Total 11-30-06	ck-emergency reaker 161,613.22*	960.00 475.58 1,435.58*	.00*	163,048.00*	
12-11-2006 12-31-2006		Mann j£	1567	59591 29194	chlorine Reclass Station Su Total 12-31-06	pplies to 65 163,048.80*	667.00 642.00 1,309.00*	.004	164,357.80*	
Total Accor	unt 1	08662-	-6516.	00 - Rep	pairs & Maintenance	20,412.68*	20,412.68*	.00*	164,357.80* !!	
Total Prope	arty	108662	- We	odland N	Manor Improv Associ	2,545,195.44*	7,077,110.24*	4,599,110.40-*	1,884,541.94-4	
GRAND TOTALS						2,545,195.44*	7,077,110.24*	4,599,110.40-+	1,864,541.94-+	

			Section 2			Charges			Credits			Net Change	Tenant
Unit	Type	Stat	Market	Name	Entity		Code	Amount		Code	Amount	In Balance	Balance
	024	0		Cana		==		*****	==				*******
44	120	U	01.07		508662	CA	UTIL	81.67				81.67	332,6
001	001	O	113.13	Borelli's Bakery		CA	UTIL	113.13				113.13	0.0
002	002	0	506.25	Boston Neck Realty		CA	UTIL	506.25				506.25	2422.5
003	003	0	212.50	Coventry Credit Union		CA	UTIL	212.50				212.50	325.0
004	004	0	62.50	CVS, Site #00621-01		CA	UTIL	62.50				62.50	-337.5
005	005	0	113.75	Drake Petroleum Co., Inc.		CA	UTIL	113.75				113.75	113.7
-006	006	V	0.00	Vacant Unit		CA	UTIL	0.00	PT	VAC	0.00	0.00	0.0
007	007	0	8130.63	Haven Health Center		CA	UTIL	8130.63				8130.63	-2688.8
800	800	0	690.17	Leisure Village		CA	UTIL	690.17				690.17	-695.6
009	009	D	5118.88	Springfield Armoury, LLC		CA	UTIL	5118.88				5118.88	0.0
010	010	0	520.19	Star Brite Car Wash		CA	UTIL	520.19				520.19	7615.7
011	011	0	1243.13	Star Brite Laundromat		CA	UTIL	1243.13				1243.13	7154.1
012	012	0	338,79	Father Paul R. Grenon		CA	UTIL	338.79				338.79	5396.
013	013	0	1100.63	Stop & Shop Supermarket Co		CA	UTIL	1100.63				1100.53	3060.6
014	014	0	262.50	Taco Bell Corp. #5261		CA	UTIL	262.50				262.50	262.
015	015	0	212.50	Tioque Avenue Assoc.		CA	UTIL	212.50				212.50	-6575.0
016	016	0	75.00	Fiogue Veterinary Clinic		CA	UTIL	75.00				75.00	-156.2
017	017	0	239.38	Fom's Fruit & Deli		CA	UTIL	239.38				239.38	314.5
018	018	0	112.50 t	J.S. Postal Office		CA	UTIL	112.50				112.50	568.7
019 (019	0	718.75	Wal-Mart Stores, Inc. #228		CA	UTIL	718.75				718.75	-223.3
020 (020	0	2555.72 W	Westwood Estates		CA	UTIL	2555.72				2555.72	-939.7
021 (021	0	290.63 V	hs Realty		CA	UTIL	290.63				290.63	5418.8
022 (022	v	0.00 V	acant Unit		CA	UTIL	0.00	PT	VAC	0.00	0.00	0.0
023 0	123	0	23.13	Coventry Primary Care Asso		CA	UTIL	23.13				23.13	-391.

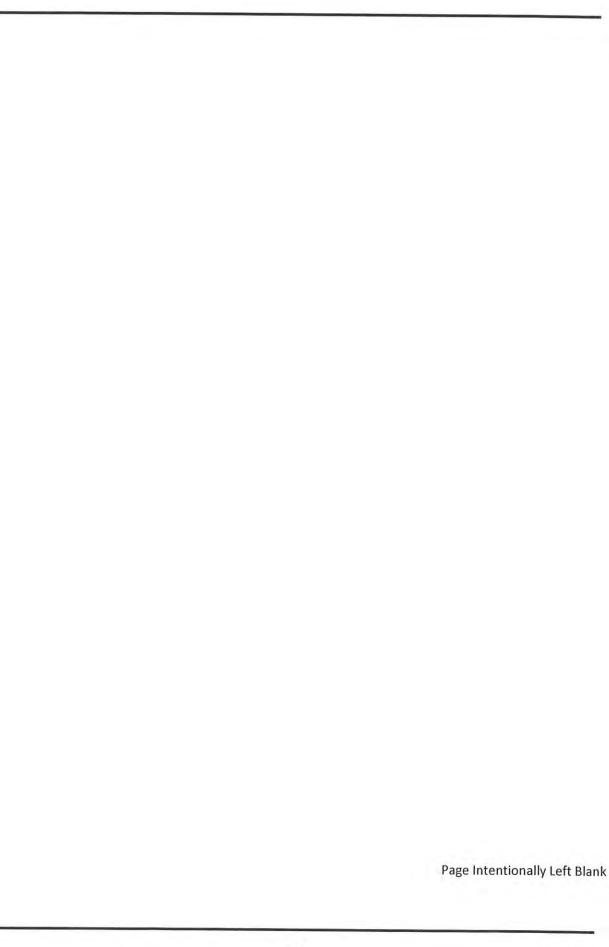
1	0	1	0	8/	2008	
	7	:	4	5	am	

HALLKEEN MANAGEMENT Woodland Manor Improvement Rent Roll As Of 8 Oct 2008

Page 2

ID 3.6.6

							Cha	rges		Cre	dits	Net Change	Tenant
Unit	Type	Stat	Market	Name	Entity		Code	Amount		Code	Amount	In Balance	Balance
-==##	****	men e		******************	A0000000	E.	****	********	==				
		-85 B	*******						==		B4======		
			22722.33					22722.33			0.00	22722.33	20978.44
×====										***		********	=========
						Ch	JTIL	22722.33	PT	VAC	0.00		
				=======================================		5.5			==		A		=========
Cotal	Market	Rent	\$ 22,722	.33 - Gain/Loss To Lease	: \$ 0.00	Net	Rent:	\$ 22,722.3	3				



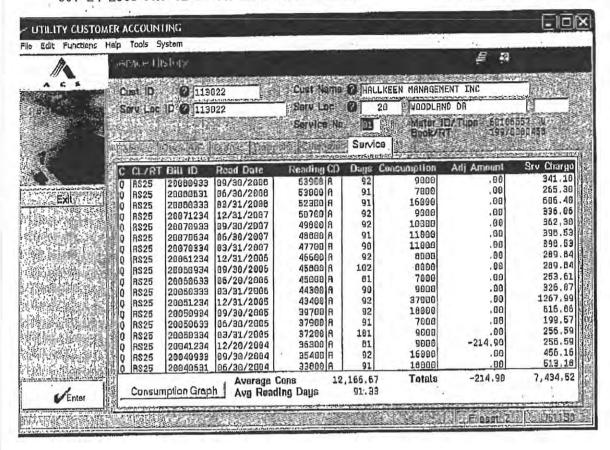
130 APPENDIX K

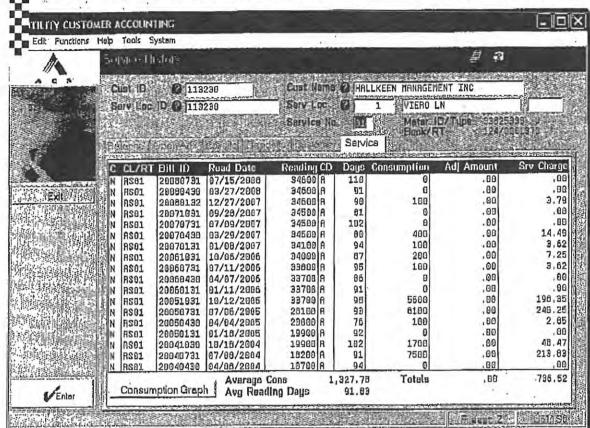
4.2 KCWA Water Flow Readings

131 APPENDIX K

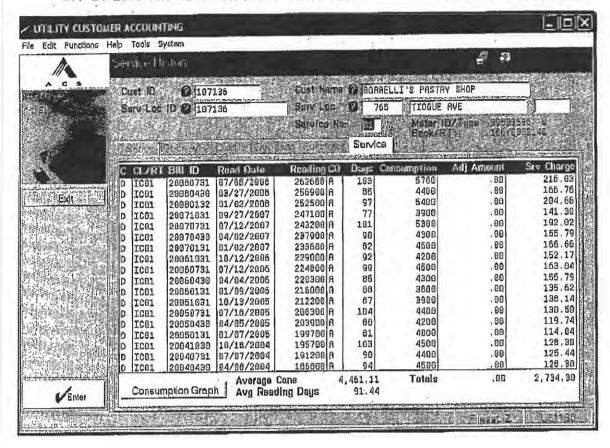


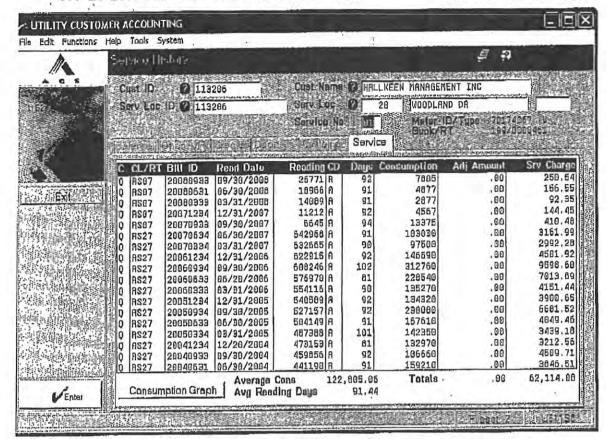
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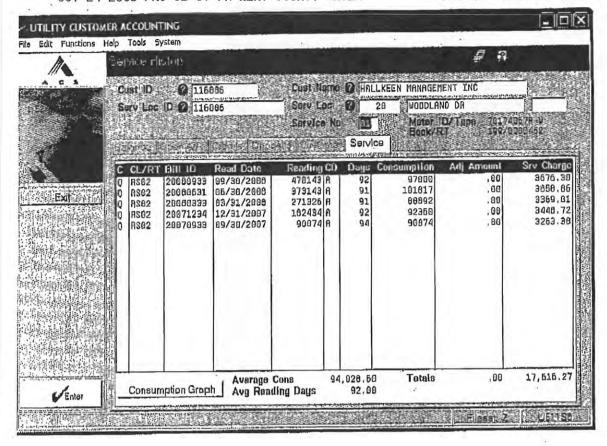


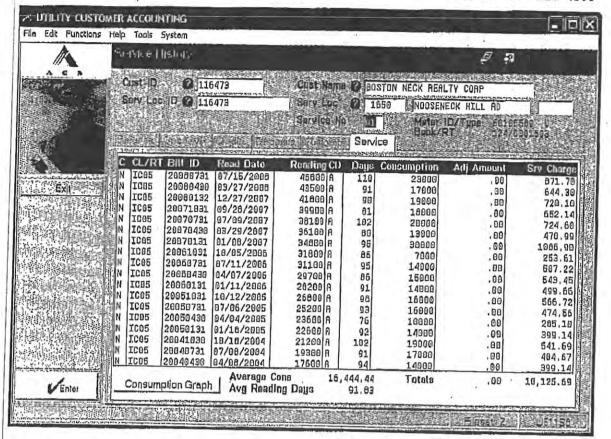


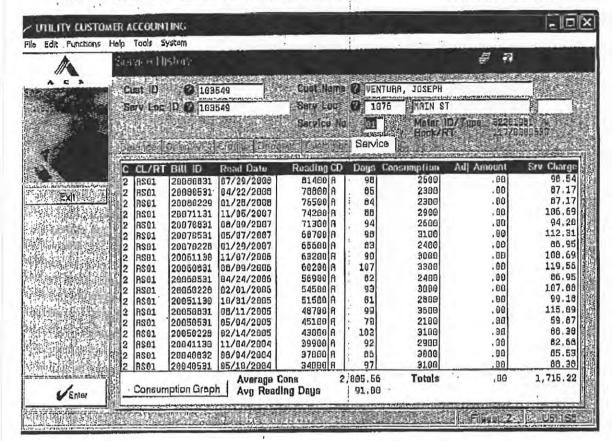
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Brandon Rages
Well-Goole

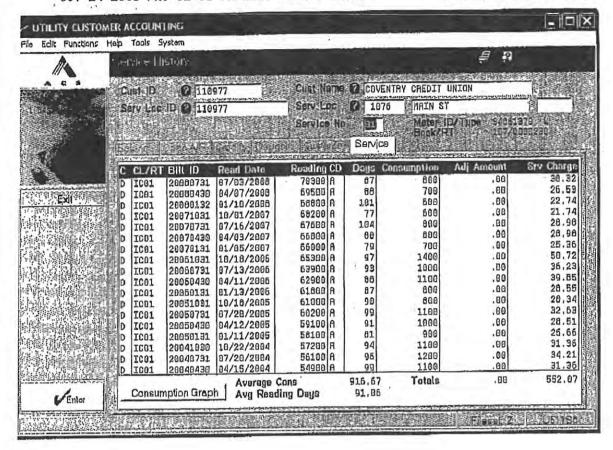


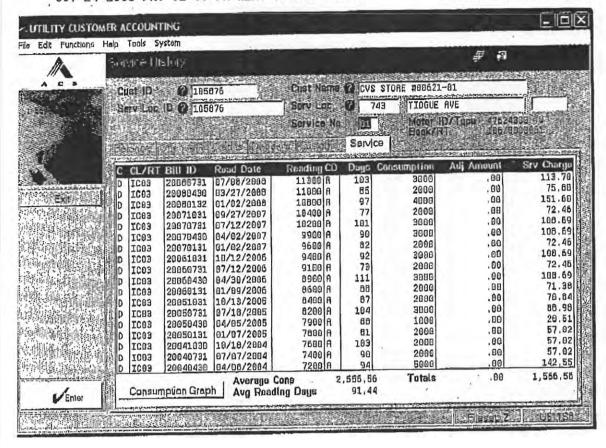


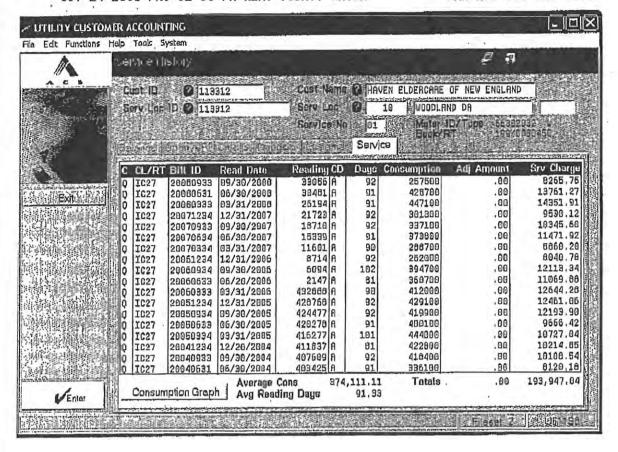


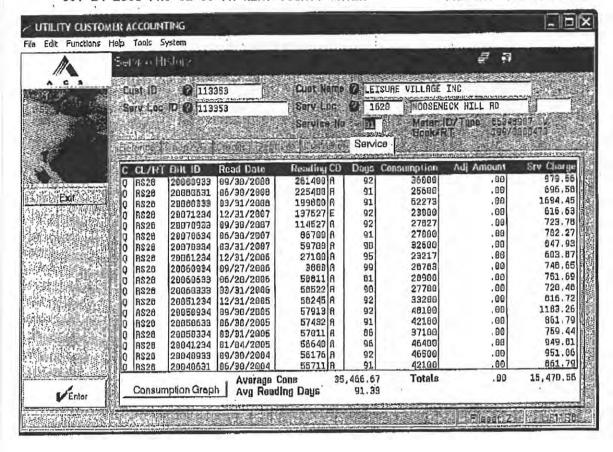


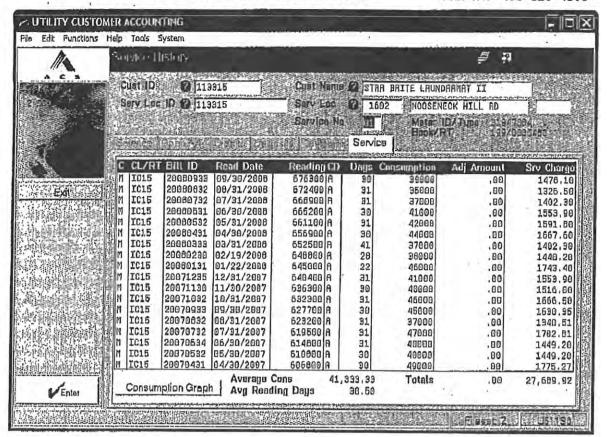


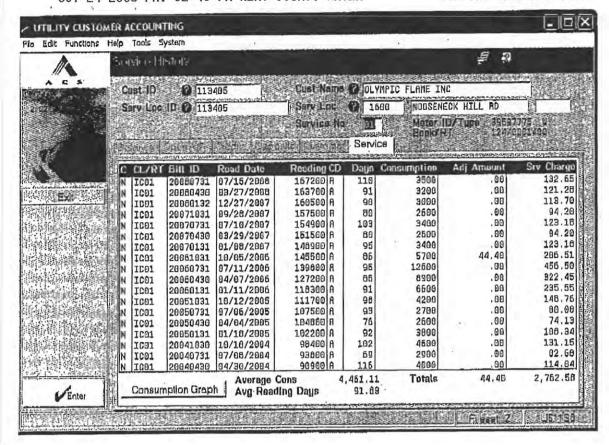


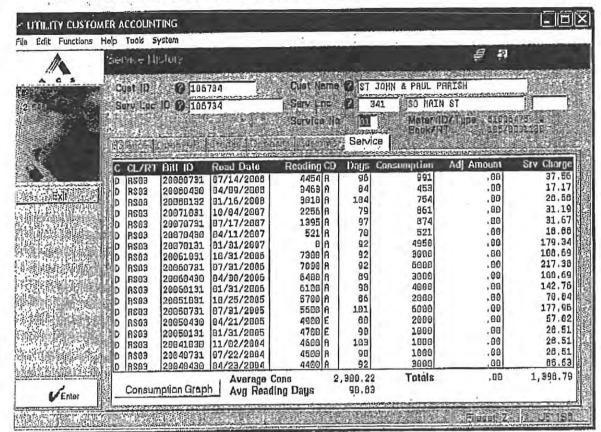




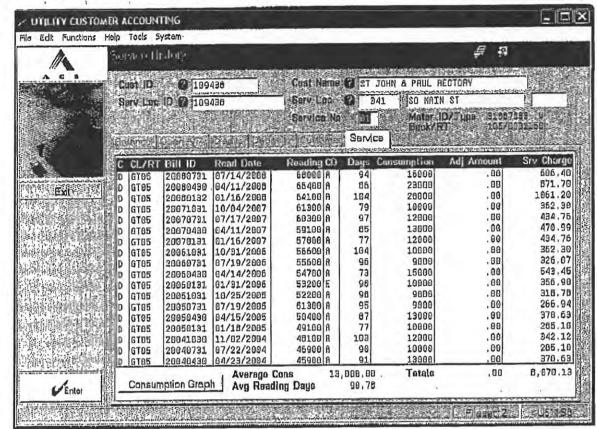




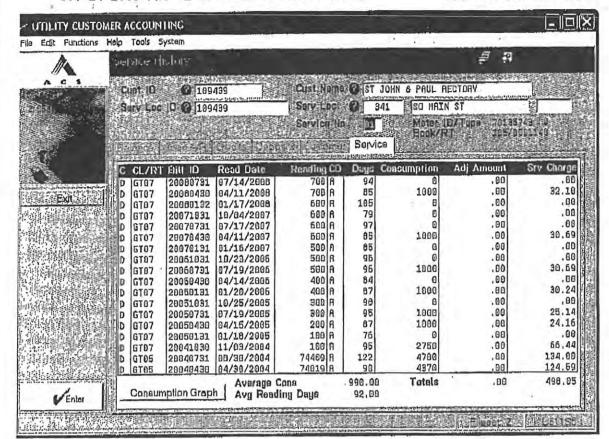




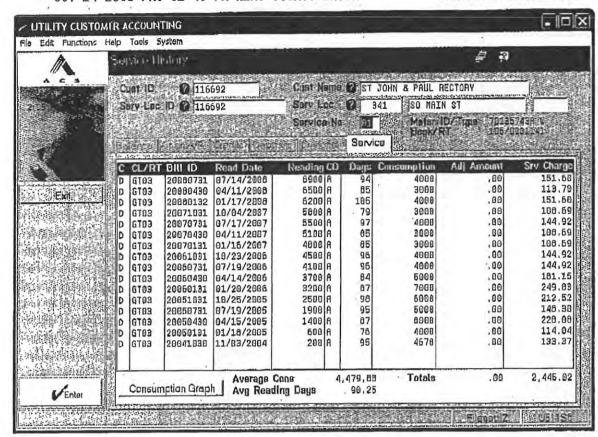
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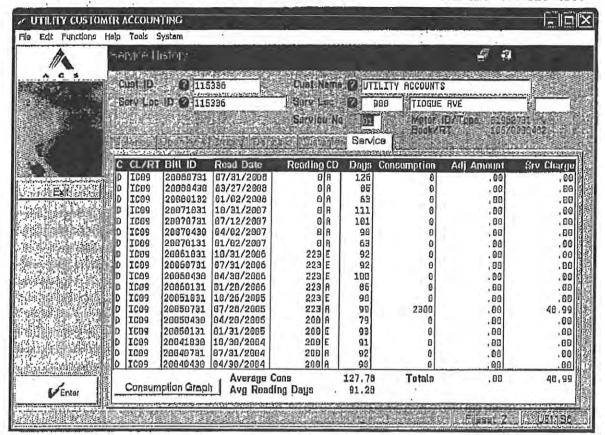
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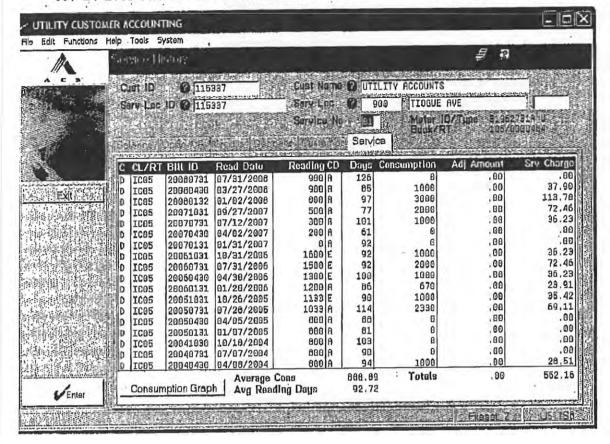


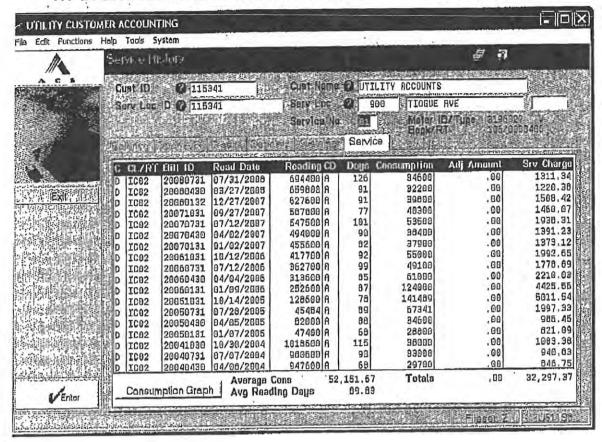
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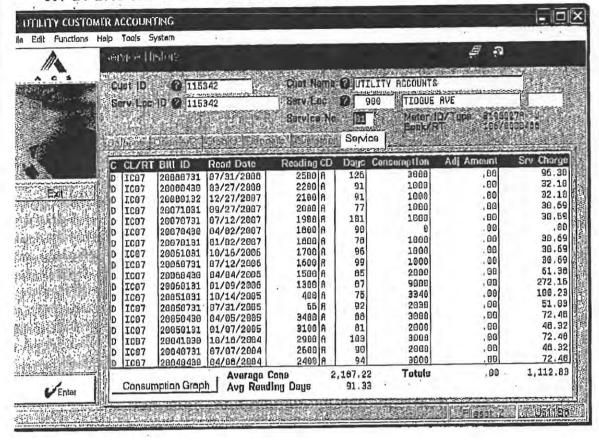


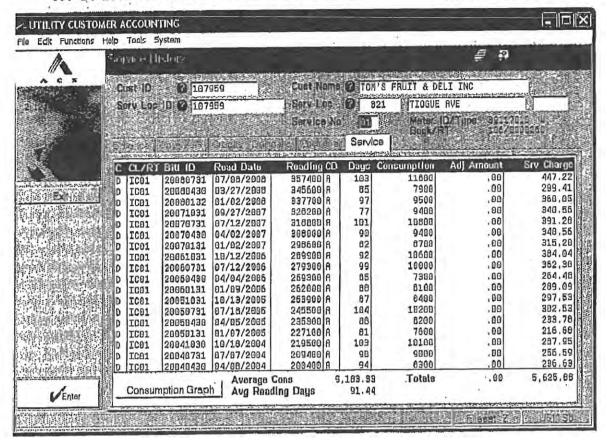
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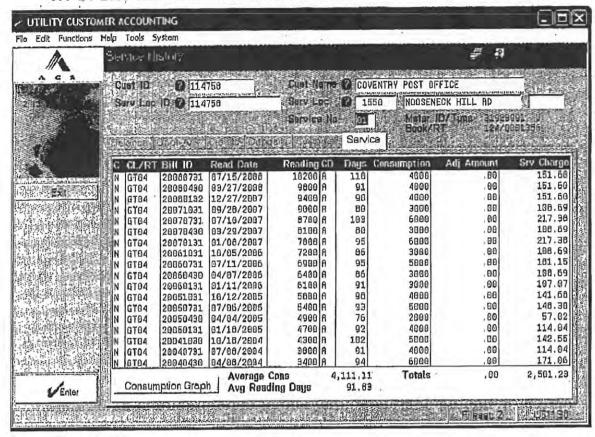


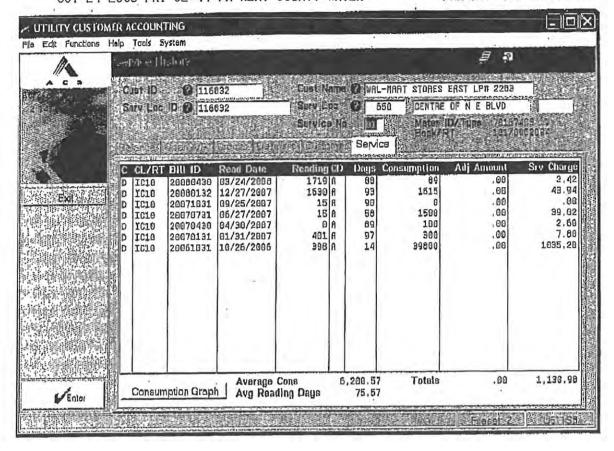


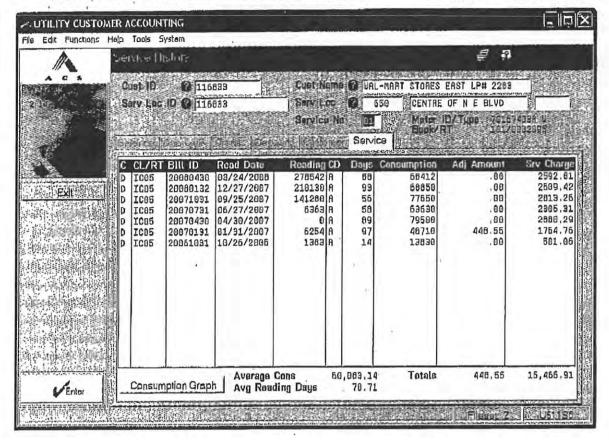


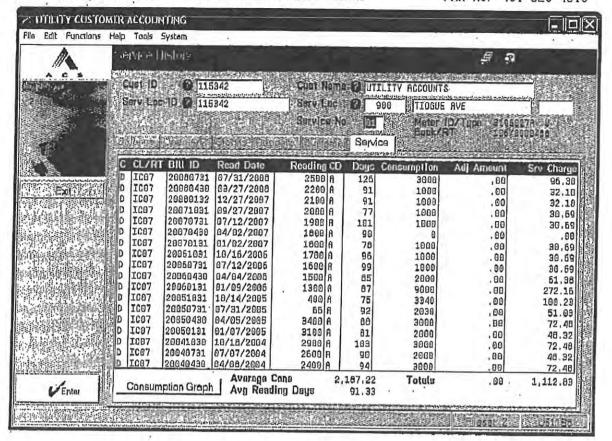


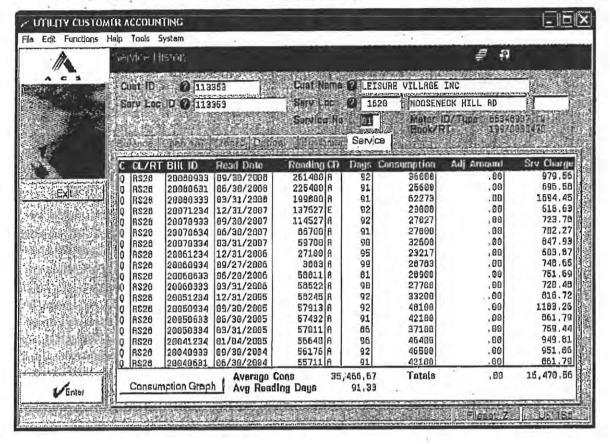


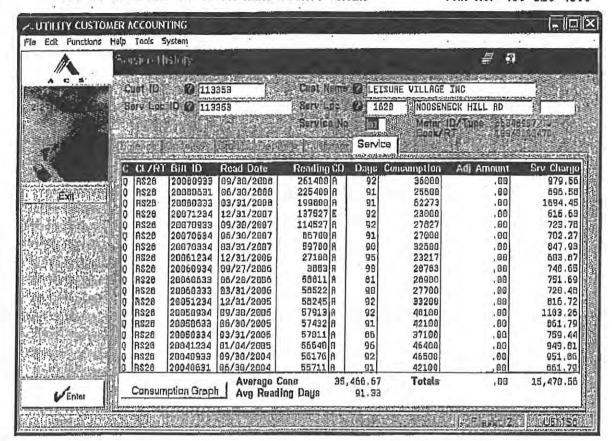


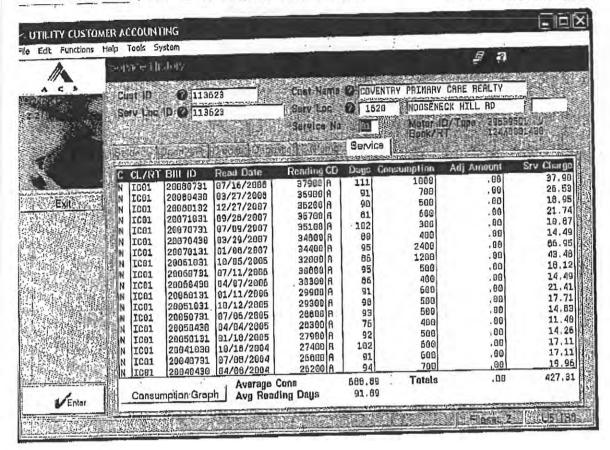


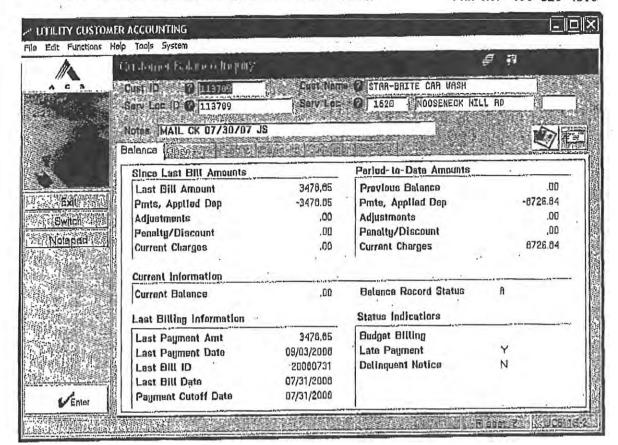


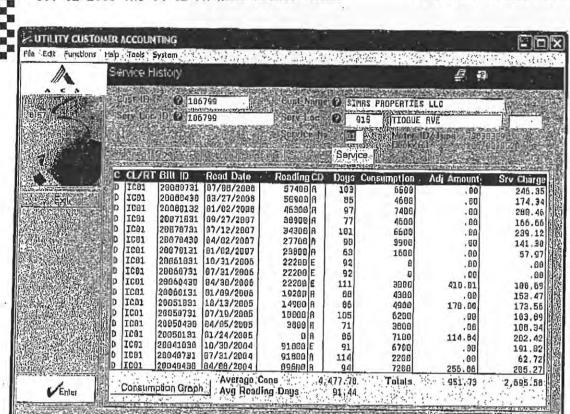


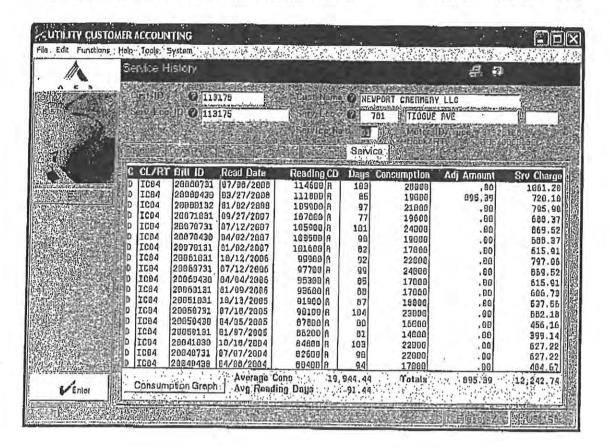


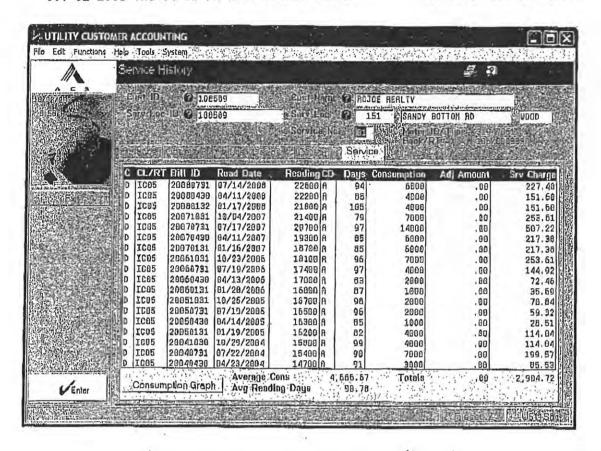


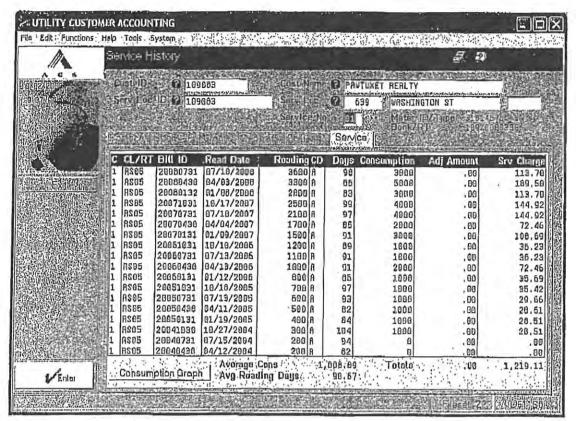


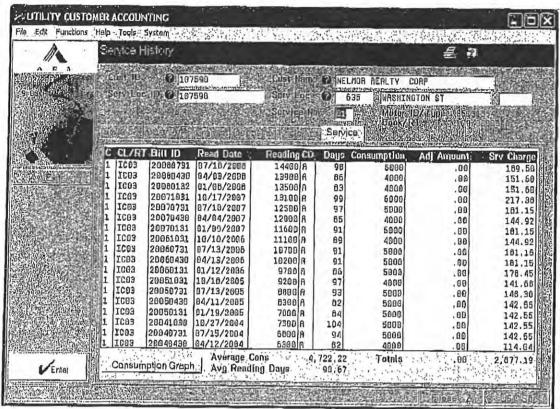


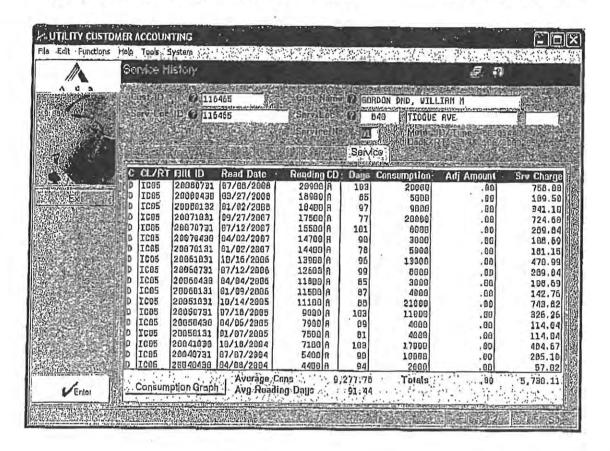


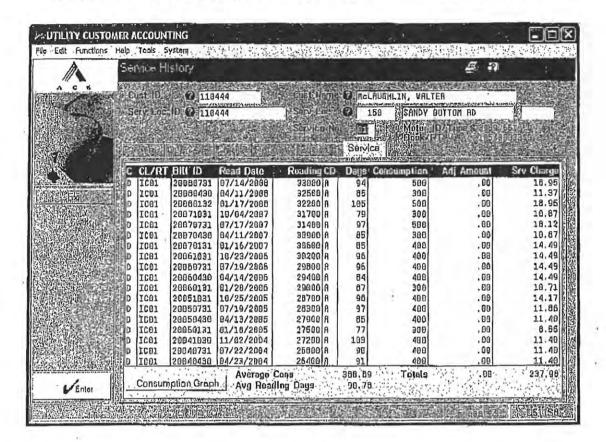


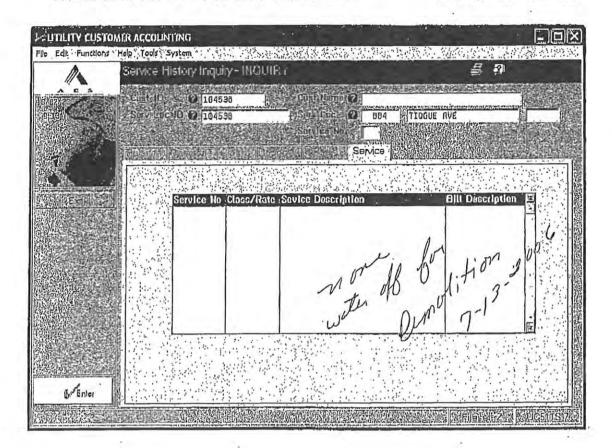


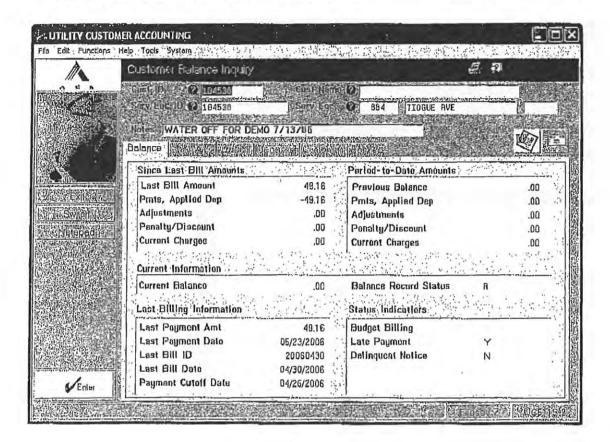


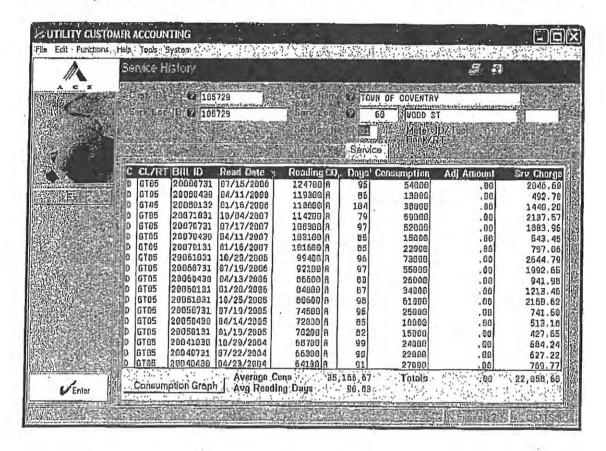


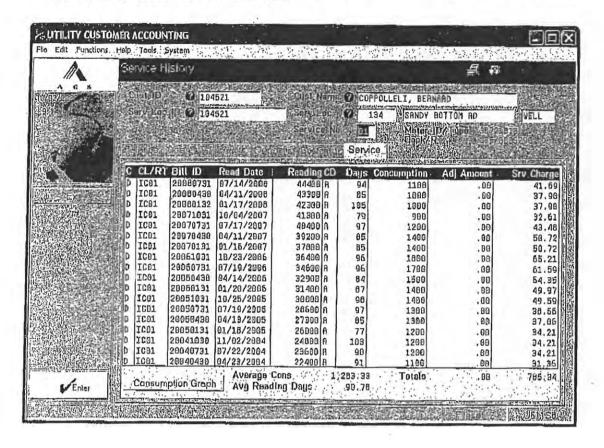


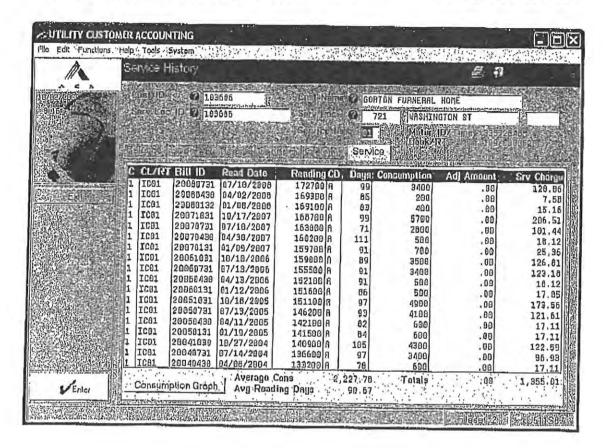


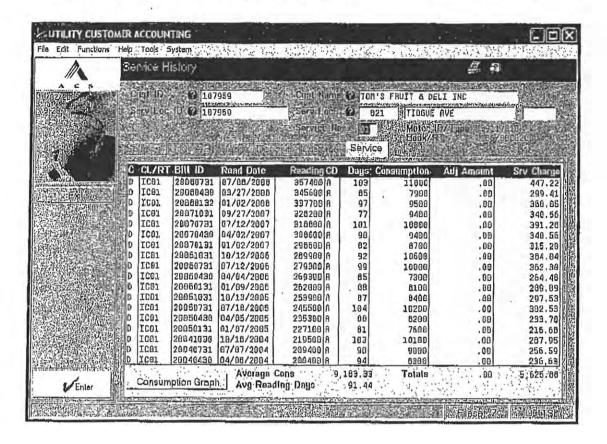


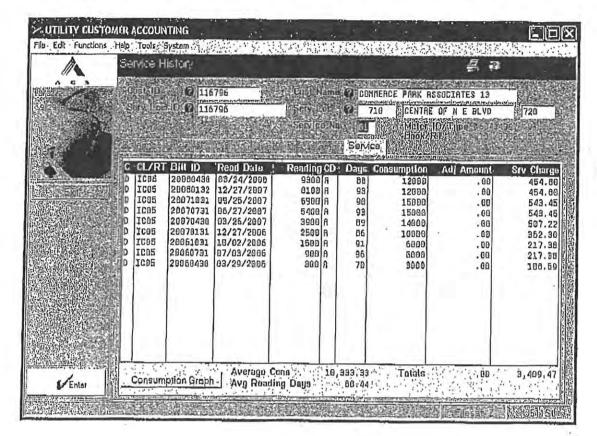


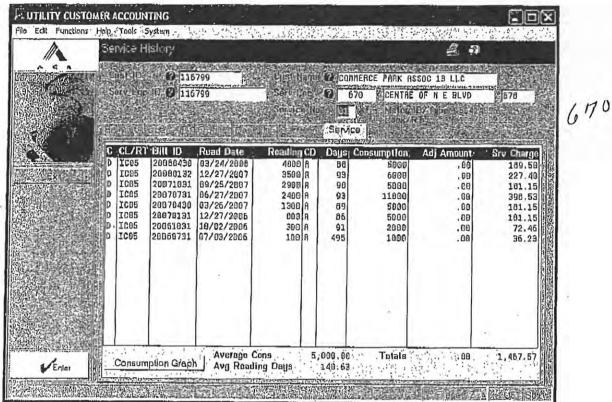


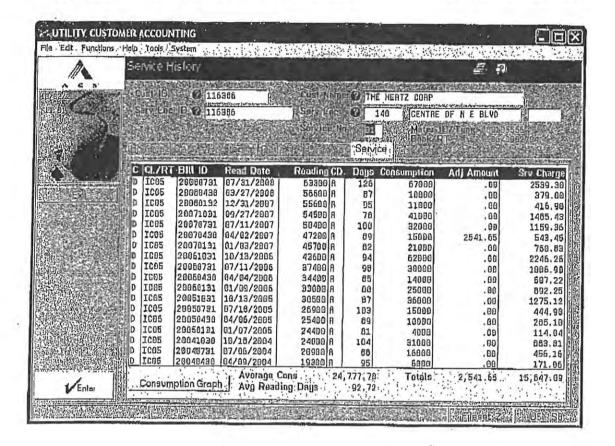


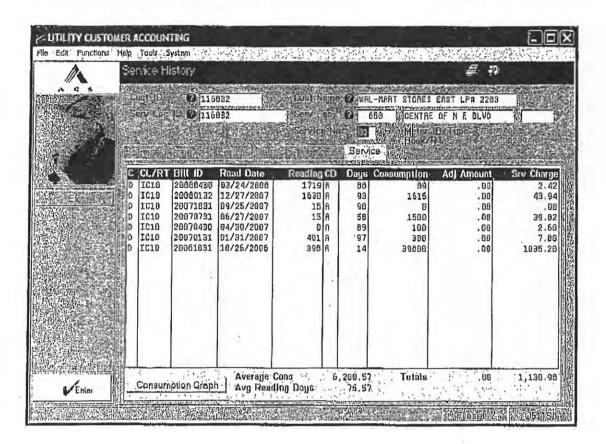


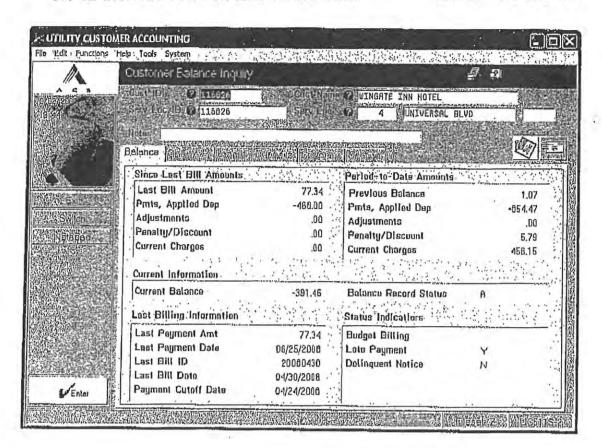


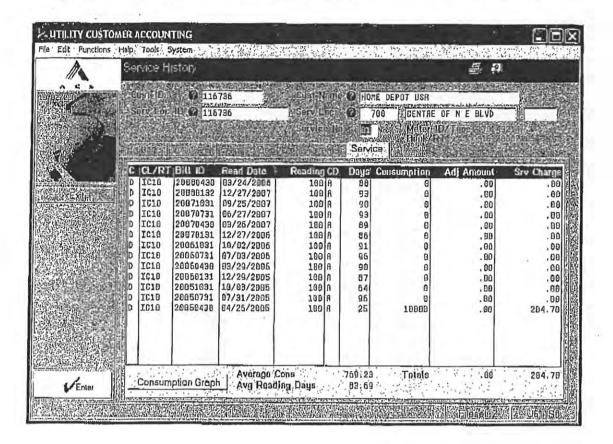


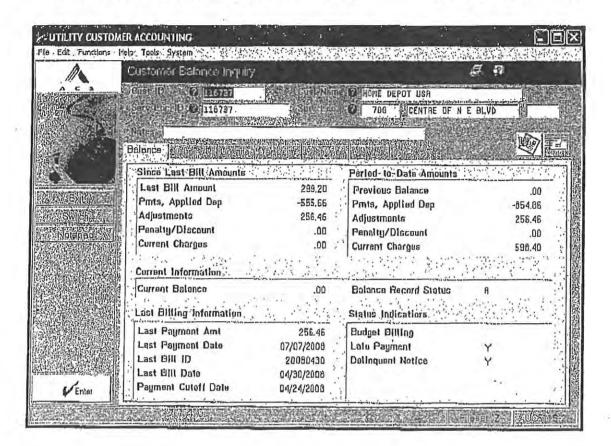


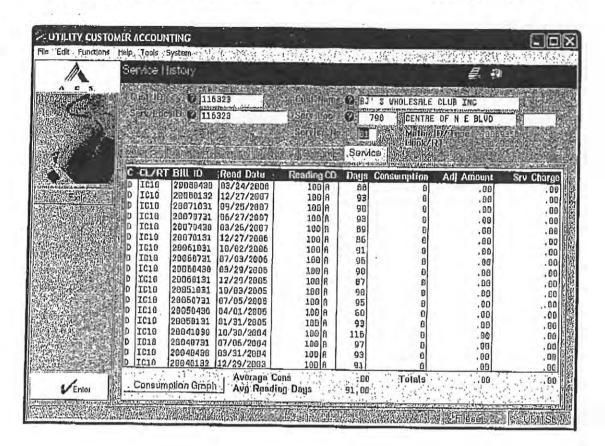


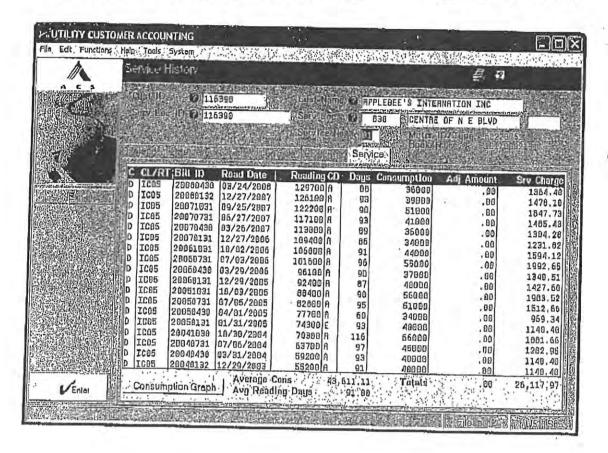


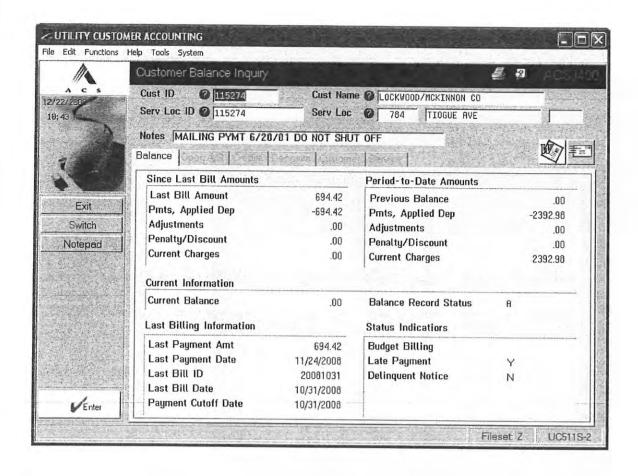


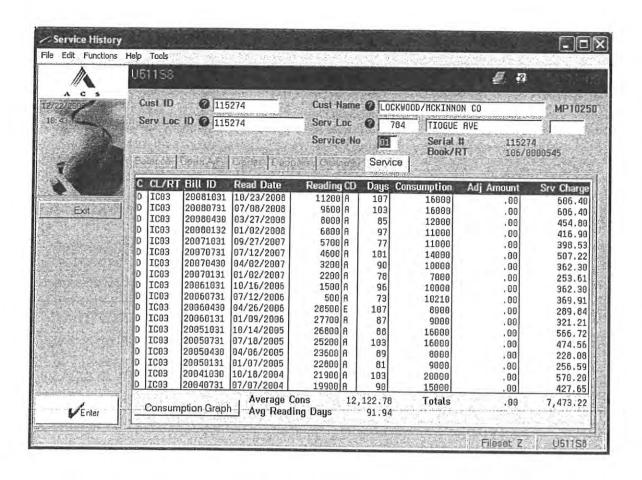


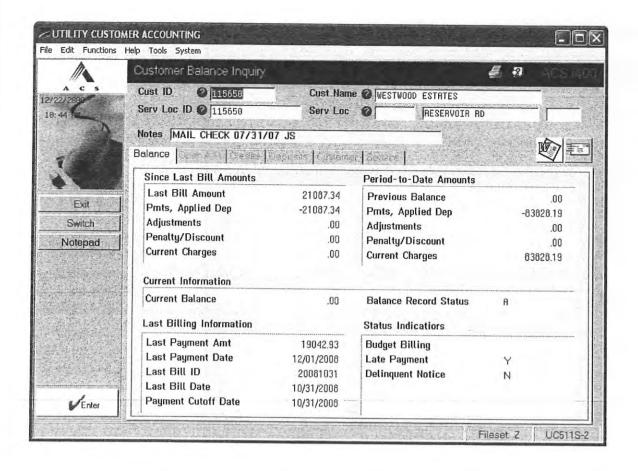


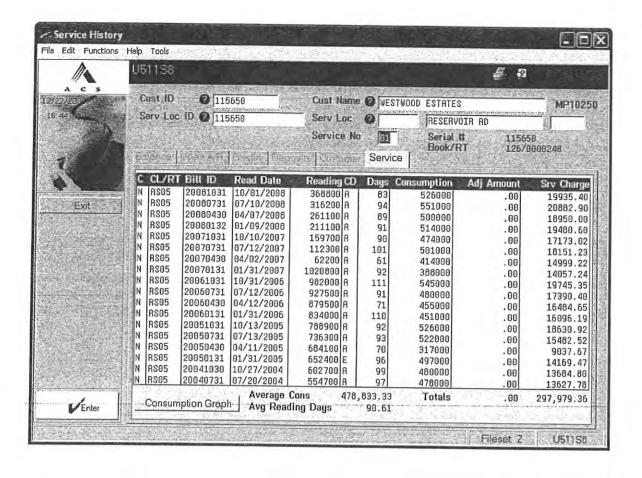


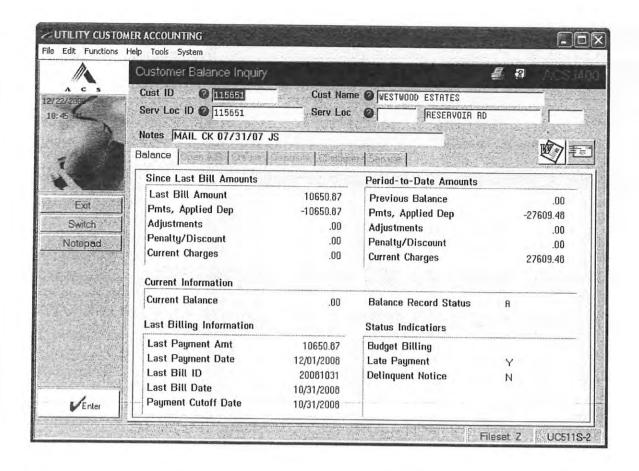


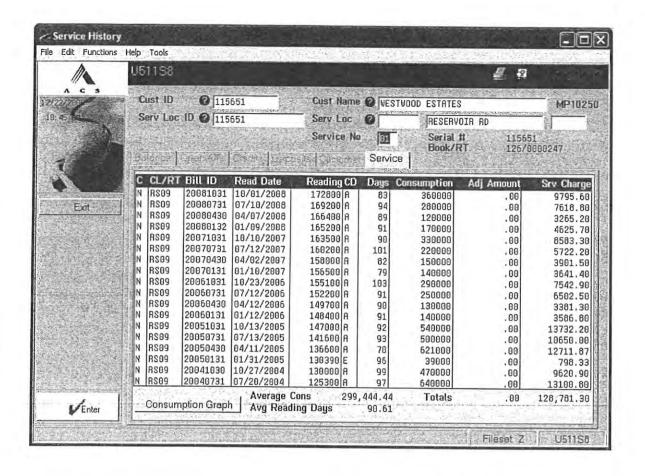


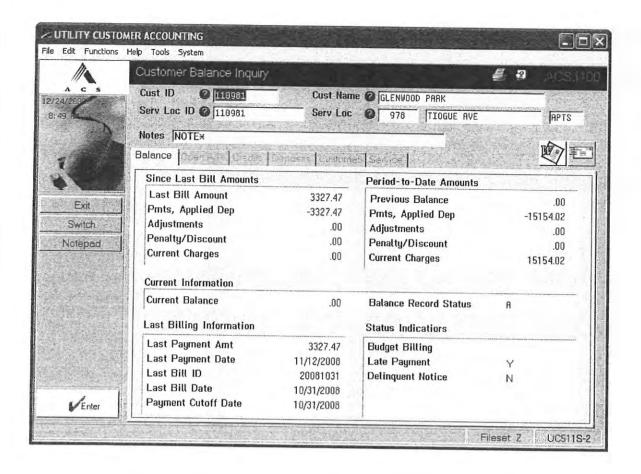


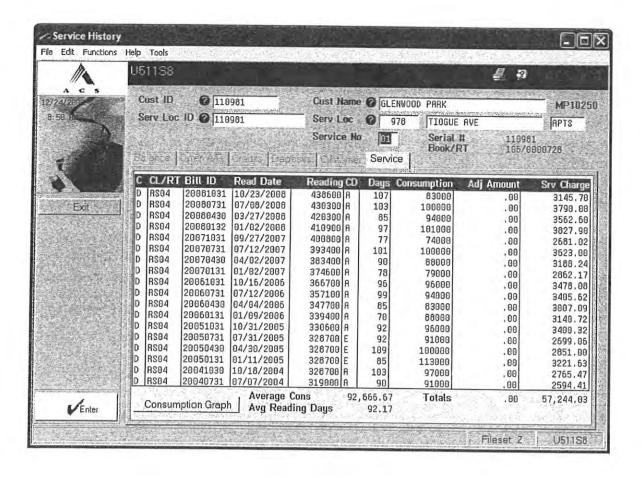


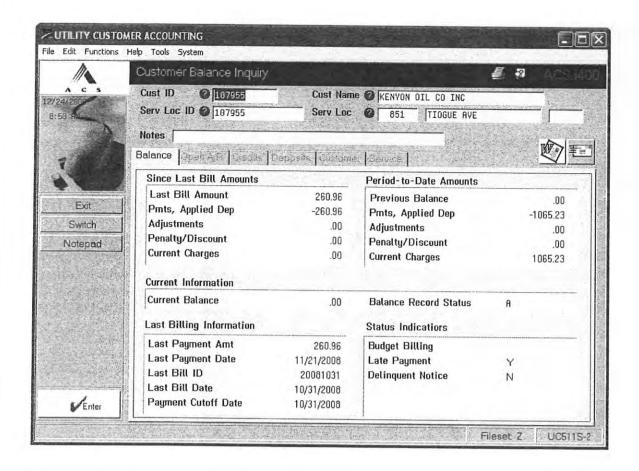


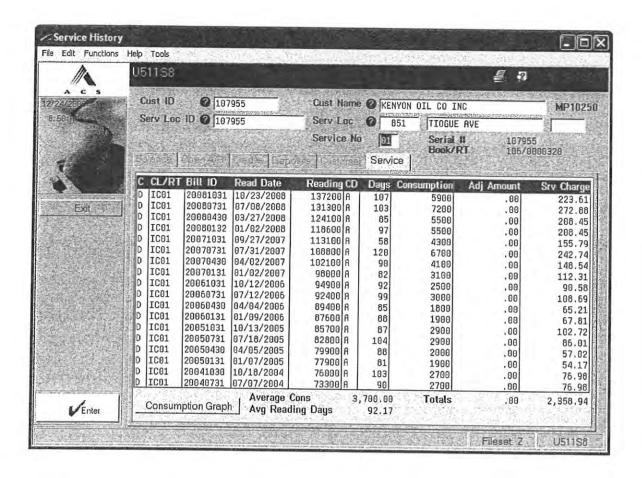


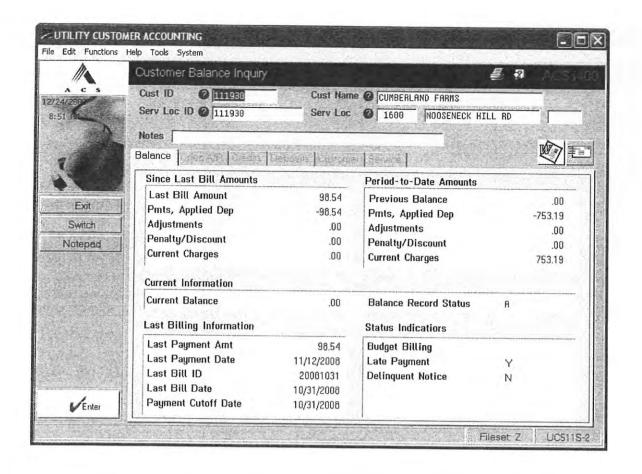


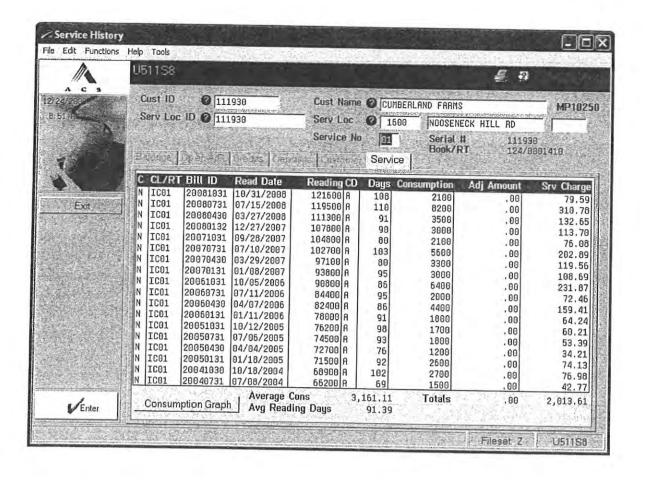


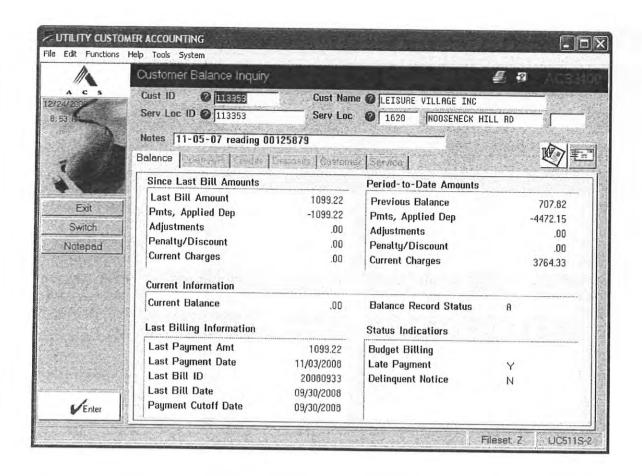


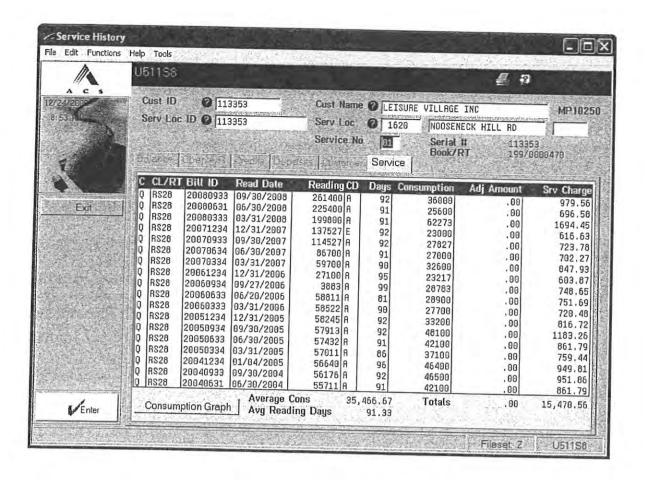


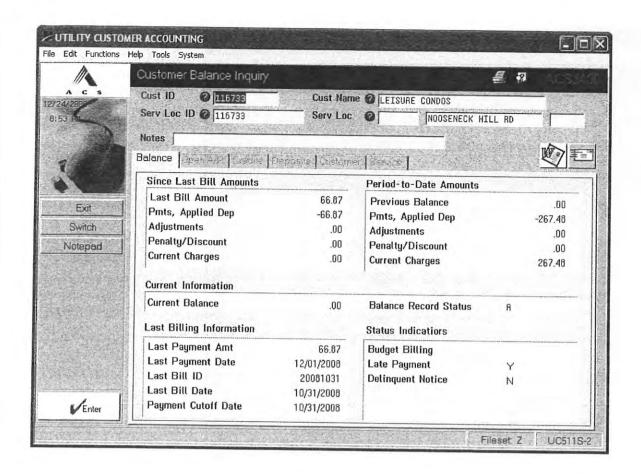


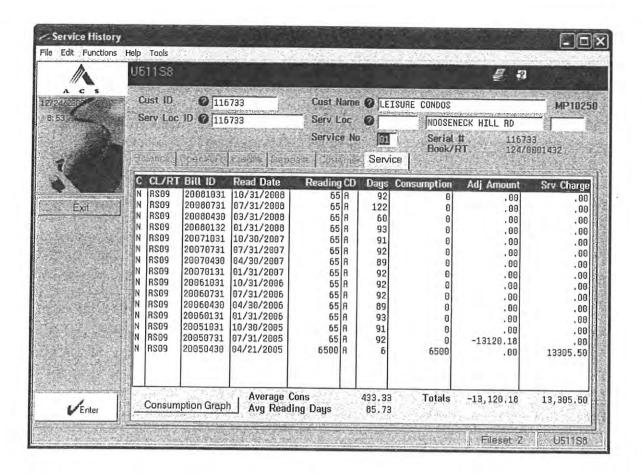


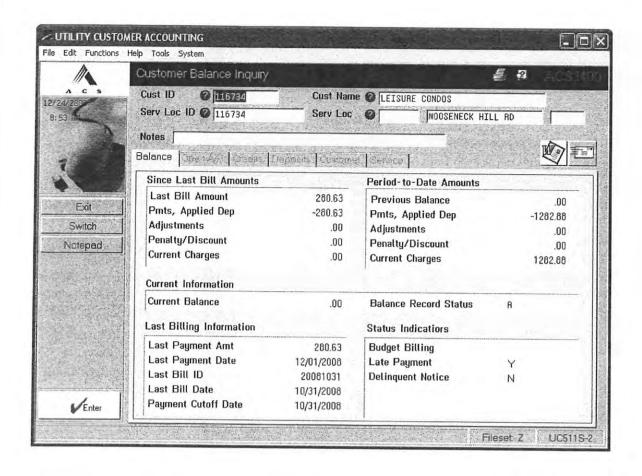




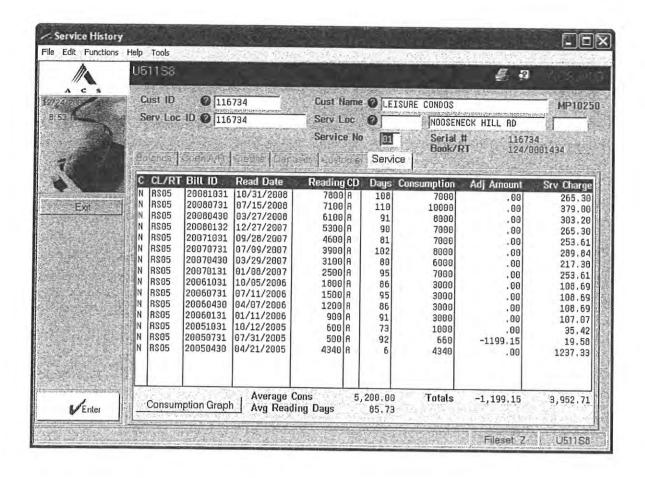








APPENDIX K





Appendix L
Town Owned Pump Station Flow Records

	Sandy Bottom Road PS			Pulaski Street Flume			Tiogue Ave Meter Pit (Woodland Manor)			Flat River Road PS		
Date	Totalizer Reading	GPD	Notes	Totalizer Reading	GPD	Notes	Totalizer Reading	GPD	Notes	Totalizer Reading	GPD	Notes
6/30/2015	150,121,000	318,276		1,355,617,000	1,027,172		263,341,440	16,728		429,000	1,621	
6/1/2015	140,891,000	249,355		1,325,829,000	961,839		262,856,320	3,034		382,000	1,645	
5/1/2015	133,161,000	212,400		1,296,012,000	1,021,133		262,762,260	14,835		331,000	NA	
4/1/2015	126,789,000	118,133		1,265,378,000	1,019,100		262,317,220	42,727		NA	NA	
3/2/2015	123,245,000	119,115		1,234,805,000	931,328		261,035,400	17,215		NA	NA	
12/31/2014	115,979,000	205,433		1,177,994,000	946,500		259,985,300	22,587		NA	NA	
12/1/2014	109,816,000	114,032		1,149,599,000	1,208,626		259,307,700	41,139		NA	NA	
10/31/2014	106,281,000	70,767		1,112,131,600	425,723		258,032,380	63,875		NA	NA	
10/1/2014	104,158,000	80,517		1,099,359,900	1,115,997		256,116,120	59,161		NA	NA	
9/2/2014	101,823,000	113,969		1,066,996,000	935,688		254,400,440	51,532		NA	NA	
8/1/2014	98,176,000	108,194		1,037,054,000	960,194		252,751,420	43,712		NA	NA	
7/1/2014	94,822,000	131,345		1,007,288,000	967,448		251,396,360	42,330		NA	NA	1
6/2/2014	91,013,000	115,875		979,232,000	946,000		250,168,800	NA		NA	NA	
5/1/2014	87,305,000	216,167		948,960,000	1,075,100		NA	NA		NA	NA	
4/1/2014	80,820,000	455,000		916,707,000	953,688		NA	NA		NA	NA	
2/28/2014	66,260,000	351,714		886,189,000	953,893		NA	NA		NA	NA	
1/31/2014	56,412,000	367,034		859,480,000	862,069		NA	NA		NA	NA	1
1/2/2014	45,768,000	433,806		834,480,000	NA		NA	NA		NA	NA	
12/2/2013	32,320,000	138,258		819,013,000	NA	Meter failed and is being repaired.	NA	NA		NA	NA	
11/1/2013	28,034,000	108,742		819,013,000	NA	Meter failed and is being repaired.	NA	NA		NA	NA	
10/1/2013	24,663,000	228,750		818,874,000	NA	Meter failed and is being repaired.	NA	NA		NA	NA	
8/30/2013	17,343,000	216,966		818,874,000	NA	Meter failed and is being repaired.	NA	NA		NA	NA	
8/1/2013	11,051,000	NA	Flow Meter Reset	808,172,000	707,258		NA	NA		NA	NA	
7/1/2013	1,004,595,000	274,357		786,247,000	518,393		NA	NA		NA	NA	
6/3/2013	996,913,000	181,485		771,732,000	431,636		NA	NA		NA	NA	
5/1/2013	990,924,000	218,600		757,488,000	471,733		NA	NA		NA	NA	
4/1/2013	984,366,000	268,290		743,336,000	523,258		NA	NA		NA	NA	
3/1/2013	976,049,000	191,586		727,115,000	472,552		NA	NA		NA	NA	
1/31/2013	970,493,000	214,935		713,411,000	450,484		NA	NA		NA	NA	
12/31/2012	963,830,000	166,964		699,446,000	450,429		NA	NA		NA	NA	
12/3/2012	959,155,000	155,455		686,834,000	430,030		NA	NA		NA	NA	
10/31/2012	954,025,000	132,367		672,643,000	425,100		NA	NA		NA	NA	
10/1/2012	950,054,000	127,333		659,890,000	388,000		NA	NA		NA	NA	
9/28/2012	949,672,000	123,750		658,726,000	425,750		NA	NA		NA	NA	
9/4/2012	946,702,000	144,029		648,508,000	444,286		NA	NA		NA	NA	
7/31/2012	941,661,000	153,621		632,958,000	443,793		NA	NA		NA	NA	
7/2/2012	937,206,000	214,000		620,088,000	462,333		NA	NA		NA	NA	
6/29/2012	936,564,000	225,286		618,701,000	223,821		NA	NA		NA	NA	
6/1/2012	930,256,000	NA		612,434,000	NA		NA	NA		NA	NA	
Average		196,376	Note 1		714,556			34,906			1,633	
Maximum		455,000	Note 2		1,208,626	Note 2		63,875	Note 2		1,645	Note 2

Notes

^{1.} Each pump at the Sandy Bottom Road PS is capable of 1,800 gpm (2,592,000 gpd) max capacity.

^{2.} Maximum flows are maximum flow during the time period of this table.



5 Centennial Drive, Peabody, MA 01960 (HQ) Tel: 978.532.1900

Town of Coventry, Rhode Island W&S Job No. 2140605

September 8, 2016

Mr. Arthur G. Zeman, P.E. Principal Engineer RIDEM Office of Water Resources 235 Promenade Street, 2nd Floor Providence, Rhode Island 02908-5767

Re:

Town of Coventry Facilities Plan Update (DEM File #16-C) Response to Comments (2nd Response)

Dear Mr. Zeman:

Per discussions with you related to the ownership of the Woodland Manor capacity at the West Warwick Treatment Plant, Weston & Sampson, Inc. has updated the Facilities Plan Update (FPU) for the Town of Coventry. Enclosed are excerpts from the FPU showing the updated changes (highlighted in yellow).

Should you have any questions or require additional information, please contact me at 1-800-SAMPSON Ext. 2421.

Very truly yours,

WESTON & SAMPSON, INC.

Tim DeGuglielmo Project Manager

Enclosure

cc: Graham Waters, Town Manager, Coventry

1 EXECUTIVE SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

1.0 General

There is currently only a limited wastewater collection system existing in the Town of Coventry. Approximately 97 percent of the residences in Coventry rely on onsite wastewater treatment systems (OWTSs) for treatment and disposal of wastewater.

Previous wastewater planning studies for Coventry recommended construction of wastewater collection facilities, with transmission to the regional wastewater treatment facility (WWTF) in West Warwick for treatment, to serve much of the densely populated eastern portion of Town. OWTS problems in the eastern portions of Town are common. In 1984 the Town executed an inter-municipal agreement (IMA) with West Warwick reserving an average daily flow of 2.25 million gallons per day (MGD) of wastewater capacity in their regional WWTF. In December 2013, the Town acquired a pump station and forcemain that were previously privately owned by the Woodland Manor Estates development. This pump station/forcemain serves properties whose capacity fall under a separate 200,000 gallons per day flow allocation in the West Warwick WWTF (future IMA revisions will be needed to address allocating this capacity to the Town).

Since the installation of the main interceptor, which collects and transports wastewater to the WWTF, the Town has begun to expand their collection system to congested and environmentally sensitive areas.

The purpose of this Facility Plan (FP) Update is to investigate and address the following:

- 1. Update of the projected wastewater flows for the 20-year (2035) and 50-year (2065) planning periods.
- 2. Provide review and evaluation of need for wastewater collection facilities, including:
 - a. delineation of problem areas,
 - b. determination of OWTS rehabilitation (or repair) feasibility, and
 - c. prioritization of sewer needs areas.
- 3. Examine relevant wastewater project financing options available and feasibility of implementation.

1.1 Findings

Chapters 3 and 4 of this Facilities Plan examine the current and expected future conditions in eastern Coventry, with specific interest in the treatment and disposal of wastewater. The investigations performed included review of all available relevant documents. The results of the OWTS survey (**Appendix A**) confirms a preponderance of OWTS problems in several areas of eastern Coventry. These areas have been delineated and were prioritized (Phase I) for sewering in the 1995 FP and subsequent reaffirmations/updates. The conclusion reached through these examinations is that the current system of wastewater disposal through onsite wastewater treatment systems (OWTSs) is not an acceptable long term solution in some areas of eastern Coventry. Continued operation of OWTSs may increase pollutant loads to ground and surface



and adjacent parcels along Hopkins Hill Road. The Phase I system, when completed, will also directly service approximately 933 properties, including many multi-family and commercial properties. The capital cost associated with the remaining Phase I construction program (Contracts 8, 9 and 11) is approximately \$6,681,000 (2015 dollars). Chapter 7 in this report outlines the implementation necessary to maintain and continue the expansion of the existing sewer system.

The Phase II sewer program could be implemented both during and following completion of Phase I, depending on economic feasibility and need. Phase II consists of approximately 203,400 feet of interceptor and lateral sewers, and eight wastewater pump stations with approximately 6,375 feet of forcemains. The Phase II system consists mainly of lateral (collector) sewers, and when completed will service approximately 3,846 properties (in addition to those served by Phase I). The total capital cost associated with Phase II is approximately \$51,662,000 (2015 dollars). Due to its magnitude, this phase would most likely be constructed over an eight to ten year period.

The Phase III sewer program could be implemented both during and after completion of the Phase II system, depending on economic feasibility and need. Phase III consists of approximately 45,150 feet of lateral sewers, and three wastewater pump stations with approximately 2,800 feet of forcemains. The Phase III system would service approximately 1,064 properties (in addition to those served by Phases I and II) when completed. The total construction cost associated with Phase III is approximately \$11,554,000 (2015 dollars). At this time, construction of the Phase III system may not commence for eight to ten years. Sewers under this phase would likely be constructed on an area by area (contract) basis, as needs arise.

Once constructed, administration, operation and maintenance of the wastewater collection system should be provided by the Town of Coventry. This will likely continue to initially include the hiring of private contractors to provide sewer system operation and maintenance services. The eventual establishment of a Coventry Sewer Department, under the current Public Works Department, is also a possibility. Included in the sewer system administration tasks would be the billing of Coventry sewer users.

Portions of Town to the north and west of the areas to be sewered will continue to be served by OWTS. Septage from the periodic pumping of these OWTSs should be disposed of at the West Warwick Regional WWTF, or Cranston WWTF. In these areas, and more importantly in areas where OWTS problems are prevalent, future provisions should be made for a public information program on the proper care and maintenance of OWTSs.

1.3 West Warwick Regional Sewer System

Wastewater and septage generated in Coventry will be transported to the West Warwick Regional Wastewater Treatment Facility (WWTF). Coventry currently has a reserve capacity of 2.25 mgd (average daily flow) in the WWTF. This is sufficient to cover the design year 2035 flow of 1.985 mgd from all phases outlined in the recommended sewer program. As of 2014, Coventry is contributing about 0.226 mgd (average daily flow) to the West Warwick WWTF (not including flows from the Woodland Manor sewer system which total 0.065 mgd, and East Greenwich/Amgen Pharmaceuticals). To date, Coventry has paid approximately \$10.9 million (in addition to the amount paid for the acquisition of the Woodland Manor infrastructure) for this capacity in West Warwick



program. The cost of the sewer projects will be paid for through assessments to sewered properties. The Town has established the method of assessment in their sewer use ordinance. This method is summarized in **Chapter 7**.

1.5 Summary

The conclusions reached from this FP Update echo those conclusions from the 1995 FP, the 2003 FP Reaffirmation and the 2010 FP Update. It is recommended that the existing sewer system be expanded to serve portions of eastern Coventry that can no longer rely on OWTSs for long term wastewater management. The plan recommended herein, however, revises the previous recommended sewer plan to provide flow allocations in areas where future development will require additional wastewater management capacity and/or add additional areas based on the additional capacity available for the Woodland Manor pump station/forcemain acquisition. This plan will still meet the need for sewering of the more densely populated areas within eastern Coventry, while also allowing the Town to provide sewer capacity for proposed developments, which are important to the local economy.

The recommended plan should be adopted, and implementation of the remainder of the Phase I sewer construction program should continue, as outlined in Chapter 7. This plan will result in a fully functioning sewer system which will serve Coventry through the year 2035 and beyond.

In order to remain eligible for State and/or Federal funding assistance, this Wastewater Treatment Facilities Plan should be reaffirmed every five years and should be updated or amended as necessary when significant changes occur that might otherwise impact the recommendations outlined in this report.



supporting their designated uses due to pollution. At the time of this Facilities Plan Update, all of the Pawtuxet River in Coventry was able to support all designated uses and was deemed fishable/swimmable.

Although there seems to be a significant increase in the water quality in Coventry, there is no way to estimate the actual number of direct wastewater and stormwater discharges in Coventry without a more comprehensive study.

3.6 Existing Wastewater Collection and Treatment System

3.6.1 West Warwick Regional Wastewater Treatment Facilities

As noted in Chapter 2 of this report, the State's 208 Areawide Water Quality Management Plan (WQMP) recommended that wastewater from Coventry be treated at the West Warwick Regional Wastewater Treatment Facility. This contradicted the previous recommendations for an independent Coventry Wastewater Treatment Facility made by earlier reports ("Preliminary Engineering Survey and Report on Sewerage and Sewage Treatment for the Town of Coventry", Fenton G. Keyes Associates, November 1966, and "Facilities Plan for Wastewater Collection and Treatment Facilities", C.E. Maguire, Inc., 1977). The recommendation of the 208 study has since been implemented, and Coventry is now a member community in the West Warwick regional system.

In 1984, the Town of Coventry signed an Inter-Municipal Agreement (IMA) with the Town of West Warwick, which provided 2.25 mgd (average daily flow) of capacity for Coventry in the West Warwick Regional Wastewater Treatment Facility.

In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain. The capacity allocation in the West Warwick system for the Woodland Manor pump station/forcemain is 0.2 mgd. Future IMA revisions will be needed to address allocating the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

The West Warwick Regional Wastewater Treatment Facility is located off Pontiac Avenue, in the northeast corner of West Warwick. The treatment facility discharges treated effluent to the Pawtuxet River. The facility can discharge an average daily flow of 10.5 mgd (peak flow of 25.34 mgd). West Warwick's facility consists of an activated sludge treatment process, along with a biological activated filter and UV disinfection.

The West Warwick facility currently has the equipment to properly accept septage for treatment. However, at this time no septage is accepted at the facility. The IMA between West Warwick and Coventry has a stipulation that would allow Coventry to dispose of septage at the facility if it were to be accepted from any other communities (including West Warwick).

Specific information on the existing and proposed West Warwick Regional Wastewater Treatment Facilities is contained in the West Warwick Wastewater Facilities Plan.



Development Corp. entered into an agreement with West Warwick to allow the discharge of 200,000 gallons per day to the West Warwick system. Since the construction of the Woodland Manor force main, the pipeline owners have allowed several pressure connections along the length of Tiogue Avenue. These connections have typically been to commercial establishments with severe OWTS problems. Such connections were approved by both West Warwick and Coventry (whose plant capacity was utilized for the connections).

Up until December 2013, this was a privately owned and operated sewer system, separate from the Town of Coventry system, and designed to provide sewer service to an area within eastern Coventry. In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain (future IMA revisions will be needed to address allocating this capacity to the Town).

Two assessments had been performed on the pump station and forcemain, and were reviewed by the Town prior to the acquisition of the infrastructure. The assessment performed by DiPrete Engineering can be found in **Appendix K**. The other assessment performed by Fuss & O'Neill is with the Town's Engineer. These assessments outlined recommended repairs and upgrades to the pump station. It is recommended the Town perform the repairs/upgrades as part of their yearly infrastructure maintenance plan.

In addition, Weston & Sampson Services has been contracted by the Town to operate and maintain the system since the acquisition. Flow records from the station can be found in **Appendix L**.

3.6.2.h Contract 03-01

The Contract 03-01 sewer project was constructed in 2004 by the Town of Coventry to service portions of Tiogue Avenue and Washington Street. This contract connected the system to the Sandy Bottom Road pump station, built under Contract 03-02 by the Town of Coventry. The connection to the pump station under the Pawtuxet River was by a depressed sewer made up of a series of ductile iron pipes (3 barrels - one 16-inch and two 12-inch pipes). Two 12-inch ductile iron force mains extend from the pump station to the intersection of Washington Street and Knotty Oak Road (approximately 2,500 feet). A 30-inch PVC gravity sewer pipe extends from the intersection of Washington Street and Knotty Oak Road to the intersection of Washington Street and Pulaski Street (approximately 6,100 feet). A 24-inch PVC gravity sewer extends from the pump station to approximately 3,000 feet west along Tiogue Avenue. This line connected to the previously "dry" sewer line installed in Hopkins Hill Road, and allowed for the activation of that sewer line.

As part of this project a flume/flow meter vault was installed to monitor and track flows from the interceptor into West Warwick. These flow records can be found in **Appendix L**. The existing telephone line communications system to send out the flow meter readings has had issues in the past. It is recommended to perform an evaluation on the communication system to see if a more suitable alternative (i.e. radio, high speed internet) is available.



3.6.3 Existing Wastewater Flows

As described above, the Town of Coventry owns approximately 2.25 mgd of total capacity in the West Warwick Wastewater Treatment Facility. This average daily flow capacity was based on the Year 2000 projections in the 1981 Amended Facilities Plan. The current estimated wastewater flow from Coventry to the West Warwick sewer system is approximately 291,000± gallons per day (gpd) average daily flow (including 65,000± gpd related to the Woodland Manor system), as shown in **Table 3-6**. The existing flows are based on of KCWA water use records. This is a conservative value, as it would be expected that sewer flows would typically represent 80% to 90% of the parcels water use. This wastewater flow also does not include flows from the Amgen facility, as they do not count against Coventry's capacity allocation in West Warwick. The present peak flow from Coventry can therefore be estimated as 1,367,000± gpd using a peaking factor of 4.7 (see **Figure 3-12**).

The Town has a total of five wastewater flowmeters located in the sewered areas. Data from these flowmeters is included in **Appendix L**. These flowmeter locations are as follows:

- <u>Pulaski Street Flow Meter</u>: This flowmeter is located on Pulaski Street near the West Warwick Town Line. It measures flow from the Contract 03-01 interceptor that runs east on Washington Street.
- <u>Sandy Bottom Road Pump Station Flow Meter</u>: This flowmeter is located on the discharge piping in the Sandy Bottom Road Pump Station (Contract 03-02). This flowmeter measures all flow pumped from the station.
- <u>Industrial Drive Pump Station Flow Meter</u>: This flowmeter is located on the discharge piping in the Industrial Drive Pump Station (Contract 7 & 7A). This flowmeter measures all flow pumped from the station.
- Woodland Manor Forcemain Flow Meter: This flowmeter is located on the Woodland Manor Forcemain, on Tiogue Avenue near the intersection of Darton Street (near #354 Tiogue Avenue). This flowmeter measures all flow pumped from the station, in addition to any ancillary parcels that are connected to the Woodland Manor Forcemain.
- Highlands at Hopkins Hill Condo Flowmeter: This flowmeter is located on Hopkins Hill Road near the intersections of Dante Drive and Enzo Drive. This flowmeter measures flow from the Highlands at Hopkins Hill Condo Development. This flowmeter was installed for billing purposes, because the detached condos do not have separate water meters. The Town typically bills sewer use charges based on water meter readings from KCWA.



industrial facility has connected into Coventry's sewer system and "mothballed" the WWTF. Further discussions on remaining WWTF infrastructure and potential use to the Town of Coventry remain unresolved.

2. West Warwick Regional Wastewater Treatment Facility

As discussed above, treatment of Coventry's wastewater at the West Warwick regional WWTF is a principal recommendation of the 208 WQMP. The 1981 Amended FP and the 1982 FP Supplement also recommended this treatment option.

Based on the previous 1995 FP, 2003 FP Reaffirmation and 2010 FP Update, the Town of Coventry has finished construction on a limited municipal sewer system. This system includes interceptor and lateral piping that collects wastewater flow from portions of the planning areas, including residences, businesses and institutions, and transports this flow to the West Warwick Wastewater Treatment Plant (WWTP).

To allow this discharge into the West Warwick sewer system, and eventually the WWTP, Coventry entered into an intermunicipal agreement (IMA) with West Warwick (originally dated November 28, 1994). The agreement included provisions for Coventry to reimburse West Warwick for capital costs related to the WWTF capacity and collection system expansions required to allow service to Coventry. West Warwick then proceeded with upgrading their WWTF to provide secondary treatment levels, and expanding the treatment plant's capacity to allow connection of the Coventry system. West Warwick also increased the capacity of their interceptors to allow the transmission of Coventry's wastewater to the regional WWTF. The IMA allows a certain amount of flow (2.25 mgd) and pollutant loading to be discharged into the West Warwick system by Coventry. All flow treated by the West Warwick WWTF is discharged into the Pawtuxet River.

In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain. The capacity allocation in the West Warwick system for the Woodland Manor pump station/forcemain is 0.2 mgd. Future IMA revisions will be needed to address allocating the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065.

Since construction of portions of the planned sewer system interceptors has been completed based upon recommendations set forth in the 1995 FP, 2003 FP Reaffirmation and 2010 FP Update, planned extension of this sewer system to serve the planning areas has been evaluated as part of this FP Update. Careful considerations were made so that the current and



table, and as discussed in Chapter 4, the 'no action' option is estimated to have the greatest detrimental long-term effect on the area, mostly by way of water quality and quality of life. The probable effect of a public education program, or an OWTS rehabilitation program, alone would be similar to the 'no action' option, though lesser in magnitude, and would likely result in some minor short-term construction related impacts. The effects of a sewer installation program on the project area would have significant short-term construction related impacts. Such a program would, however, result in significant long-term benefits to the community, both in water quality and in quality of life.

5.8 Financial Considerations for Alternatives

The final consideration for selecting an appropriate option for addressing the planning area OWTS problems is project cost. From a public opinion standpoint, this is perhaps the most important consideration. The question of the affordability of a project most often determines whether it is eventually implemented, or falls by the wayside. In Coventry past initiatives based on recommendations from prior FPs have failed, mostly due to real or perceived financial impacts of the proposed sewer construction program. Therefore, financial considerations will continue to play a major role in selecting the best available option.

For the purposes of this analysis, a planning period of 20 years has been used. Analyses include an estimated present worth value for each option discussed.

5.8.1 No Action

The 'no action' alternative is always the most advantageous from an initial cost viewpoint. Since this option requires no initial capital input by the Town, the capital cost associated with it (other than for individual OWTS care and maintenance) is negligible. Actual annual costs associated with this option would be borne by individual property owners, and are difficult to predict. Such costs would include OWTS maintenance pumping, and repair and potential replacement of failing OWTSs. Based on the average system pumping criteria of one pump-out per three years used to estimate septage volumes in Chapter 4, and an average pump-out charge of \$200 as determined from previous Septage Hauler Interviews, the minimum cost of this option is approximately \$67 per home per year.

In addition, costs already expended by the Town for a sewer system would be wasted if this option was selected. To date these costs include approximately \$10.9 million (in addition to the amount paid for the acquisition of the Woodland Manor infrastructure), for capacity in the West Warwick sewer system and WWTF upgrades, and approximately \$20.6 million for installation of existing pump station, interceptor and lateral sewers. Unfortunately, selection of the `no action' alternative provides no wastewater management benefit to the Town. Where significant water quality and public health concerns currently exist, this is not an acceptable alternative.



limited OWTS failures, this option is cost effective, but could be considered equivalent to the 'no action' option, since OWTS reconstruction can be left to the individual property owner. For areas where a significant percentage of existing OWTS systems are failing, this option is not as acceptable, since the costs for rehabilitating many systems is significant, and may approach the cost of lateral sewer installation.

5.8.5 <u>Wastewater Collection and Treatment System</u>

In many areas, the installation of a wastewater collection system is the only reasonable alternative for permanently ending the chronic OWTS failure problems.

5.8.5.a <u>Sewer Interceptor System</u>

The previous 1995 FP and 2010 FP Update outlined the three most logical options for proposed sewer interceptor systems. The option previously recommended and constructed is briefly described below. The original interceptor plan from the 1995 FP is included in **Figure 5-1** (Note that since the 1995 FP and 2010 FP Update some of the interceptors have been constructed, see **Figure 3-10** for the current existing interceptors):

Central Pumping Station at Tiogue Avenue and Washington Street Interceptor: This option included constructing a pump station on Sandy Bottom Road. A new force main was installed on Sandy Bottom Road that discharges to a gravity interceptor at the approximate intersection of Washington Street and Knotty Oak Road. This gravity interceptor would then travel east along Washington Street to the intersection of Quidnick Avenue where it would then follow an abandoned railroad bed to Whitford Street and down Pulaski Street to the West Warwick Town boundary.

This option was selected in the previous report based on the proposed benefits and the project's cost effectiveness. Based on this recommendation of the 1995 FP, this option, including the Sandy Bottom Road Pump Station, forcemain and Washington Street interceptor to the West Warwick Town boundary were constructed.

In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain. With the existing pump station and forcemain infrastructure already being installed, there is potential to use this pump station/forcemain to sewer adjacent areas previously eliminated or deemed to be not cost effective to sewer due to location (i.e. Planning Area N/N-1). Also, as portions of the forcemain may be flowing under gravity conditions, further investigation should be made to assess the feasibility of using portions of Woodland Manor force main to service parcels along Tiogue Avenue where collection sewers have yet to be constructed. Future IMA revisions will be needed to address allocating the Woodland Manor capacity to the Town prior to any of these potential projects being constructed, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

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In the 2003 FP Reaffirmation, additional wastewater treatment capacity was allocated for two proposed developments (Pine Ridge Subdivision and Center of New England) that would significantly change the original assumption for sewer flow for the parcels. Due to this additional wastewater allocation need, Planning Areas (AA and AB) with less need for sewering were removed and instead it was recommended to continue the utilization of the existing OWTSs.

In the 2010 FP Update, additional wastewater treatment capacity was allocated for multiple proposed developments that significantly changed the original assumption for sewer flow for the parcels, and two industrial properties (Clariant Corporation and Rhodes Technologies) that were granted connection to the system, that previously had a private WWTF and were unaccounted for in previous FP's allocated wastewater treatment capacity. As part of the 2010 FP Update, Planning Areas AF, AD, Y and portions of Planning Areas AE, N, O, X and Z with less need for sewering were removed and instead it was recommended to continue the utilization of the existing OWTSs.

The Town's wastewater capacity per their existing IMA with West Warwick, provides the Town with a total wastewater treatment capacity of 2.25 mgd in the West Warwick system. Future IMA revisions will be needed to address officially allocating the 0.2 mgd of the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

As part of the selected plan areas adjacent to the Woodland Manor pump station and forcemain that were previously ruled out or eliminated due to conventional sewer construction feasibility were analyzed with regards to this recently acquired infrastructure. Also, a small area to the southwest of Planning Area N that was not included in the original "sewered" area plan was analyzed to determine the potential need for sewering.

6.1.2 Revised Recommended Plan

The revised recommended revisions to the 2010 FP Update sewering plan are described below and include the addition of properties in Planning Area N previously removed in previous FP Update and inclusion of an area to the southwest of Planning Area N that was not originally included in the original "sewered" area plan, but is in a location that was determined to have a need for sewering.

Information collected for each Planning Area to determine sewer needs is summarized in **Table 6-1**. Based upon this information, a new recommended sewer plan can be established. **Figure 6-1** shows this revised sewer plan, and the areas that are recommended for removal. It should be noted that the full or partial removal of an area does not mean that area will never receive municipal sewers. Circumstances could arise that cause a Planning Area to be reinstated to the recommended plan for sewering, such as a sudden increase in need or increased available wastewater treatment capacity obtained by the Town. These circumstances will continue to be monitored in future planning exercises and changes made based upon the findings.

The following sub-sections 6.1.2.a to 6.1.2.ii briefly describe each planning area and based on information presented in this report, either confirm the recommendations of the



6.1.2.mPlanning Area M

Planning Area M was recommended for sewering as part of the 1995 FP, 2003 FP Reaffirmation and 2010 FP Update reports. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTSs and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The majority of wastewater from this area originates from the mobile home compounds located in the northeast portions of the planning area and is pumped south along Reservoir Road into the Tiogue Avenue Interceptor (West). This area was proposed to be sewered as part of the Phase III sewer program, meaning the area was deemed to be poor for OWTS construction, but that other areas (Phase I and Phase II areas) were deemed either to have a greater need for sewers or their locations were such that sewering was more economically feasible.

Currently, the mobile home compounds located in this area are connected into the Woodland Manor Forcemain located on Tiogue Avenue. The Town's recent acquisition of the Woodland Manor Pump Station/Forcemain provides potential connection to these parcels into the Town's system. However, prior to this potential connection, future IMA revisions will be needed to address officially allocating Woodland Manor capacity to the Town.

Based upon updated information obtained for this report, the need to serve the remaining parcels in this area by means of an off-site wastewater management solution still exists. Therefore, the recommendation for this area to remain in the Phase III sewer program is confirmed.

6.1.2.n Planning Area N

Planning Area N was recommended for sewering as part of the 1995 FP report. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTSs and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The majority of wastewater from this area is to flow to the now Town owned Woodland Manor Pump Station, which transmits flow to West Warwick. This area was proposed to be sewered as part of the Phase III sewer program, meaning the area was deemed to be poor for OWTS construction, but that other areas (Phase I and Phase II areas) were deemed either to have a greater need for sewers or their locations were such that sewering them was more economically feasible.

Based on information in the 2010 FP Update, it was recommended that all parcels in this area are removed from the sewering plan, in favor of the continued use of existing OWTSs for wastewater disposal, with the exception of those parcels able to be served by gravity sewers from the existing system (see Chapter 6 of the 2010 FP Update for more detailed information).

However, because of the Town's recent acquisition of the Woodland Manor forcemain and pump station, there is the ability for some of the parcels in this area to be sewered by gravity to this pump station. This will allow a portion of the parcels previously recommended to continue the use of OWTS systems, to be



allowed to connect to the municipal sewer system. Prior to allowing this potential connection, IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town.

Other parcels located in this planning area that are still in a remote location and would require pump stations or low pressure sewers to be installed based on the topography of this area will continue utilize the existing OWTSs for wastewater disposal. As stated in the 2010 FP Update, drawbacks to the continued removal of these parcels from the sewer plan are its close proximity to Johnson Pond and the possibility that poor soils not conductive to on-site systems may be located in the area. However, due to the increased treatment capabilities of current conventional or A/E OWTS technologies for use where possible site restrictions are a factor, options exist for providing adequate treatment of wastewater by use of OWTSs in this planning area. This factor compiled with the fact that the area has a large concentration of single family homes where a majority of the lot sizes are sufficient for conventional OWTS construction making sewering this area a lower priority.

Therefore, it is recommended that all parcels able to flow by gravity into the Woodland Manor Pump Station be recommended for sewering, while the remaining parcels are recommended for the continued use of existing OWTSs for wastewater disposal.

Due to continued reliance on OWTSs and their possible impact with the environment caused by improperly functioning OWTS, coupled with lack of general knowledge that most homeowners have regarding operation and maintenance (O&M) their septic systems, a public education program (as described in Chapter 5) is recommended in this planning area. This area should continue to be monitored for any future signs of widespread OWTS failure.

Additional flows generated by sewering this area can be reallocated by the use of the additional capacity gained by the Town from the purchase of the Woodland Manor Forcemain/Pump Station. Prior to allowing this potential connection, IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town.

6.1.2.n.1 Planning Area N-1

Due to the Town's purchase of the Woodland Manor Forcemain/Pump Station infrastructure and the now Town owned infrastructure in close proximity, there are some additional adjacent areas that can be served by this pump station. This area is southwest of Planning Area N, and included the parcels bordering Nooseneck Hill Road to the Town line. This area includes both residential and commercial properties, including a mobile home park (Maple Root Village), in close proximity to Maple Root Pond, which is tributary to the south branch of the Pawtuxet River. Maple Root Village consists of approximately 187 small mobile home lots located on a large parcel adjacent to Maple Root Pond. This area is also outlined as having poor soils for a properly functioning OWTS system. Also, the mobile homes present economic and on-site restrictions prohibiting properly functioning OWTSs (i.e. small lot sizes and densely populated). These reasons also diminish the feasibility of constructing newer properly functioning system.



Based upon updated information obtained for this report, the need to serve this area by means of an off-site wastewater management solution exists. Therefore, the recommendation for this area to be included in the Phase II sewer program is confirmed. Prior to allowing this potential connection, IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town.

6.1.2.o Planning Area O

Planning Area O was recommended for sewering as part of the 1995 FP report. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTSs and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The majority of wastewater from this area is proposed to flow to the Washington Street Interceptor via a pump station to be constructed. This area was proposed to be sewered as part of the Phase III sewer program, meaning the area was deemed to be poor for OWTS construction, but that other areas (Phase I and Phase II areas) were deemed either to have a greater need for sewers or their locations were such that sewering was more economically feasible.

Based on information in the 2010 FP Update, it was recommended that a portion of the parcels in this area that would require a pump station to reach the Washington Street Interceptor were removed from the sewering plan, in favor of the continued use of existing OWTSs for wastewater disposal (see Chapter 6 of the 2010 FP Update for more detailed information). Upon the review of this area as part of this FP Update, the concerns over economic feasibility for sewer construction, and the relatively low occurrence of OWTS repairs from 2008-2014 (7% of the removed parcels, **Appendix A**) are still present and the recommendation to remove the selected parcels from the sewering plan remains.

6.1.2.p Planning Area P

Planning Area P was recommended for sewering as part of the 1995 FP, 2003 FP Reaffirmation and 2010 FP Update reports. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTS and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The wastewater from this area is proposed to flow through the existing Washington Street Interceptor by gravity into West Warwick. This area was proposed to be sewered as part of the Phase I sewer program, meaning the area was deemed to have the greatest need in the Town for an off-site wastewater management solution.

Based upon updated information obtained for this report, the need to serve this area by means of an off-site wastewater management solution still exists. Therefore, the recommendation for this area to remain in the Phase I sewer program is confirmed. Sewers have been installed to serve parcels adjacent to Washington Street, and the remaining parcels in this area will be served as part of Sewer Construction Contract No. 8. The estimated date of commencement for the project is March 2018, based upon the 2015 Priority Determination System's Project Information Sheets submitted to RI-DEM.



June 8, 2016

Tim DeGuglielmo, P.E. Weston & Sampson Five Centennial Drive Peabody, MA 01960-7985

RE: Review of Coventry Facilities Plan Update (DEM file #16-C)

Coventry, Rhode Island

Dear Mr. DeGuglielmo:

The Rhode Island Department of Environmental Management, Office of Water Resources (OWR) has reviewed the above referenced Facilities Plan Update (FPU) and has the following comments that must be addressed prior to approval:

- 1. On page 1-5, please revise the last paragraph to "In order to remain eligible for State and/or Federal funding assistance, this Wastewater Treatment Facilities Plan should be reaffirmed every five years and should be updated or amended as necessary when significant changes occur that might otherwise impact the recommendations outlined in this report."
- 2. On page 3-14, under section 3.3.1, please change "Division of Air and Hazardous Materials" to "Office of Air Resources."
- 3. On page 3-29, section 3.6.1 (see also page 3-33 section 3.6.2.g and throughout the FPU) mentions the Intermunicipal Agreement between Coventry and West Warwick and the acquisition of Woodland Manor's 0.2 MGD of capacity. Has the Intermunicipal Agreement been formally amended to increase Coventry's allocated flow to West Warwick from 2.25 MGD to 2.45 MGD? If so, please append a copy of the executed new agreement to the FPU. Also, with the additional flow allocated to Coventry, have the percentages for Coventry's financial share of West Warwick's WWTF upgrades been adjusted to both party's satisfaction?
- 4. On page 3-34, section 3.6.2.i, the last sentence should be revised to, "The flows should be monitored, and once flows consistently reach 80% of the station's capacity, an upgrade should be performed to the station."
- 5. On pages 3-39, 4-11 and 7-9, the FPU recommends an I/I study in the older sewered sections of Town. Please include the preparation of an I/I study in Figure 7-1 Implementation Schedule.
- 6. On page 4-11, section 4.4, the first sentence states that there are eight additional proposed projects and the second sentence states that there are six. Please revise as necessary.
- 7. On page 6-11, last sentence, please revise the estimated date of commencement for Area P to match Contract 8's date of commencement in Figure 7-1 Implementation Schedule. As written, October 2010 seems incorrect, as does the reference to the 2010 PDS Project Information Sheet (it should reference

Tim DeGuglielmo, P.E. June 8, 2016 Page 2 of 2

the 2015 PDS Project Information Sheet). Appendix G indicates a commencement date of March 2018 for Contract 8.

- 8. On page 6-22, section 6.1.2.ii, in the first sentence, change "AC" to "AI."
- 9. On page 7-1, in the second sentence, shouldn't the references be "As part of the 1995 Facilities Plan, 2003 FP Reaffirmation and **2010** FP update?"
- 10. On page 7-7, in Table 7-2, the Total Project Construction Cost and the Total Local Cost for Contract 10 East Shore Drive Area don't agree. One is shown as \$2,120,000 and the other is shown as \$2,190,000. Please revise as necessary.
- 11. On page 7-9, section 7.1.9 explains the requirement for a Fiscal Sustainability Plan, but no Plan is presented in the FPU. The FPU should either include this Plan or include it as part of the Implementation Plan in section 7.2 and include its preparation as part of the Implementation Schedule on Figure 7-1. In order for project costs to be eligible for reimbursement through the SRF Program, a Fiscal Sustainability Plan must be completed.
- 12. Please include all Intergovernmental Review Process correspondence in Appendix M.

Please provide a written response to the above comments and submit copies of any revised pages. Once OWR determines that the comments have been satisfactorily addressed, OWR will direct the Town to schedule its final Public Hearing. Concurrently, OWR will advertise a thirty (30) day Public Notice of Intent to Issue a Finding of No Significant Impact in the Providence Journal. Once the Town's Public Hearing process is completed, please submit two (2) hard copies and one (1) electronic copy in .pdf format of the final FPU. The final FPU shall include all revisions made based on OWR's comments above and any other revisions made as a result of the Public Hearing and Intergovernmental Review processes. Upon receipt of the final FPU, OWR will issue an approval.

If you have any questions, please contact me at 401.222.4700, x7251 or at art.zeman@dem.ri.gov

Sincerely

Art Zeman, P.E., Principal Engineer Wastewater Planning & Design Section

Office of Water Resources

AGZ/agz

Electronic copy:

Kent Nichols, Weston & Sampson

tel: 978-532-1900 fax: 978-977-0100 www.westonandsampson.com

engineering, energy, planning, permitting, design, construction, operation, maintenance



Town of Coventry, Rhode Island W&S Job No. 2140605

July 25, 2016

Mr. Arthur G. Zeman, P.E. Principal Engineer RIDEM Office of Water Resources 235 Promenade Street, 2nd Floor Providence, Rhode Island 02908-5767

Re: Town of Coventry Facilities Plan Update (DEM File #16-C)
Response to Comments

Dear Mr. Zeman:

Weston & Sampson, Inc. has reviewed you letter dated June 8, 2016 and has addressed the comments concerning the recently reviewed Facilities Plan Update (FPU) for the Town of Coventry. The following are the requested narrative responses to your comments:

- 1. On page 1-5, please revise the last paragraph to "In order to remain eligible for State and/or Federal funding assistance, this Wastewater Treatment Facilities Plan should be reaffirmed very five years and should be updated or amended as necessary when significant change occur that might otherwise impact the recommendations outlined in this report."
 - The text has been revised as requested. Excerpts showing the revisions have been attached.
- 2. On page 3-14,under section 3.3.1, please change "Division of Air and Hazardous Materials" to "Office of Air Resources".
 - The text has been revised as requested. Excerpts showing the revisions have been attached.
- 3. On page 3-29, section 3.6.1 (see also page 3-33 section 3.6.2.g and throughoutt the FPU) mentions the Intermunicipal Agreement between Coventry and West Warwick and the acquisition of the Woodland Manor's 0.2 MGD of capacity. Has the Intermunicipal Agreement been formally amended to increase Coventry's allocated flow to West Warwick from 2.25 MGD to 2.45 MGD? If so, please append a copy of the executed new agreement to the FPU. Also, with the additional flow allocated to Coventry, have the percentages for Coventry's financial share of West Warwick's WWTF upgrades been adjusted to both party's satisfaction?
 - The IMA with West Warwick has not been amended. Text regarding this has been revised and Section 7 Implementation has also been revised to show this future step for the Town. Currently the Town is in no danger of exceeding their existing capacity. This additional Woodland Manor capacity is only required to handle Coventry projected wastewater flows for future planning years (2065 and beyond). However, the IMA should be amended in the future to properly allocate the Woodland Manor's capacity to the Town.

Massachusetts Connecticut New Hampshire Vermont New York Pennsylvania New Jersey South Carolina Florida

- 4. On page 3-34, section 3.6.2.i, the last sentence should be revised to, "the flows should be monitored, and once flows consistently reach 80% of the station's capacity, and upgrade should be performed to the station.
 - The text has been revised as requested. Excerpts showing the revisions have been attached.
- 5. On pages 3-39, 4-11 and 7-9, the FPU recommends an I/I study in the older sewered section of Town. Please include the preparation of an I/I study in Figure 7-1 Implementation Schedule.
 - Figure 7-1 has been updated to show the recommended I/I investigations dates. The updated Figure has been attached.
- 6. On pages 4-11, section 4.4, the first sentence states that there are eight additional proposed projects and the second sentence states that there are six. Please revise as necessary.
 - The text has been revised to show six currently proposed projects, as per the 2015 Project Description Forms. Excerpts showing the revisions have been attached.
- 7. On page 6-11, last sentence, please revise the estimated date of commencement for Area P to match Contract 8's date of commencement in Figure 7-1 Implementation Schedule. As written, October 2010 seems incorrect; as does the reference to the 2010 PDS Project Information Sheet (it should reference the 2015 PDS Project Information Sheet). Appendix G indicates a commencement date of March 2018 for Contract 8
 - The text has been revised to show the March 2018 commencement date, as per the Town's 2015 PDS Project Information Sheet. Excerpts showing the revisions have been attached.
- 8. On page 6-22, section 6.1.2.ii, in the first sentence, change "AC" to "AI".
 - The text has been revised as requested. Excerpts showing the revisions have been attached.
- 9. On page 7-1, in the second sentence, shouldn't the references be "As part of the 1995 Facilities Plan, 2003 FP Reaffirmation and **2010** FP Update?"
 - Correct. The text has been revised as requested. Excerpts showing the revisions have been attached.
- 10. On page 7-7, in Table 7-2, the Total Project Construction Cost and the Total Local Cost for Contract 10 East Shore Drive Area don't agree. One is shown as \$2,120,000 and the other is shown as \$2,190,000. Please revise as necessary.
 - The text has been revised to show the \$2,120,000 project construction cost. Excerpts showing the revisions have been attached.
- 11. On page 7-9, section 7.1.9 explains the requirement for a Fiscal Sustainability Plan, but no Plan is presented in the FPU. The FPU should wither include this Plan or include it as part of the

Implementation Plan in section 7.2 and include its preparation as part of the Implementation Schedule on Figure 7-1. In order for project costs to be eligible for reimbursement through the SRF Program, a Fiscal Sustainability Plan must be completed.

- The text has been revised to note that a Fiscal Sustainability Plan will need to be complete for every project under the SRF Program. Figure 7-1 has also been revised to show this. Excerpts showing the revisions have been attached.
- 12. Please include all Intergovernmental Review Process correspondence in Appendix M.
 - We have provided the letter template and all the Intergovernmental Review Contracts that
 the letter was mailed to. In addition, any response letter received from various agencies has
 been attached as well. No responses were received other than from the agencies provided.

Should you have any questions or require additional information, please contact me at 1-800-SAMPSON Ext. 2421.

Very truly yours,

WESTON & SAMPSON ENGINEERS, INC.

Tim DeGuglielmo Project Manager

Enclosure

cc: Graham Waters, Town Manager, Coventry

Excerpt(s) of FP for RI-DEM Review Comment #1

Chapter 7 presents a method of financing the estimated costs of the proposed sewer program. The cost of the sewer projects will be paid for through assessments to sewered properties. The Town has established the method of assessment in their sewer use ordinance. This method is summarized in **Chapter 7**.

1.5 Summary

The conclusions reached from this FP Update echo those conclusions from the 1995 FP, the 2003 FP Reaffirmation and the 2010 FP Update. It is recommended that the existing sewer system be expanded to serve portions of eastern Coventry that can no longer rely on OWTSs for long term wastewater management. The plan recommended herein, however, revises the previous recommended sewer plan to provide flow allocations in areas where future development will require additional wastewater management capacity and/or add additional areas based on the additional capacity obtained by the Woodland Manor pump station/forcemain acquisition. This plan will still meet the need for sewering of the more densely populated areas within eastern Coventry, while also allowing the Town to provide sewer capacity for proposed developments, which are important to the local economy.

The recommended plan should be adopted, and implementation of the remainder of the Phase I sewer construction program should continue, as outlined in Chapter 7. This plan will result in a fully functioning sewer system which will serve Coventry through the year 2035 and beyond.

In order to remain eligible for State and/or Federal funding assistance, this Wastewater Treatment Facilities Plan should be reaffirmed every five years and should be updated or amended as necessary when significant changes occur that might otherwise impact the recommendations outlined in this report.

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Excerpt(s) of FP for RI-DEM Review Comment #2

- Public and Semi-Public Uses, including schools, churches, town administrative facilities, Police and Fire Stations and other similar uses. These facilities are also concentrated in the eastern end of town convenient to the largest portion of Coventry's population.
- Parks, Recreation and Open Space Uses, including Agricultural Land, with the majority of open space and agricultural areas in the western and central parts of town.

Land use and development in Coventry is regulated by the town's Zoning Ordinance and Land and Subdivision Regulations. **Figure 3-7**, excerpted from the 2008 CCP (draft), shows the existing zoning districts for eastern Coventry.

3.3 Other Environmental Conditions

In addition to the areas discussed above, several other environmental conditions are relevant to the preparation of this wastewater facilities plan. These conditions include air quality, noise levels, wildlife and plant habitats, and other specific areas of concern as discussed below.

3.3.1 Air Quality

The Town of Coventry, as per the RIDEM Office of Air Resources, complies with the US Clean Air Act.

As of EPA's April 2012 Ozone Designations, Coventry is now in "Attainment" for the ground level ozone standards, however, in 2004 the entirety of Kent County was not in "Attainment" per the EPA's ground level ozone standards. The basis of the problem was "smog" created by hydrocarbons, oxygen and nitrogen combining in the presence of sunlight to form an inversion layer.

3.3.2 Noise Pollution

Industry-related stationary noise in Coventry is relatively light. Vehicular activity accounts for most of the Town's noise pollution with Route 3 (Tiogue Avenue) being the biggest offender, followed by Route 117 and, despite its volumes, Interstate 95 creates minimal impact due to its remote location on the fringe of Town. Coventry is located on a flight path to the T. F. Green State Airport and these flight patterns add significant noise impacts and visual disruptions to some areas of Coventry. In addition, some migratory bird patterns have been observed to be adversely affected by flight patterns over Coventry.

3.3.3 Wildlife

Coventry's approximate 62 square miles of land mass is home and habitat for numerous common and rare species of animals and plant life, all contributing to the delicate ecological balance of the area.



Excerpt(s) of FP for RI-DEM Review Comment #3

1 EXECUTIVE SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

1.0 General

There is currently only a limited wastewater collection system existing in the Town of Coventry. Approximately 97 percent of the residences in Coventry rely on onsite wastewater treatment systems (OWTSs) for treatment and disposal of wastewater.

Previous wastewater planning studies for Coventry recommended construction of wastewater collection facilities, with transmission to the regional wastewater treatment facility (WWTF) in West Warwick for treatment, to serve much of the densely populated eastern portion of Town. OWTS problems in the eastern portions of Town are common. In 1984 the Town executed an inter-municipal agreement (IMA) with West Warwick reserving an average daily flow of 2.25 million gallons per day (MGD) of wastewater capacity in their regional WWTF. In December 2013, the Town acquired a pump station and forcemain that were previously privately owned by the Woodland Manor Estates development. This pump station/forcemain came with an additional 200,000 gallons per day of capacity in the West Warwick WWTF (future IMA revisions will be needed to address officially allocating this capacity to the Town).

Since the installation of the main interceptor, which collects and transports wastewater to the WWTF, the Town has begun to expand their collection system to congested and environmentally sensitive areas.

The purpose of this Facility Plan (FP) Update is to investigate and address the following:

- 1. Update of the projected wastewater flows for the 20-year (2035) and 50-year (2065) planning periods.
- 2. Provide re-allocation of flow capacity to study areas as a result of the newly acquired capacity from the Woodland Manor pump station/forcemain acquisition.
- 3. Provide review and evaluation of need for wastewater collection facilities, including:
 - a. delineation of problem areas,
 - b. determination of OWTS rehabilitation (or repair) feasibility, and
 - c. prioritization of sewer needs areas.
- 4. Examine relevant wastewater project financing options available and feasibility of implementation.

1.1 Findings

Chapters 3 and 4 of this Facilities Plan examine the current and expected future conditions in eastern Coventry, with specific interest in the treatment and disposal of wastewater. The investigations performed included review of all available relevant documents. The results of the OWTS survey (**Appendix A**) confirms a preponderance of OWTS problems in several areas of eastern Coventry. These areas have been delineated and were prioritized (Phase I) for sewering in the 1995 FP and subsequent reaffirmations/updates. The conclusion reached through these examinations is that the current system of wastewater disposal through onsite wastewater treatment systems



supporting their designated uses due to pollution. At the time of this Facilities Plan Update, all of the Pawtuxet River in Coventry was able to support all designated uses and was deemed fishable/swimmable.

Although there seems to be a significant increase in the water quality in Coventry, there is no way to estimate the actual number of direct wastewater and stormwater discharges in Coventry without a more comprehensive study.

3.6 Existing Wastewater Collection and Treatment System

3.6.1 West Warwick Regional Wastewater Treatment Facilities

As noted in Chapter 2 of this report, the State's 208 Areawide Water Quality Management Plan (WQMP) recommended that wastewater from Coventry be treated at the West Warwick Regional Wastewater Treatment Facility. This contradicted the previous recommendations for an independent Coventry Wastewater Treatment Facility made by earlier reports ("Preliminary Engineering Survey and Report on Sewerage and Sewage Treatment for the Town of Coventry", Fenton G. Keyes Associates, November 1966, and "Facilities Plan for Wastewater Collection and Treatment Facilities", C.E. Maguire, Inc., 1977). The recommendation of the 208 study has since been implemented, and Coventry is now a member community in the West Warwick regional system.

In 1984, the Town of Coventry signed an Inter-Municipal Agreement (IMA) with the Town of West Warwick, which provided 2.25 mgd (average daily flow) of capacity for Coventry in the West Warwick Regional Wastewater Treatment Facility.

In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain along with its allocated capacity in the West Warwick system. The capacity allocation in the West Warwick system for the Woodland Manor pump station/forcemain is 0.2 mgd. With the existing West Warwick IMA capacity and the addition of the Woodland Manor capacity, the Town of Coventry has 2.45 mgd of average daily flow capacity in the West Warwick Regional WWTF. Future IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

The West Warwick Regional Wastewater Treatment Facility is located off Pontiac Avenue, in the northeast corner of West Warwick. The treatment facility discharges treated effluent to the Pawtuxet River. The facility can discharge an average daily flow of 10.5 mgd (peak flow of 25.34 mgd). West Warwick's facility consists of an activated sludge treatment process, along with a biological activated filter and UV disinfection.

The West Warwick facility currently has the equipment to properly accept septage for treatment. However, at this time no septage is accepted at the facility. The IMA between West Warwick and Coventry has a stipulation that would allow Coventry to dispose of septage at the facility if it were to be accepted from any other communities (including West Warwick).



Development Corp. entered into an agreement with West Warwick to allow the discharge of 200,000 gallons per day to the West Warwick system. Since the construction of the Woodland Manor force main, the pipeline owners have allowed several pressure connections along the length of Tiogue Avenue. These connections have typically been to commercial establishments with severe OWTS problems. Such connections were approved by both West Warwick and Coventry (whose plant capacity was utilized for the connections).

Up until December 2013, this was a privately owned and operated sewer system, separate from the Town of Coventry system, and designed to provide sewer service to an area within eastern Coventry. In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain along with its allocated capacity in the West Warwick system (future IMA revisions will be needed to address officially allocating this capacity to the Town).

Two assessments had been performed on the pump station and forcemain, and were reviewed by the Town prior to the acquisition of the infrastructure. The assessment performed by DiPrete Engineering can be found in **Appendix K**. The other assessment performed by Fuss & O'Neill is with the Town's Engineer. These assessments outlined recommended repairs and upgrades to the pump station. It is recommended the Town perform the repairs/upgrades as part of their yearly infrastructure maintenance plan.

In addition, Weston & Sampson Services has been contracted by the Town to operate and maintain the system since the acquisition. Flow records from the station can be found in **Appendix L**.

3.6.2.h Contract 03-01

The Contract 03-01 sewer project was constructed in 2004 by the Town of Coventry to service portions of Tiogue Avenue and Washington Street. This contract connected the system to the Sandy Bottom Road pump station, built under Contract 03-02 by the Town of Coventry. The connection to the pump station under the Pawtuxet River was by a depressed sewer made up of a series of ductile iron pipes (3 barrels - one 16-inch and two 12-inch pipes). Two 12-inch ductile iron force mains extend from the pump station to the intersection of Washington Street and Knotty Oak Road (approximately 2,500 feet). A 30-inch PVC gravity sewer pipe extends from the intersection of Washington Street and Knotty Oak Road to the intersection of Washington Street and Pulaski Street (approximately 6,100 feet). A 24-inch PVC gravity sewer extends from the pump station to approximately 3,000 feet west along Tiogue Avenue. This line connected to the previously "dry" sewer line installed in Hopkins Hill Road, and allowed for the activation of that sewer line.

As part of this project a flume/flow meter vault was installed to monitor and track flows from the interceptor into West Warwick. These flow records can be found in **Appendix L**. The existing telephone line communications system to send out the flow meter readings has had issues in the past. It is recommended to perform an evaluation on the communication system to see if a more suitable alternative (i.e. radio, high speed internet) is available.



limited OWTS failures, this option is cost effective, but could be considered equivalent to the 'no action' option, since OWTS reconstruction can be left to the individual property owner. For areas where a significant percentage of existing OWTS systems are failing, this option is not as acceptable, since the costs for rehabilitating many systems is significant, and may approach the cost of lateral sewer installation.

5.8.5 <u>Wastewater Collection and Treatment System</u>

In many areas, the installation of a wastewater collection system is the only reasonable alternative for permanently ending the chronic OWTS failure problems.

5.8.5.a Sewer Interceptor System

The previous 1995 FP and 2010 FP Update outlined the three most logical options for proposed sewer interceptor systems. The option previously recommended and constructed is briefly described below. The original interceptor plan from the 1995 FP is included in **Figure 5-1** (Note that since the 1995 FP and 2010 FP Update some of the interceptors have been constructed, see **Figure 3-10** for the current existing interceptors):

Central Pumping Station at Tiogue Avenue and Washington Street Interceptor: This option included constructing a pump station on Sandy Bottom Road. A new force main was installed on Sandy Bottom Road that discharges to a gravity interceptor at the approximate intersection of Washington Street and Knotty Oak Road. This gravity interceptor would then travel east along Washington Street to the intersection of Quidnick Avenue where it would then follow an abandoned railroad bed to Whitford Street and down Pulaski Street to the West Warwick Town boundary.

This option was selected in the previous report based on the proposed benefits and the project's cost effectiveness. Based on this recommendation of the 1995 FP, this option, including the Sandy Bottom Road Pump Station, forcemain and Washington Street interceptor to the West Warwick Town boundary were constructed.

In December 2013, the Town of Coventry acquired the Woodland Manor Estates pump station and forcemain along with its allocated capacity in the West Warwick system. With the existing pump station and forcemain infrastructure already being installed, there is potential to use this pump station/forcemain to sewer adjacent areas previously eliminated or deemed to be not cost effective to sewer due to location (i.e. Planning Area N/N-1). Also, as portions of the forcemain may be flowing under gravity conditions, further investigation should be made to assess the feasibility of using portions of Woodland Manor force main to service parcels along Tiogue Avenue where collection sewers have yet to be constructed. Future IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

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In the 2003 FP Reaffirmation, additional wastewater treatment capacity was allocated for two proposed developments (Pine Ridge Subdivision and Center of New England) that would significantly change the original assumption for sewer flow for the parcels. Due to this additional wastewater allocation need, Planning Areas (AA and AB) with less need for sewering were removed and instead it was recommended to continue the utilization of the existing OWTSs.

In the 2010 FP Update, additional wastewater treatment capacity was allocated for multiple proposed developments that significantly changed the original assumption for sewer flow for the parcels, and two industrial properties (Clariant Corporation and Rhodes Technologies) that were granted connection to the system, that previously had a private WWTF and were unaccounted for in previous FP's allocated wastewater treatment capacity. As part of the 2010 FP Update, Planning Areas AF, AD, Y and portions of Planning Areas AE, N, O, X and Z with less need for sewering were removed and instead it was recommended to continue the utilization of the existing OWTSs.

As part of this FP Update, the additional capacity obtained from the purchase of the Woodland Manor forcemain and pumping station (0.2 mgd) has caused an increase in the wastewater treatment capacity in West Warwick. The additional capacity from the Woodland Manor forcemain purchase combined with the amount of wastewater flow Coventry originally had capacity for in their existing IMA with West Warwick, provides the Town with a total wastewater treatment capacity of 2.45 mgd in the West Warwick system. Future IMA revisions will be needed to address officially allocating the Woodland Manor capacity to the Town, however this additional capacity is not required for projected wastewater flows until 2065, see **Table 4-5** and **Appendix B**.

As part of the selected plan areas adjacent to the Woodland Manor pump station and forcemain that were previously ruled out or eliminated due to conventional sewer construction feasibility were analyzed with regards to this recently acquired infrastructure. Also, a small area to the southwest of Planning Area N that was not included in the original "sewered" area plan was analyzed to determine the potential need for sewering.

6.1.2 Revised Recommended Plan

The revised recommended revisions to the 2010 FP Update sewering plan are described below and include the addition of properties in Planning Area N previously removed in previous FP Update and inclusion of an area to the southwest of Planning Area N that was not originally included in the original "sewered" area plan, but is in a location that was determined to have a need for sewering.

Information collected for each Planning Area to determine sewer needs is summarized in **Table 6-1**. Based upon this information, a new recommended sewer plan can be established. **Figure 6-1** shows this revised sewer plan, and the areas that are recommended for removal. It should be noted that the full or partial removal of an area does not mean that area will never receive municipal sewers. Circumstances could arise that cause a Planning Area to be reinstated to the recommended plan for sewering, such as a sudden increase in need or increased available wastewater treatment capacity obtained by the Town. These circumstances will continue to be monitored in future planning exercises and changes made based upon the findings.



- 1. Inventory of critical assets that are part of the infrastructure project;
- 2. Evaluation of the condition and performance of inventoried assets or asset groupings;
- 3. Certification that the recipient has evaluated and will be implementing water and energy conservation efforts as part of the project/plan; and
- 4. Plan for maintaining, repairing, funding, and as necessary, replacing infrastructure constructed.

The FSP pertains only to the assets/infrastructure being constructed as part of the project receiving SRF funding. However, the FSP's developed should be considered "living documents" that are meant to be reviewed, revised, expanded and implemented as part of the on-going operation and management of the Town's system. It is recommended the Town create and update their FSP prior to the implementation of future sewer projects.

7.2 Implementation Plan

This section discusses the steps necessary to assure proper implementation of the recommended plan. Included is a discussion of the administrative and institutional responsibilities for implementation, as well as a list of specific implementation steps and a preliminary implementation schedule. Several items are discussed in detail, including the recommended plan for administration and O&M of the sewer system.

7.2.1 <u>Implementation Responsibilities</u>

The parties responsible for implementation of the recommended plan include the town of Coventry, acting through its Town Council, Town Manager and with the help support of the Town's Sewer Sub-Committee, and the town of West Warwick, acting through its Town Council. The town of Coventry has jurisdiction over the construction and operation of a sewer system within the town of Coventry. The town of West Warwick has jurisdiction over the Regional Wastewater Collection System and Treatment Facilities located within the town of West Warwick.

The existing intermunicipal agreement between Coventry and West Warwick, included as **Appendix I** to this facilities plan, outlines the responsibilities of Coventry and West Warwick as they relate to the construction and operation of a wastewater collection system in Coventry. The financial acceptability of the wastewater facilities plan is principally the concern of the town of Coventry (acting through its Town Council). A majority of the financial responsibilities of Coventry to West Warwick for the construction of regional system components to date have been met. Payment of Coventry's share of remaining and future costs for the construction of regional system components are the only financial concern of West Warwick. The construction of sewers in Coventry is solely the financial responsibility of the Town of Coventry. Currently the elected Coventry Town Council is the acting deciding body for the Town. The Coventry Town Council currently has responsibility for the planning, constructing, financing, administration, operating and maintaining of all the Coventry wastewater collection system. The financial acceptability of the recommended sewer system will therefore be decided by the Town Council of Coventry.

Per the IMA agreement, the agreement should be reviewed annually by both parties and any necessary revisions should be negotiated. In addition, revisions to the IMA with West Warwick will be needed to address officially allocating the Woodland Manor



capacity to the Town. This allocation of capacity may also change the responsibilities of the cost share for future regional system components.

The Coventry Sewer Sub-Committee (CSSC) was created in previous years as an advisory board that could provide guidance and recommendations to the Town Council to vote on for implementation. Items relating to planning, construction or connection into the municipal system are first heard by the CSSC, and then a recommendation is made to the Town Council to vote on.

While the O&M of the sewer system is the responsibility of the Town Council, the Coventry Department of Public Works (DPW) is designated by the Town Council to provide the necessary O&M to the sewer system.

Current sewer users in Coventry are billed user charges by both the Town of Coventry billing department and also by West Warwick. Users receive two billings from each municipality. This has led to confusion from residents and the unintentional non-payment of the bills. In order to remedy the confusion Coventry has decided to combine the West Warwick user charges, with the Coventry user charges and issue one single bill to the users. Coordination is on-going between both Coventry's and West Warwick's sewer billing entities and implementation of this billing process is expected to take place for the next fiscal year.

The implementation responsibilities of Coventry and West Warwick are summarized as follows:

Town of Coventry:

Following approval of this facilities plan, the Town of Coventry should take action to assure:

- the appropriation of the funds and the completion of design and construction of the recommended plan;
- the continued review and update as needed to the recently adopted sewer ordinance;
- the continued review and update as needed to the existing intermunicipal agreement with West Warwick. This includes the revisions needed to officially allocate the Woodland Manor capacity to the Town;
- the continued administration, operation and maintenance of the sewer system (including an approved system of sewer user charges);
- and review the IMA with West Warwick annually to revise/negotiate changes as necessary and ensure it is fair to both parties.

The completion of these implementation tasks will require appropriate actions by specific town authorities, including the Town Council, the Town Manager, the Director of Public Works, the Director of Planning, the Finance Director and the Tax Assessor.

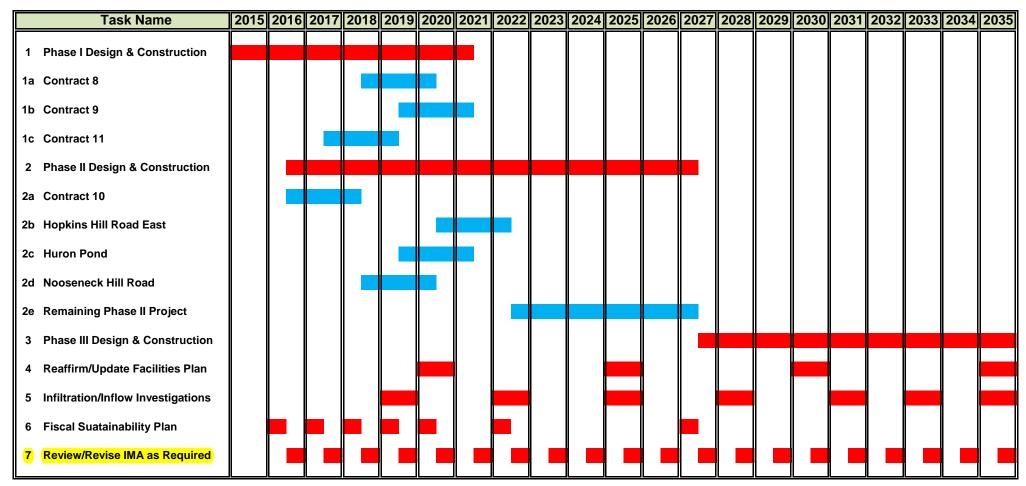
West Warwick:

The Town of West Warwick should take action to assure the proper administration, operation and maintenance of the regional wastewater facilities.

The final approval of this wastewater facilities plan, should meet no opposition from sources outside of Coventry. The acceptability of this facilities plan to the Town of



Figure 7-1 Implementation Schedule



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3.6.2.i <u>Contract 03-02</u>

The Sandy Bottom Road Pump Station was constructed under Contract 03-02 concurrently with the gravity sewers and force main in Contract 03-01. The Sandy Bottom Road Pump Station is a custom designed 3 level pump station with separate dry and wet process areas. The pump station was constructed with 2 pumps initially, but was designed for the addition of two larger pumps such that the future capacity of the upgraded station will be sufficient to handle flows from the majority of the sewered areas in eastern Coventry. The location and elevation of this station was selected to allow gravity sewer service to most of the areas along the South Branch of the Pawtuxet River.

The Sandy Bottom Road pump station includes sewage grinders in the wetwell area, and the station discharges through a dual 12-inch force main to allow for significant variations in design flow rates. The station is equipped with a flow meter and enhanced instrumentation and control (I&C) system.

The Town currently contracts out the operation and maintenance services for the station. The operation and maintenance service contract includes responding to any alarms/emergencies at the station and to repair the equipment as necessary to ensure proper operations.

This station is presently equipped to handle initial design flows from the Coventry system, including flows from the Amgen facility. The station will need to be upgraded with one or more additional or larger pumps as the service areas outlying from Tiogue Avenue, Hopkins Hill Road, and Main Street are sewered.

Flow records from the station have been included in **Appendix L**. These records show that the current pumps are able to handle the flows experienced at the station. At this time a pump capacity upgrade is not recommended. The flows should be monitored, and once flows consistently reach 80% of the station's capacity, an upgrade should be performed to the station.

3.6.2.j Contract 03-03

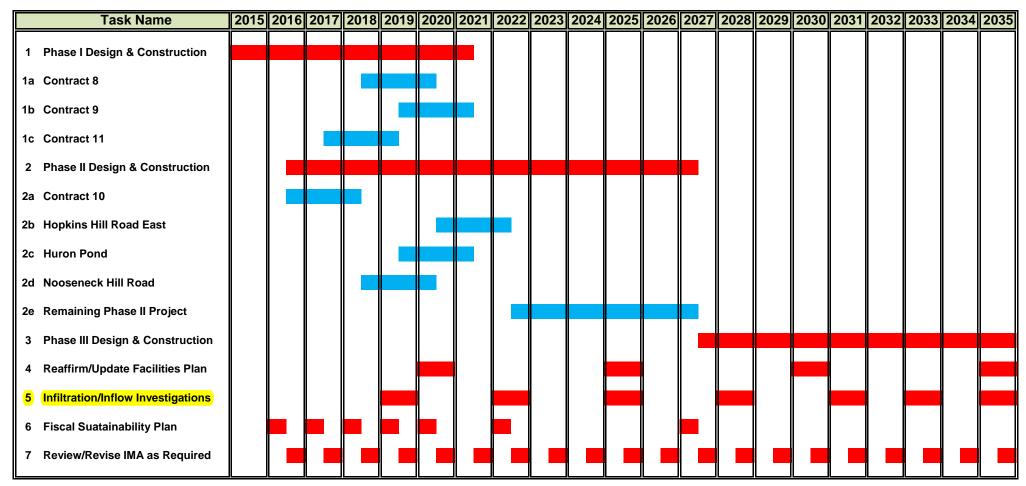
The Hopkins Hill Road force main was constructed in 2006 by the Town of Coventry to connect the West Greenwich Technology Park with the existing gravity sewer in Hopkins Hill Road. It consists of approximately 2,500 feet of 12-inch ductile iron force main from the Coventry / West Greenwich town line and 971 feet of 8-inch ductile iron force main on Hopkins Hill Road.

3.6.2.k Contract 4

The Tiogue Avenue gravity sewer system was constructed in 2007 by the Town of Coventry to provide service to more of Tiogue Avenue and Ramblewood Estates, a mobile home park in Coventry. It consisted of approximately 2,900 feet of 18-inch PVC pipe along Tiogue Avenue to Ramblewood Estates, 1,200 feet of 18-inch PVC pipe in Morningside Drive, 900 feet of 18-inch PVC pipe in "D" Lane, 500 feet 18-inch PVC pipe in Monroe Drive and 1,000 feet of 18-inch ductile iron pipe along a cross country portion. The project also includes 8-inch PVC lateral pipes in Anthony Street (820 feet) Fairview Avenue (1,270 feet), Ray Street (580 feet) and Wood Street (1,125 feet).



Figure 7-1 Implementation Schedule



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Implementation of the water conservation program will help reduce Coventry's wastewater flows, and therefore the costs of transmitting and treating the wastewater.

4.3.3.b Infiltration/Inflow (I/I) Reduction

To date no studies of infiltration/inflow (I/I) problems have been conducted on the sewer pipelines located in Coventry. Since no study has been completed, an accurate estimate of the volume of I/I entering the system cannot be made. Due to the relatively recent age of the Coventry Sewer System, it is assumed that excessive I/I (i.e. more than 120 gpcd infiltration and 275 gpcd inflow) does not exist. However, it is recommended that the Town begin plans for I/I studies/investigations on areas in Town with older sewers constructed in the 1980s (i.e. Hopkins Hill Road, North Road Terrace, New London Turnpike). Any sources of I/I discovered in the I/I investigations should be eliminated.

4.3.3.c Industrial Pretreatment Program

There are several industrial users currently connected to the system. The wastewater discharged by these users is regulated by the West Warwick Industrial Pretreatment Program (IPP). The intent of this program is to achieve the objectives of the U.S. EPA's National Pretreatment Program. The West Warwick IPP was approved by the EPA on September 9, 1983 (most recent Code Ordinance update in 1990), and is currently in compliance with RI-DEM regulations.

As the Coventry wastewater collection system expands in the future, the West Warwick IPP will continue to govern industrial users of the sewer system. The IPP will be modified by West Warwick, as needed, to maintain compliance with state and federal pretreatment requirements.

4.4 Future Planned Sewer Construction Projects

Based on previous recommendations from the 1995 FP, existing sewer construction projects have been built and six additional proposed sewer construction projects are in the preliminary planning phase to be built. These six additional projects (Contracts 8, 9, 10, 11, Hopkins Hill East, and Huron Pond) have been submitted as part of the RIDEM's Fiscal Year (FY) 2015 Priority Determination System for SRF funding, as described in Chapter 7 of this report. In addition, there is an area of need identified in this report that will be evaluated for sewering in the future (Nooseneck Hill Road Sewer Project). The submittal for this program is attached in **Appendix G.** The existing projects have been described in Chapter 3 and the eight proposed projects are described as follows. Please note that the contract numbering is only for discussion purposes, and does not mandate the order of implementation. A location plan of these projects can be seen in **Figure 4-3**.



Based upon updated information obtained for this report, the need to serve this area by means of an off-site wastewater management solution exists. Therefore, the recommendation for this area to be included in the Phase II sewer program is confirmed.

6.1.2.0 Planning Area O

Planning Area O was recommended for sewering as part of the 1995 FP report. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTSs and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The majority of wastewater from this area is proposed to flow to the Washington Street Interceptor via a pump station to be constructed. This area was proposed to be sewered as part of the Phase III sewer program, meaning the area was deemed to be poor for OWTS construction, but that other areas (Phase I and Phase II areas) were deemed either to have a greater need for sewers or their locations were such that sewering was more economically feasible.

Based on information in the 2010 FP Update, it was recommended that a portion of the parcels in this area that would require a pump station to reach the Washington Street Interceptor were removed from the sewering plan, in favor of the continued use of existing OWTSs for wastewater disposal (see Chapter 6 of the 2010 FP Update for more detailed information). Upon the review of this area as part of this FP Update, the concerns over economic feasibility for sewer construction, and the relatively low occurrence of OWTS repairs from 2008-2014 (7% of the removed parcels, **Appendix A**) are still present and the recommendation to remove the selected parcels from the sewering plan remains.

6.1.2.p Planning Area P

Planning Area P was recommended for sewering as part of the 1995 FP, 2003 FP Reaffirmation and 2010 FP Update reports. This was due to certain economic and on-site restrictions prohibiting properly functioning OWTS and justifying the need to provide the parcels with an off-site wastewater management solution (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). The wastewater from this area is proposed to flow through the existing Washington Street Interceptor by gravity into West Warwick. This area was proposed to be sewered as part of the Phase I sewer program, meaning the area was deemed to have the greatest need in the Town for an off-site wastewater management solution.

Based upon updated information obtained for this report, the need to serve this area by means of an off-site wastewater management solution still exists. Therefore, the recommendation for this area to remain in the Phase I sewer program is confirmed. Sewers have been installed to serve parcels adjacent to Washington Street, and the remaining parcels in this area will be served as part of Sewer Construction Contract No. 8. The estimated date of commencement for the project is March 2018, based upon the 2015 Priority Determination System's Project Information Sheets submitted to RI-DEM.



manage their wastewater (see previous Chapters and the 1995 FP for a more detailed evaluation of this area). This alternative was recommended because many lots in this area are undersized for conventional OWTS use; however, the remote location makes sewering this area through connection to the municipal sewer system economically in-feasible. The 1995 report recommended that localized collector sewer systems be installed for restrictive lots and that the systems transmit the wastewater from these parcels to a community OWTS for disposal.

Based upon updated information obtained for this report, the need for this area to be served by an off-site wastewater management solution still remains economically in-feasible option. Therefore, the recommendation for this area to remain excluded from the sewer program is confirmed.

6.1.2.ii Planning Area Al

Planning Area AI was not recommended for sewering as part of the 1995 FP report; it was instead recommended that this area continue to treat their wastewater on-site through the use of OWTSs (see previous and the 1995 FP for a more detailed evaluation of this area). Removal of this area was recommended to allow wastewater allocation to areas with a greater need for sewers.

Based upon updated information obtained for this report, the need for this area to be served by off-site wastewater management solution remains low and the projected flows for the area are better allocated to areas with greater need. Therefore, the recommendation that this area remain excluded from the sewer program is confirmed.

Based upon needs data, including OWTS repair information obtained from RI-DEM, development density and GIS mapping, the Planning Areas that were removed from the recommended sewer plan in previous FPs, FP Reaffirmations and FP Updates were determined to have the least need and greatest sewer construction difficulty and associated cost of the remaining areas to be sewered. OWTS information, presented in Chapter 3, show that these areas experience low to moderate OWTS problems in comparison to the remaining Planning Areas. Also, with the exception of Area Z, these Planning Areas were in the Phase III sewer construction, based on the 1995 Facilities Plan. Phase III construction represented areas with the least amount of sewering need, and areas where either sewer construction may be difficult or where Phase I and Phase II sewers needed to be built before sewer access could be obtained. Since Phase I sewers have yet to be completed, the Phase III sewers are still in the conceptual phase and given the current rate of the sewer installation, it may still be several years away from completion.

6.2 Recommended Sewer Collection System Cost Estimate

The cost of installing conventional sewer collection systems in the study areas for which they have been identified as a feasible option have been generated as part of this study. The detailed collection system costs are based on a preliminary layout of sewers on town assessor's maps, with the aid of topographic mapping prepared as part of the 1966 Keyes report. The estimated sewering costs for each study area are shown on **Table 6-2**. A detailed street by street breakdown of these costs is included in **Appendix F**.



7 ARRANGEMENTS FOR IMPLEMENTATION

7.0 General

The final step in the facility planning process, after the alternatives have been evaluated and the final plan has been selected, is to begin implementation of the selected wastewater management plan. As part of the 1995 Facilities Plan, 2003 FP Reaffirmation and 2010 FP Update, the selected plan at that time began implementation based on the recommendations of this section. A three phased recommended sewer plan was created. Currently, Area U was completely served by the municipal sewer and Areas A, B, F, G, I, J, K, L, N, O, P, Q, R, S, V, W and AE have been partially served by the municipal sewer based upon that recommended sewer plan. Future sewer construction contracts 8, 9, 10, 11, Hopkins Hill Road East, Huron Pond, and Nooseneck Hill Road Sewer Projects have been proposed to sewer additional Phase I and Phase II sewer areas. Contract 9 and 11 will completely serve Area G, , Contract 8 will complete Area P, Contract 10 will complete Area C, Hopkins Hill Road East will serve approximately 60% of Area K (184 parcels), Huron Pond will serve parcels in the northern portion of Area J and the Nooseneck Hill Road Sewer Project will serve a portion of Area N and all of Area N-1. Once the completion of Contracts 8, 9 and 11 occur all Phase I recommended sewers will be constructed. The remaining proposed sewer contracts serve areas in the Phase II recommended sewer program. As part of this report, the implementation of this revised selected three-phased plan, as discussed in Chapter 6 of this report, will be reviewed.

The major factors which must be addressed to continue the wastewater management plan are: to identify the necessary implementation steps, including institutional responsibilities, system operation and maintenance requirements and an implementation schedule; and to establish a financial plan to fund the recommended improvements. The financial plan identifies methods for financing the costs associated with the project, including system construction financing, administration costs and yearly system operation, maintenance and replacement (OM & R) costs. These items are discussed in detail in the following sections.

7.1 Financial Plan

Previous sewer programs prior to the 1995 Facilities Plan were rejected by voters for various reasons, including the costs involved with the system construction. For this reason, perhaps the most important implementation issue to be addressed is the acceptability of financing of the recommended plan. A financial plan for a wastewater collection system must include a system for financing system construction (capital) costs, as well as annual system operation and maintenance (O&M) costs. Since a phased sewer construction program is selected, considerations for financing capital and annual costs for each phase of the recommended system construction must be considered. The financing of construction and O&M costs are emphasized in the following discussions.

7.1.1 Capital (Construction) Costs

Chapter 6 included a discussion of the estimated capital costs associated with each phase of the recommended sewer construction. Also discussed were Coventry's share of capital costs associated with improvements to the West Warwick Regional



the current assessment method and through sewer user charges (as discussed later in this chapter).

7.1.6 Future Phase Construction Cost Allocation

The cost of constructing the continuing and future phases of the recommended plan should also be considered in any proposed financing system, since financing used for Phase I will set a precedent for future construction. The estimated costs for construction of the recommended Phase II and Phase III sewer system, as presented in Chapter 6 and **Appendix F**, are summarized in **Table 7-2**. Sewer construction costs were obtained from actual bids by contractors on similar type projects. The costs do not include Phase I sewer construction costs which are included in **Table 7-1**. As noted for Phase I costs, the costs for West Warwick regional projects are not included in this discussion, but are discussed separately later in this chapter.

TABLE 7-2
SUMMARY OF PHASE II & III CAPITAL CONSTRUCTION COSTS

Proposed Sewer Construction Projects							
Phase II							
Project Description	Total Project Construction Cost	Less Grants	Total Local Cost				
Contract 10 – East Shore Drive Area	\$2,120,000	None	\$2,120,000				
Hopkins Hill Road East Sewer Project	\$2,250,000	None	\$2,250,000				
Huron Pond Sewer Project	\$2,110,000	None	\$2,110,000				
Nooseneck Hill Road	\$3,300,000	None	\$3,300,000				
Totals	\$9,780,000						

Remaining Sewer System							
	Phase III	Total					
Lateral Sewers	\$35,270,000	\$9,970,000	\$45,240,000				
Interceptors	\$4,230,000	\$630,000	\$4,860,000				
Pump Stations and Forcemains	\$2,400,000	\$950,000	\$3,350,000				
Totals	\$41,900,000	\$11,550,000					

7.1.7 West Warwick Regional System Costs

Chapter 6 included a summary of Coventry's share of costs of West Warwick regional projects. These costs are for projects completed to date as well as for planned projects. As discussed previously, Coventry has paid over \$10.8 million to date to West Warwick for their share of the improvements to the regional facilities that were designed and constructed to serve Coventry. The West Warwick Treatment Plant is currently undergoing an upgrade to reduce the phosphorus in the facilities effluent. The estimated cost of this upgrade is \$12.5 million. Coventry's share of the final total project cost is 23% per their IMA agreement.



- 1. Inventory of critical assets that are part of the infrastructure project;
- 2. Evaluation of the condition and performance of inventoried assets or asset groupings;
- 3. Certification that the recipient has evaluated and will be implementing water and energy conservation efforts as part of the project/plan; and
- 4. Plan for maintaining, repairing, funding, and as necessary, replacing infrastructure constructed.

The FSP pertains only to the assets/infrastructure being constructed as part of the project receiving SRF funding. However, the FSP's developed should be considered "living documents" that are meant to be reviewed, revised, expanded and implemented as part of the on-going operation and management of the Town's system. It is recommended the Town create and update their FSP prior to the implementation of future sewer projects.

7.2 Implementation Plan

This section discusses the steps necessary to assure proper implementation of the recommended plan. Included is a discussion of the administrative and institutional responsibilities for implementation, as well as a list of specific implementation steps and a preliminary implementation schedule. Several items are discussed in detail, including the recommended plan for administration and O&M of the sewer system.

7.2.1 Implementation Responsibilities

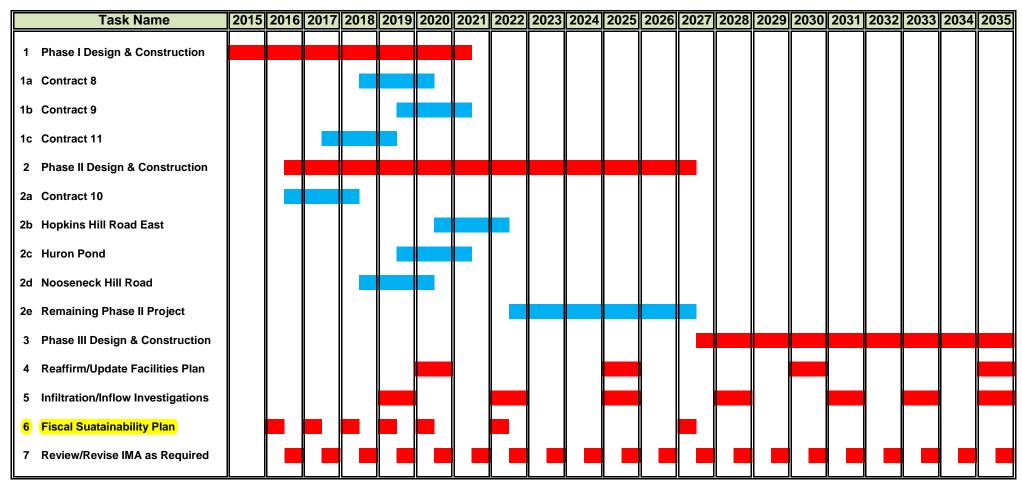
The parties responsible for implementation of the recommended plan include the town of Coventry, acting through its Town Council, Town Manager and with the help support of the Town's Sewer Sub-Committee, and the town of West Warwick, acting through its Town Council. The town of Coventry has jurisdiction over the construction and operation of a sewer system within the town of Coventry. The town of West Warwick has jurisdiction over the Regional Wastewater Collection System and Treatment Facilities located within the town of West Warwick.

The existing intermunicipal agreement between Coventry and West Warwick, included as **Appendix I** to this facilities plan, outlines the responsibilities of Coventry and West Warwick as they relate to the construction and operation of a wastewater collection system in Coventry. The financial acceptability of the wastewater facilities plan is principally the concern of the town of Coventry (acting through its Town Council). A majority of the financial responsibilities of Coventry to West Warwick for the construction of regional system components to date have been met. Payment of Coventry's share of remaining and future costs for the construction of regional system components are the only financial concern of West Warwick. The construction of sewers in Coventry is solely the financial responsibility of the Town of Coventry. Currently the elected Coventry Town Council is the acting deciding body for the Town. The Coventry Town Council currently has responsibility for the planning, constructing, financing, administration, operating and maintaining of all the Coventry wastewater collection system. The financial acceptability of the recommended sewer system will therefore be decided by the Town Council of Coventry.

The Coventry Sewer Sub-Committee (CSSC) was created in previous years as an advisory board that could provide guidance and recommendations to the Town Council to vote on for implementation. Items relating to planning, construction or connection into



Figure 7-1 Implementation Schedule



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Intergovernmental Review Contract List

Name	Misc1	Misc2	Misc3	Address	City State Zip
Mr. Christopher J. Raithel	RI Department of Environmental Management	Division of Fish and Wildlife	Great Swamp Field Headquarters	277 Great Neck Road	West Kingston, RI 02892
Ms. Nancy Hess	Principal Environmental Planner	RI Statewide Planning Program		One Captol Hill	Providence, RI 02908
Mr. Robert A. Smith, P.E.	Deputy Chief Engineer	RI Department of Transportation		Two Capitol Hill, Rm. 224	Providence, RI 02903-1124
Mr. Edward F. Sanderson, Executive Director	State historic Preservation Office	Historical Preservation & Heritage Commission	Old State House	150 Benefit Street	Providence, RI 02903-1029
Mr. John Brown	Historic Preservation Officer	Narragansett Tribal Historic Preservation Office		4425 South County Trail	Charlestown, RI 02813
Mr. Grover J. Fugate, Executive Director	Coastal Resources Management Council	Oliver H. Stedman Government Center		4808 Tower Hill Road, Suite 3	Wakefield, RI 02879-1900
Mr. Christopher Modisette	State Resource Conservationist	Natural Resources Conservation District		60 Quaker Lane, Suite 40	Warwick, RI 02886
Mr. Christopher Boelke	Field Office Supervisor	DOC/NOAA/NMFS/NERO		55 Great Republic Drive	Gloucester, MA 01930
Mr. Joseph Antonio	Senior Environmental Scientist	RI Department of Environmental Management	Office of Customer & Technical Assistance	235 Promenade Street	Providence, RI 02908

tel: 978-532-1900 fax: 978-977-0100 www.westonandsampson.com

engineering, energy, planning, permitting, design, construction, operation, maintenance



Town of Coventry, Rhode Island W&S Project No. 2140605.A

March 25, 2016

- «Name»
- «Misc1»
- «Misc2»
- «Misc3»
- «Address»
- «City_State_Zip»

Re: Intergovernmental Review Request

Facilities Plan Update - Coventry, RI

Dear «Name»

On behalf of the Town of Coventry, Rhode Island, Weston & Sampson, Inc. is informing you of the impending submittal of an Update to the Town's Wastewater Facilities Plan (FP). This letter is to notify your department of the submittal provide a brief background of the changes incorporated into the FP Update and allow you to request a copy of the FP Update document for review, if your department has any questions/comments.

The original FP that this document is updating was approved to RI-DEM May 1995, with a Reaffirmation approved in 2003, and a previous update approved in 2009. This FP Update specifically addresses updated planning area projected wastewater flows, update of the current status of the Town's sewer program. This includes the additional infrastructure and associated capacity in the West Warwick Treatment Plan obtained by the Town of Coventry through the purchase of the Woodland Manor residential housing development's sewer system in 2013.

Research was conducted to update pertinent information and to determine the need for off-site wastewater management in the planning areas, as selected in the original 1995 FP. The Town is limited by an inter-municipal agreement (IMA) with West Warwick on the amount of wastewater capacity they own at the West Warwick Wastewater Treatment Facility. With the additional capacity associated with the Town's Woodland Manor sewer system purchase, the Town is proposing on adding an extension to their planning areas (new Planning Area N-1). This new planning area was analyzed based on considering the need for sewers, as well as any environmental and economic impacts incurred by sewering/not sewering the area. This new area is located southwest of existing Planning Area N, and is adjacent to Maple Root Pond. Sewering Planning Area N-1 will allow the extension of sewers to an area that is currently serviced by on-site treatment systems (i.e. septic systems), but has a need for offsite wastewater management solutions.

The attached Figure 6-1 shows the planning areas selected for sewering as part of the FP, as well as planning areas not recommended for sewering based on recommendations in the 1995 FP, 2003 Reaffirmation, 2009 FP Update and this 2016 FP Update.

Please note that the 21 day review period commences upon the receipt of this letter. We are assuming that if no questions and/or comments have been identified in this 21 day review period, then there are

Massachusetts Connecticut New Hampshire Vermont New York Pennsylvania New Jersey South Carolina Florida

no concerns with the work under the FP Update within your department.

Planned draft submittal of the FP Update to RI-DEM is being made March 28th, and final submittal planed within the following months once all review comments have been addressed. If you or your department has any concerns, please request a copy of the FP Update that will be submitted to Mr. Art Zeman, at the RIDEM Office of Water Resources for review.

Please contact either myself (800-726-7766 x2408) or Tim DeGuglielmo (x2421) with any questions concerning the intergovernmental review of the Coventry Wastewater Facilities Plan Update.

Very truly yours, WESTON & SAMPSON ENGINEERS, INC.

Tim DeGuglielmo, P.E. Project Manager

Enclosures

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Department of Transportation Two Capitol Hill Providence, RI 02903

Office 401-222-2450 Fax 401-222-3905

April 22, 2016

Tim DeGuglielmo, P.E., Project Manager Weston & Sampson Engineers, Inc. Five Centennial Drive Peabody, MA 01960-7985

Subject:

Town of Coventry Wastewater Facilities Plan Update

Intergovernmental Review Request

Dear Mr. DeGuglielmo:

As requested, our office has reviewed your letter (attached) and the corresponding figure outlining the areas selected for proposed sewering. You indicate in the letter that the Update to the Town's Wastewater Facilities Plan is for the extension of existing sewers into areas that are currently serviced by on-site treatment systems.

With respect to the areas selected for sewering, our only requirement is that a Utility Permit(s) from the Rhode Island Department of Transportation (RIDOT) is required for any work within the State Right-of-Way. This includes any roads that may be owned or maintained by the State. We suggest that you consult with the RIDOT draft 10-year construction located following plan that is on the website: http://www.dot.ri.gov/documents/news/TAC_Submission/RIDOT_2015_TAC_Submission.pdf to determine if there are any proposed RIDOT projects that may affect the Town's Plan. Please note that the Department has a moratorium restricting the installation of utilities in a road for five (5) years after the pavement has been placed, with the exception of emergency situations.

If you have any questions or require any additional clarification, please do not hesitate to contact me or Luanne Nevitt, P.E., at 222-2023, extension 4049 or 4052, respectively.

Very Truly Yours,

Vincent J. Palumbo, P.E.

Attachments

VJP/lkn

cc: Messrs. Fish, Healey, Palumbo (all w/o attachments)

File (w/attachments)

State of Rhode Island and Providence Plantations Coastal Resources Management Council Oliver H. Stedman Government Center 4808 Tower Hill Road, Suite 3 Wakefield, RI 02879-1900

(401) 783-3370 Fax (401) 783-3767

April 5, 2016

Mr. Tim DeGuglielmo, P.E. Weston & Sampson Engineers, Inc. Five Centennial Drive Peabody, MA 01960-7985

Re: Town of Coventry Wastewater Facilities Plan Update – Intergovernmental Review Reference CRMC File 2016-03-113

Dear Mr. DeGuglielmo,

The consulting firm Weston & Sampson Engineers filed with the Coastal Resources Management Council (CRMC) an Intergovernmental Review Request for an update to the Town of Coventry Wastewater Facility Plan. The request and Revised Recommended Sewer Plan were received in this office on March 28, 2016. The CRMC has conducted a review as provided through the Department of Environmental Management Office of Water Resources. The Updated Plan has been prepared to add new sewer service areas within the town presently served by onsite wastewater treatment systems (OWTS).

The CRMC has reviewed the proposed Plan for conformance with the Coastal Resources Management Plan (CRMP) and as to whether the Plan would pose any adverse impact to coastal resources of the state. We have concluded that there will not be an adverse impact to coastal resources, provided the project is constructed, operated, and maintained in strict accordance with the state and EPA rules and regulations that govern such facilities. Based on the information you submitted, the CRMC will not request nor need to review the final Facility Plan Update that will be filed with RIDEM.

Sincerely,

James Boyd

CRMC Coastal Policy Analyst

James Boyd

/kc

cc: Grover J. Fugate, CRMC Executive Director Jeffrey M. Willis, CRMC Deputy Director CRMC File 2016-03-113

Art Zeman, RIDEM

STATE OF RHODE ISLAND AND PROVIDENCE PLANTATIONS



HISTORICAL PRESERVATION & HERITAGE COMMISSION

Old State House • 150 Benefit Street • Providence, R.I. 02903-1209

TEL (401) 222-2678

FAX (401) 222-2968

TTY / Relay 711

Website www.preservation.ri.gov

RIHPHC No. 11606 160504.05

4 May 2016

Tim DeGuglielmo, P.E. Project Manager Weston & Sampson Five Centennial Drive Peabody, MA 01960

Re:

Wastewater Facilities Plan Update

Coventry, Rhode Island

Dear Mr. DeGuglielmo:

The Rhode Island Historical Preservation and Heritage Commission (RIHPHC) staff has reviewed the information provided for the above-referenced project. The Town of Coventry has updated its Wastewater Facility Plan (FP). The FP Update identifies the need for additional infrastructure and an extension of the Town's planning area (Planning Area N-1).

Based on the information provided, the RIHPHC has concluded that the areas identified in the FP have a low potential to contain potentially significant archaeological resources. In order to adequately assess effects on significant architectural resources, the RIHPHC will need to review the locations of any proposed wastewater pump stations.

These comments are provided in accordance with the Rhode Island Historic Preservation Act and Rhode Island General Laws. If you have any questions, please contact Glenn Modica, Senior Project Review Coordinator of this office at glenn.modica@preservation.ri.gov or 401-222-2671.

Very truly yours,

Edward F. Sanderson

Executive Director

State Historic Preservation Officer

Public Hearing Coventry Sewer Sub-Committee Meeting October 12, 2016



AMENDED COVENTRY SEWER SUBCOMMITTEE PUBLIC HEARING

Town Hall Council Chambers 1670 Flat River Road, Coventry, RI Wednesday, October 12, 2016 6:00 pm

1. Meeting call to order

2. Attendance

3. Review of Emergency Evacuation Plan

4. Approval of September 14, 2016 meeting minutes

5. Public Hearing – "Wastewater Facility Plan Update"

6. Adjournment

Glen Skurka Chairman

Leonard Piette, Vice Chairman

John Colaluca

Doug Finegan

Gregory Laboissonniere

Kerry McGee

Tony Raposo

Joseph Spada

Charles Horan

Posted: October 4, 2016



TOWN OF COVENTRY 1670 Flat River Road, Coventry, RI 02816 Tel. (401) 822-9173 Fax (401) 822-9132

October 4, 2016

Kent County Daily Times 1353 Main Street West Warwick, RI 02893

Attn: Sara (Coventry Probate Account #10656)

Please advertise the following legal block ad October 7, 2016.

Dek \$ 61,28

TOWN OF COVENTRY SEWER SUBCOMMITTEE PUBLIC HEARING

The Sewer Subcommittee will conduct a Public Hearing on October 12, 2016 at 6:00 pm in the Coventry Town Council Chambers, 1670 Flat River Road to discuss the "Wastewater Facility Plan Update".

Deborah A. Lavoie, Deputy

TOWN OF COVENTRY SEWER SUBCOMMITTEE PUBLIC HEARING

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Deborah A. Lavoie, Deputy

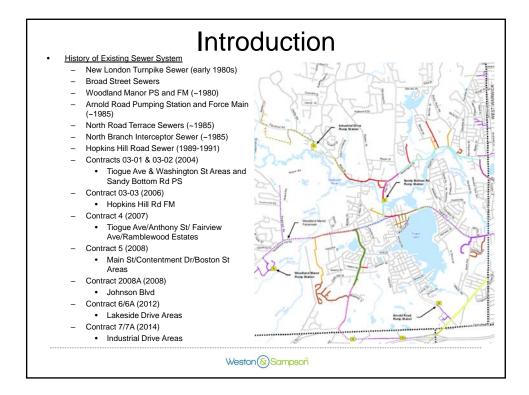


2015/16 Coventry Wastewater Facilities Plan Update

Presented by: Kent Nichols, Weston & Sampson Tim DeGuglielmo, Weston & Sampson

Presented at: Coventry Sewer Subcommittee Meeting October 12, 2016

Weston & Sampson



Facility Plan Introduction

- Facility Plan (FP) to be updated every 5-years for a 20-year future planning period.
 - Last Update in 2015.
- Original Wastewater Studies began in late 1960s to early 1970s
- History of this Facility Plan
 - 1995 Facilities Plan
 - 2003 Facilities Plan Reaffirmation
 - 2010 Facilities Plan Update
- Purpose of this Update is to include any significant changes from previous FP
 - New users
 - Additional Infrastructure Acquisitions (i.e. Woodland Manor)
 - Proposed changes in Town Sewering Plan locations
- Approved FP is required to be eligible for the SRF program.



Timeline

Submittal of Draft FP Update to RI-DEM

March 2016

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RI-DEM issues 30-day Public Notice for Comments

RI-DEM Public Notice for Comments Ends

September 19, 2016

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Public Hearing on FP Update

October 12, 2010

(Sewer Sub-Committee Meeting)

October 19, 2016

RI-DEM Approval

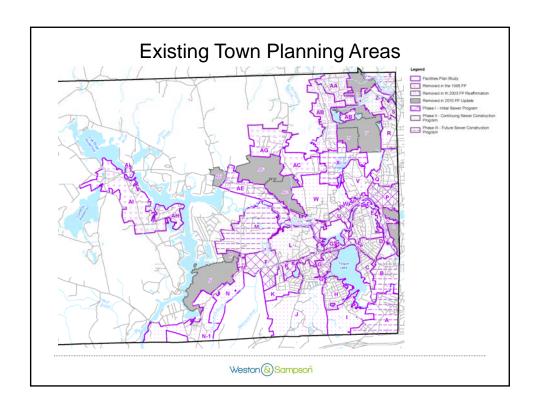
Late October 2016



Changes Included in the 2016 FP Update

- Update/Confirm information from the previous FP document (2010 FP Update).
- Update Wastewater Flow Estimates for the 20-year Planning Period.
- Update the FP to include recently constructed and/or acquired sewer infrastructure.
 - Sewer Contract 6/6A (Lakeside Drive Area).
 - Sewer Contact 7/7A (Industrial Drive Area).
 - Woodland Manor System (Pump Station and Forcemain).
- Proposed utilization additional capacity in the Woodland Manor System to include additional areas of need (i.e. Area N-1 – Nooseneck Hill Road/Mapleroot Village).
- Provide recommendations for the Town's wastewater system moving forward.





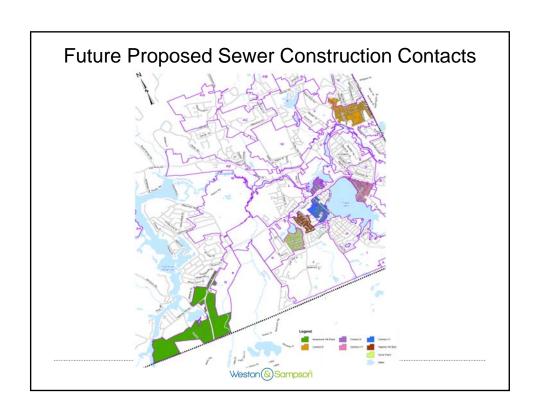
Sewer Flows from Planning Areas for
20-year & Full Buildout Planning Periods

	ADF Flo	ADF Flow (GPD)		ADF Flow (GPD)			ADF Flo	w (GPD)	
Area	20-Year	<u>Full BO</u>	<u>Area</u>	20-Year	Full BO	<u>Area</u>	20-Year	<u>Full BO</u>	
Α	83,355	170,880	N*	2,042	4,205	Z*	45,177	46,476	
В	20,198	55,803	N-1	68,508	70,548	AA	OWTS	(2003)	
С	48,564	51,069	0*	4,271	10,754	AB	OWTS	(2003)	
D	62,814	66,084	Р	175,771	180,580	AC	OWTS	(1995)	
Е	100,485	105,283	Q	95,536	104,266	AD	OWTS	(2010)	
F	110,801	118,662	R	33,394	37,729	AE*	2,590	64,107	
G	66,918	71,838	S	28,586	30,836	AF	OWTS	(2010)	
Н	92,831	98,081	Т	25,079	71,111	AG	OWTS	(1995)	
I	42,389	44,009	U	114,857	121,121	АН	OWTS	(1995)	
J	308,090	313,010	V	83,978	85,943	Al	OWTS	(1995)	
К	71,419	75,589	W	108,503	111,668	WM	66,791	67,688	
L	102,279	108,054	Х*	1,470	60,784	TOTAL = 1,984,818 / 2,413,914			14
М	16,945	66,648	Υ	OWTS	(2010)	L.31A		l Area Removal (20	

Recommendations

- Continue with Sewer Program.
 - Lakeside II/Arnold Road Sewers
 - Quidnick Village Sewers
 - Hopkins Hill East Sewers
 - Huron Pond Sewers
 - Contracts "9", "10", "11"
 - Nooseneck Hill Road/Maple Root Village
 - Additional areas of need
- Review IMA Agreement with West Warwick
- Review "older" areas of sewer system for Infiltration/Inflow potential.
- Continue reviewing/updating assessment/sewer rates as needed.
- Update Facilities Plan (every 5 years)







Weston & Sampson

Town Council Meeting/Work Session January 11, 2016 Wastewater Facilities Plan Update

Town Council Meeting January 11, 2016

EXECUTIVE SESSION - 6:00 p.m.

- 1. Town Manager Recruitment per RIGL 42-46-5 (a) (1)
- 2. Miozzi Consent Judgment KC 2010-1574 per RIGL 42-46-5 (a) (2)
- 3. Imposition of Impact fees pursuant to agreement for the "Highlands" arising from litigation and potential litigation KC CA #03-444 and KC CA #13-5001 pursuant RIGL 42-46-5 (a) (2)
- Imposition of Impact fees pursuant to agreement for the Village Green Condominiums arising from litigation and potential litigation KC CA #03-444 and KC CA #13-5001 pursuant to RIGL 42-46-5 (a) (2)

A motion was made by Councilman McGee seconded by Councilwoman Duxbury to come out of Executive Session. All voted aye.

A motion was made by Councilman McGee seconded by Councilwoman Duxbury to seal minutes of Executive Session. All voted aye.

WORK SESSION – 6:30 p.m.

1, Coventry Landfill Closure Update

Engineer Richard Hittinger updated the Town Council on the landfill closure and gave a power point presentation which included a proposed modification to the plan. Assisting and answering questions along with Mr. Hittinger were Attorney Joseph Farside, representing the town in this matter; Attorney David Graham who represents the PRP group; and Mr. Ed Summerly, design engineer.

Discussion centered around remediation and closure of the landfill, the BUD program and use of a synthetic cap. Mr. Hittinger went on to state that the consent decree for remediation requires that the town and the prp group remediate and close the inactive landfill on Arnold Road, with total cost of the work estimated at seven to ten million dollars. The BUD (Beneficial Use Determination) program was developed to help offset costs and was approved by both the Council and DEM in 2013. The site has been accepting BUD materials for 8 months, but the acceptance rates have been far below what was projected. The PRP group is considering BUD program modification pending tonight's hearing.

Currently DEM approval calls for the installation of a low permeability soil cap, in order to limit surface water infiltration through the cap and also to control storm water runoff and soil erosion. Discussion tonight pertains to upgrading to an impermeable synthetic cap.

Mr. Hittinger went on to explain that one of the significant problems is that we have a total lead acceptance level of 500 parts per million, significantly lower than the Cranston or Central landfills, which have programs like this. The difference is that they both accept up to 2000 parts lead per million, which we would be able to accept if we agreed to put a synthetic cap on after we reach our final grade.

Interim Manager Kerbel added that as part of the contract with DiGregorio, they were charging

\$20.00 a ton. I had a conversation early on with DEM, and it was agreed that there are a couple of issues. Maybe the fee is high and others are charging less, but others are allowed to accept a higher lead level. DiGregorio has reduced their fee from \$20.00 to \$15,00, we are recommending this impermeable cap, which will allow us to take a higher concentration of lead. The bottom line is that the lead content is too low for many of the soils.

At the current pace, closure could take more than ten years. DEM has indicated a willingness to allow soil with higher lead concentration if the soil cap is replaced by a synthetic cap. By changing it should allow closure in less than five years. The proposed design changes include a impervious cap, upgrade of storm water controls at the site and the institution of soil blending and odor monitoring. Cranston landfill has been doing this successfully for five years.

Councilwoman Duxbury is concerned about drainage, especially with the lake nearby. Mr. Hittinger went on to explain the benefits of closure with turf technology where the town will experience enhanced groundwater protection, decreased operation and maintenance costs, enhanced landfill gas and odor control, quicker implementation and become more compatible with solar power end use. It will be more aesthetically pleasing.

DEM's policy with a soil cap limits the lead concentration to a maximum of 500 parts per million. . We initially asked for 2,000 ppm. The low lead concentration of 500 ppm has been limiting some of the soil that is acceptable at the facility. DEM would like to see this landfill remediated and closed in five years.

With the modification, it will first be tested in a very small area under a controlled method. Manager Kerbel said that if the impervious cap has more runoff, that's good news as the runoff isn't going into the landfill but will run off the top. Mrs. Duxbury is also concerned about odor. Councilman Laboissonniere asked where the c & d facilities are and remarked that many years ago there was a facility on Colvintown Road, there was a lot of stuff going in there and he wonders if that particular facility is going to get ramped up again. There was a spontaneous combustion incident there that lasted six weeks. Mr. Hittinger replied that the facilities could be anywhere, but most likely they are in the RI area. This material comes from demo companies. Manager Kerbel stated that this is the reason why we are talking about very localized testing in the beginning. The materials will be tested first before they are accepted. DEM has a list of unacceptable materials and it is the job of onsite people to monitor and make sure testing is complied with. Councilman Laboissonniere asked if there is a vendor list. Mr. Hittinger did not know but Attorney Farside advised that there is a very extensive application process with DEM, so in the end we will know where they came from and what the contents are.

Solicitor Gorham asked how they could have been so far off the BUD projections. Attorney Hittinger said this is a concept that has worked very well for other clients, but not so well here. Besides the economy being an issue, originally we thought we could get the 2000 parts per million, but DEM's policy is that we can only take up to 500 ppm without a synthetic cap. There are not a lot of these projects in RI. Mr. Hittinger added that it was the Solid Waste Division of DEM that said we could not have 2000 ppm and lowered to 500 ppm without the synthetic cap. Cranston can have 2000 ppm because they have the synthetic cap. This is an unwritten policy of DEM, it is not totally fair. If we are going to mimic Cranston, then we are going to have to have a synthetic cap. It is actually beneficial for the town to make this change. Solicitor Gorham understands, but doesn't get why we didn't start with this design and strategy in the beginning.

After completion of remediation, it will require continued storm water maintenance and groundwater monitoring for 30 years.

With the synthetic cap, the lead will be isolated from the rain water. There is much more protection than with the soil cap, as the soil cap allows a small amount of water to go through. The synthetic cap stops all water from going through and the lead stays underneath. He went on to show a comparison of estimated costs, both with the current cap and with a synthetic cap. (See presentation for comparisons)

What is recommended is to submit an application to DEM to include the closure turf cap, and request that soil be acceptable with lead levels up to 2000 ppm and c & d fines. Then, implement a limited, phased trial of c & d fines with perimeter monitoring. The town will have authority to stop acceptance of c & d fines if odors become a problem. Control the placement of c & d fines and high lead soils in a predetermined area of the landfill. Councilman McGee wants to be assured of strict monitoring.

To date, \$1.6 million has been spent on the landfill. President Shibley asked how the initial estimates of \$7 million to \$10, million would change if this is approved and Mr. Hittinger replied there would be a cost increase of about \$1.3 million.

Manager Kerbel added that the town approved a \$5 million bond and has already borrowed \$860,000 of that five million authorization. The ironic part of all of this, when the cost goes up, revenue goes up and the town's out of pocket expenses are less under this program, if everything works right. If it doesn't, then we would have to borrow a lot more of that five million. This is why we want the town to have veto power of the c & d fines.

Councilwoman Duxbury asked the projected time period to finish the project and Mr. Hittinger replied five years. However, she is still concerned about the lead going from 500 ppm to 2000 ppm Mr. Hittinger responded that 2000 ppm is the maximum, the materials may not be that high, yet higher than the 500 ppm. Current we can only accept up to 500 ppm. Mrs. Duxbury feels there may be another idea out there and is not anxious to jump into this without making sure. She would like to wait and see if the reduction in tipping fees has an impact.

Councilman McGee feels much more confident with a barrier being put in there. President Shibley doesn't think it will matter waiting a month or so, they can still continue what they have been doing. If we have to go with the synthetic cap, that's the way we can get that landfill done in five years. Mr. Hittinger said that the application will take about six weeks to prepare.

Dog Park

Manager Kerbel gave a summary of previous discussions about a dog park behind the Town Hall Annex. However, the recommendation tonight is that it be relocated adjacent to the Oliveiri property on Route 117 near the sewer pump station, which is town owned and previously used as a t ball field.

Parks and Recreation Director Jay Primiano submitted a relocation request to the Town Council, requesting construction of a 150 x 100 foot dog park in conjunction with the Dog Park Committee.

Posts and rails from the greenway sewerage project will be repurposed, labor will come from the Parks division and dollars from the "Friends of Coventry Dog Park. One of the benefits to the dog park will be the ability for dogs and owners to socialize and it is within walking distance from more densely populated areas through use of the greenway. The park will service both small and large dogs separately. There will be limited square corners in the park which will diminish threatening dog cornering. As we foresee a potentially greater use of the Town Hall Annex for recreation

programming, we would like to reserve the space at the annex for potential future programs.

The cost to the town will be little to no expense. The Parks Division will provide labor, machinery and fuel to run the machinery and will contribute already stockpiled materials currently stored at Central Coventry Park. The Dog Park Friends will contribute \$3,800.

As far as future costs, dog waste bags will need to be replenished (contributed by Dog Park Friends), Parks and Recreation already cuts and trims the grass in the area and restriping of the parking lot will be completed eventually.

Councilwoman Carlson asked if there will still be room for the horse caravans and Mr. Primiano replied that there is sufficient space. She doesn't want to see the horses frightened by barking dogs. She also asked if the dogs will need to have current licenses and rabies tags, along with monitoring to make sure they are healthy. Mr. Primiano replied that our signage should accommodate that issue. This seems to be a group of people who are really self monitoring. It is possible that we may work with animal control and they could do spot checks from time to time. However, in Charlestown there was never any checks and there were also no problems over a 3 ½ year period.

Mrs. Carlson asked about liability insurance and what would happen if someone gets attacked? Will certain breeds, for example pit bulls, boxers, german shepherds, be allowed to come in? Who is liable? Mr. Primiano believes the Interlocal Trust would cover this. He also does not plan to discriminate against specific types of dog breeds, although that would be Council's choice.

As far as dog waste, there will be receptacles and Parks and Recreation would pick up periodically. In the budget you will see that the expenses will be covered by Dog Park Association; we would be handling the labor aspect of the project.

Councilman Laboissonniere asked whether he has had discussions with abutting neighbors and homeowners. There are a lot of homes over there and dogs do bark. If the neighbors have no problem with it, then he doesn't either, but thinks they do need to be consulted. Mr. Primiano replied that he has had a short discussion about running the program on site and there is a strong desire by the business owner to get more people over there. Eventually there will be a business there.

Councilwoman Carlson asked whether this project needs to go to the Zoning Board and Solicitor Gorham is not sure, will have to look into it. Councilman McGee added that we didn't think there was a need to go to zoning at the previous annex location. He thinks the dog park is a great idea, good location and we will be utilizing our town property. There is already an ordinance requiring that dogs are licensed, and in order to be licensed the rabies shots need to be up to date. He also doesn't think there should be any discrimination of breeds going into the park.

Councilman Laboissonniere asked who maintains the right of way and Mr. Primiano said that as he understands it, there is a 30 foot right of way on the western side of the property abutting the stone wall and it is maintained and plowed by the town. There is really very little development needed, the land is flat, grass is growing and it is in good condition. It is an ideal situation and could be done relatively quickly.

Councilwoman Duxbury thinks this is a good idea, but wants to make sure the operation is monitored, that there are waste bags available, that the waste is picked up and disposed of, that only licensed animals are allowed, who exactly will run the park and if it is the dog park association, are there policies regarding the operation of the park that they will have to follow? Will the town contribute any resourses? Mr. Primiano responded that there may be some collaboration, the

association will continue to raise money and the town will be responsible for the property and cutting the grass, as we do already. Mrs. Duxbury wants to go into this with eyes open and wants to know how problems and issues get resolved if they arise.

Mr. Primiano does not see this as being a high maintenance project. Councilwoman Duxbury suggested speaking with Colonel Macdonald to see if Animal Control can have a plan if they are going to have to play a role in monitoring. She also believes that the people around that area have a right to know about the dog park. I don't have an issue with relocating the park as long as people in the neighborhood are fine with it. I understand the town will be a back up to the dog organization, certainly the town can support this type of thing. Mr. Primiano will report back to council after more details are worked out.

Sewer Facility Plan

Glen Skurka, Chairman of the Sewer Subcommittee and Kent Nichols of Weston and Sampson were present to discuss the sewer facities plan. Mr. Skurka advised that the plan needs to be restructured, as required by DEM. Mr. Nichols gave an update, referring to the handout summary with three maps attached. The plan is kind of a roadmap for the sewers in Coventry. It has already been changed and modified many times, The document tonight intends to show about a 20 year plan for the town. We have already done some pretty amazing things and there is a map included of our existing systems along with additional discussed projects. The town has a lot of capital that you are not using. The attached maps show the assessment of existing conditions on the first map, proposed sewer contracts on the second map and the revised recommended sewer plan on the third page.

He gave an overview of the facilities plan update, the goals of the new update, the current and future flows into the wastewater system and the assessment of future wastewater planning via future sewer contracts including operations, maintenance, and preventative maintenance items along with reviews from the town, Department of Environmental Management, comments and the final submission to DEM.

Coventry still has 9/10's of their capacity at the West Warwick plant. Manager Kerbel indicated that the Council needs to identify an area, as we have the bond money and are paying interest on the money.

Mr. Nichols went on to describe the many different areas outlined on the third map, those in purple as potential areas with some areas removed to dedicate more to economic development.

A few things continued to change since Contract 7, we were going to go on to Contract 8, but did not. However, there are a lot of future areas that can be expanded and part of this plan is to figure out where the needs might have changed for the updated plan. The town now is sitting with a couple of million dollars that needs to be allocated somehow and you need to identify where to go next. Contracts 8 – 10 have been plotted on the map to show us future projects. In addition there are a couple of spots where the town has talked about heading further west than the post office on Route 3, a great development area there. We are here to see what you want to do next. Manager Kerbel agreed that we need to identify a project and spend the money, approximately 2.2 million, and that is the next step for Council, to look at the maps, identify a project, come to a conclusion and get it underway.

Mr. Nichols went on to explain that Contract 8 was stopped because of the costs, with so much rock and ledge in the area. Councilmember McGee, also a member of the Sewer Subcommittee,

advised that combining projects was also discussed due to costs, however, nothing is set in stone.

TOWN COUNCIL MEETING - 7:00 p.m.

Present: Councilman McGee, Councilwoman Duxbury, Vice-President Carlson, President Shibley, Councilman Laboissonniere, Town Manager Kerbel, Town Solicitor Gorham

Pledge of Allegiance Invocation Review of Emergency Evacuation Plan Approval of Town Council minutes December 7 and December 14, 2015

Councilman Laboissonniere referred to the end of the December 7 minutes and asked that the incorrect spelling of his last name be corrected.

Councilwoman Duxbury asked that in the December 14 minutes, on page 8, third paragraph, that the word "trash" be inserted, where she refers to the "new program", so it will read "new trash program".

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to approve minutes as corrected. All voted aye.

President's Comments

President Shibley announced a ribbon cutting ceremony on Friday at 11:00 a.m. at the Pawtuxet River Stabilization site located at the General Nathanael Greene Bridge, having been postponed from December 11, 2015. The ceremony will take place outside, weather permitting.

Open House will be held at the Coventry High School, Regional Tech Career building, on January 16th from 6 p.m. to 8 p.m. New programs will be announced for 2016.

Superior Court Judge Silverstein approved the receiver's petition to sell the Hope Mill. Coventry owns 7.5 acres there and is owed about \$56,000. We hope to see that money and Solicitor Gorham understands that Coventry will be paid.

There is a vacancy on the Coventry Land Trust. If anyone is interested, send in your application to the Town Clerk.

Council District Updates

District 3 Councilman McGee was happy to report that a portion of Blackrock Road has been paved.

Distrtict 5 Councilwoman Duxbury commented that some vehicle thefts have occurred in her district and Coventry Police have increased patrols. Whoever is performing these thefts is not making noise and leaving car doors ajar, so please lock your cars.

There were no reports this evening from District 1 Vice-President Carlson and District 2 Councilman Laboissonniere.

District 4 President Shibley announced that the "Dollar House" on Washington Street has been

razed and the gate house on Tiogue Lake has been vandalized. There was a fire at the plaza where Dragon Palace is located, but due to the rapid response from the adjoining fire district, damage was less severe than it could have been and was mostly smoke and water.

LICENSES

- 1. Renewal of Firearms licenses:
 - (a) Rhode Island Gunworks, 303 S. Main Street
 - (b) Mid-State Gun Co., LLC, 1200 Tiogue Avenue
 - (c) Hawkins Machine Co., Inc., 374 Hopkins Hill Road

A motion was made by Councilman McGee seconded by Councilman Laboissonniere to approve renewals. All voted Aye.

RESOLUTIONS

1. <u>Authorizing the Town Council President to enter into an agreement with the Town Manager</u>

President Shibley announced that the new Town Manager is Mr. Graham Waters, currently a city manager in New Carrollton, MD. He was unanimously selected by the Town Council and will begin employment in Coventry on February 16, 2016.

A motion was made by Vice-President Carlson seconded by Councilman Laboissonniere to approve resolution. All voted Aye.

2. Appointing Tax Assessor for the Town of Coventry

Manager Kerbel announced that the new Tax Assessor, unanimously agreed upon by Council, currently works in Providence and has previously worked in Burrillville and Attleboro, MA. Mr. James Drew is a resident of Exeter.

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to approve resolution. All voted aye.

3. Accepting the actuarial valuation of the Police Pension Plan for FY 17

Manager Kerbel advised that the funding percentage is going up. Although it is still low, it is heading in the right direction. However, the plan is consistent with the funding improvement plan submitted to the State of RI, which in 2012 was 9.9% funded; 10.3% in 2013; 12.9% in 2014 and currently 14.6% in 2015, per Finance Director Thibeault.

A motion was made by Councilman Laboissonniere seconded by Councilman McGee to approve resolution. All voted aye.

4. Adopting borrowing priorities

Manager Kerbel explained that the schedule for the bond requires action by the Council for borrowing that will occur later in the spring. We are borrowing approximately 3.9 million, which includes about \$3.225 million for the road bond, \$150,000 on the automated recycling program, and

approximately \$450,000 for landfill remediation. This is not a final number, we just need authorization. Included in the road bond, there is a policy issue, we will still borrow the maximum of \$3,225 million, the maximum allowed, but in question is whether or not to do the off right of way, off pavement, on a state road, but is part of the RI Infrastructure Bank's priority projects. If you agree to it, we will use some town funds to do some streetscape projects. We need to know if this is a priority or if you just want to use the road bond to pave town roads.

DPW Director Kevin McGee stated that it is \$880,000 for the streetscape; however, our portion would be \$80,000, 10%. We have to decide if it will be done as part of the bond. If we don't do it, we will lose \$800,000 of state money. This is a 10% match.

Mrs. Duxbury agrees, clarifying that it won't take money away from paving roads, except for the 10%. At some point Mrs. Duxbury would like to get a list of what we have done and what the costs of those items have been, in order to see what projects we have completed and what the costs were.

Councilman Laboissonniere feels that this is a great investment. Councilman McGee referred to the automated collection bond 5.5 million and we have about 1.2 million remaining. Finance Director Thibeault indicated that we will not use the whole \$5.5 million; we have only issued what we have used. Councilwoman Duxbury asked if at the end of the year we can do a post audit, look at what Mr. Hoover's original prediction was that this was supposed to pay for itself and see how that compares with what has actually happened? He probably based that prediction on the \$5.5 million, but with \$1.2 million remaining, it exceeds expectations

A motion was made by Councilman McGee seconded by Councilman Laboissonniere to approve resolution. All voted aye.

5. Rescheduling Town Council meeting

A motion was made by Councilman McGee seconded by Vice-President Carlson to reschedule the Town Council meeting from January 25, 2016 to January 26, 2016. All voted aye.

Manager Kerbel explained that next three items are all for approval of appropriations using impact fees. The items are broken, but have a useful life of more then ten years. Each of the items was less than \$10,000. We are recommending approval of these resolutions using impact fees.

- 6. Approving replacement of hot water heater at annex
- 7. Approving purchase of repeater for antennae
- 8. Approving Tiogue Lake Gatehouse Repair

A motion was made by Councilman McGee seconded by Councilwoman Duxbury to approve Resolution numbers 6, 7 and 8. All voted aye.

- 9. <u>Authorizing the Interim Town Manager to sign an agreement regarding "Village</u> Green" Impact Fees
- 10. <u>Authorizing the Interim Town Manager to sign an agreement for Impact Fees for the</u> "Highlands" arising from litigation KC CA #03-444 and KC CA #13-5001

Manager Kerbel asked to consider Resolutions #9 and #10 together. He was authorized to sign an agreement earlier that called for a range of impact fees in Village Green from \$1700 to approximately \$5200; in the Highlands from \$1700 to about \$7600. The solicitor and I have

negotiated with Mr. Mihailidies, owner of the properties. He is looking for certificates of occupancy on about twenty units, twelve in Village Green and eight in the Highlands. He has also agreed to pay \$1700, the lower amount in Village Green and \$4450 in the Highlands. This will result in about \$56,000 or so to the town.

A motion was made by Councilman Laboissonniere seconded by Councilwoman Duxbury to approve resolutions. All voted aye.

PUBLIC HEARINGS

1. <u>Application for new Class B Ltd. liquor license by Leea Cavanaugh dba</u> Greenway Café, 21 Hill Farm Road (formerly Pete's Pizza)

A motion was made by Councilman Laboissonniere seconded by Councilman McGee to open public hearing. All voted aye.

Leea Cavanagh was present and told the Council that she will be open for breakfast and lunch; operating hours will be from 6 a.m. to 3 p.m. She is confident that she will do well with the location being next to the greenway. Council agreed that she has a great location and wishes her luck.

There was no public comment.

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to close public hearing. All voted aye.

A motion was made by Councilman McGee seconded by Vice-President Carlson to approve application. All voted aye.

2. <u>Amending Chapter 153 of the Coventry Code of Ordinances, Licensed Businesses, Section 153-4 Closing hours for asphalt plants and cement plants</u>

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to open public hearing. All voted aye.

Manager Kerbel said what this amendment does is changes and includes the time for processing firewood and mulch including warming up machines and queuing or loading trucks, in the definition of operations. Solicitor Gorham explained that there is one exception and that would be for firewood harvested from one's own property. Then this ordinance does not apply.

Councilwoman Duxbury said that her reasons for this amendment are threefold: The first reason stems from many complaints from residents in the area about noise coming from operations other than asphalt plants; secondly, the police need more definition for enforcement; and thirdly if we have hours of operation that apply to businesses in an industrial park, it doesn't provide a fair playing ground when some businesses have hours and restrictions and some do not. We received feedback from Colonel MacDonald and it is important that the police have the tools to enforce. Chief MacDonald stated that he supports the proposed ordinance with the changes.

There was no public comment.

A motion was made by Councilman Laboissonniere seconded by Councilwoman Duxbury to close public hearing. All voted aye.

A motion was made by Councilwoman Duxbury seconded by Vice-President Carlson to approve ordinance amendment. All voted aye.

3. Amendment to the Zoning Ordinance to allow for reasonable citing of solar energy Facilities

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to open public hearing. All voted aye.

Manager Kerbel pointed out that the recommendations from the Planning Commission have been included in the Council packets. The ordinance has been slightly modified and if you want to accept the Planning Commission recommendations, then you want to vote on the ordinance as amended by the Planning Commission.

Planning Director Paul Sprague advised that the Planning Commission recommended to additionally allow solar powered electrical generating stations on roof mounts in general business zones and industrial zones, the reason being that Planning felt there may be large buildings throughout this town that could accommodate solar on the rooftop, and made the recommendation that Council give consideration to allowing major solar energy in all zones except for Village Main Street Commercial.

President Shibley said that he doesn't see GB 1 on the matrix and Mr. Sprague replied that although there is a GB 1 and a GB, on the matrix it is just shown as GB. Solicitor Gorham asked if there were any other changes to text and Mr. Sprague responded there were not, just changing N (Not permitted) to S (Special Use) on the matrix with the exception of VMC. Only the matrix needed to be changed, no change in verbiage.

There was no public comment.

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to close public hearing. All voted aye.

A motion was made by Councilman McGee seconded by Councilwoman Carlson to approve ordinance with amendments. All voted aye.

4. <u>Transportation Improvement Program and adoption of resolution approving submission of program</u>

A motion was made by Vice-President Carlson seconded by Councilwoman Duxbury to open public hearing. All voted aye.

Manager Kerbel stated that every few years the state requires the town to give input to the transportation improvement program. It requires cities and towns to submit priorities to them. We made our submission on Friday and you have in your packet the road paving priorities of the town including the completion of the trestle trail project and streetscape improvement projects that we talked about. We discussed all this briefly with the legislators at the December 15 meeting. We will see what happens.

There was no public comment.

A motion was made by Councilman Laboissonniere seconded by Vice-President Carlson to close

public hearing. All voted aye.

A motion was made by Councilman McGee seconded by Councilman Laboissonniere to approve resolution. All voted aye.

PUBLIC COMMENT

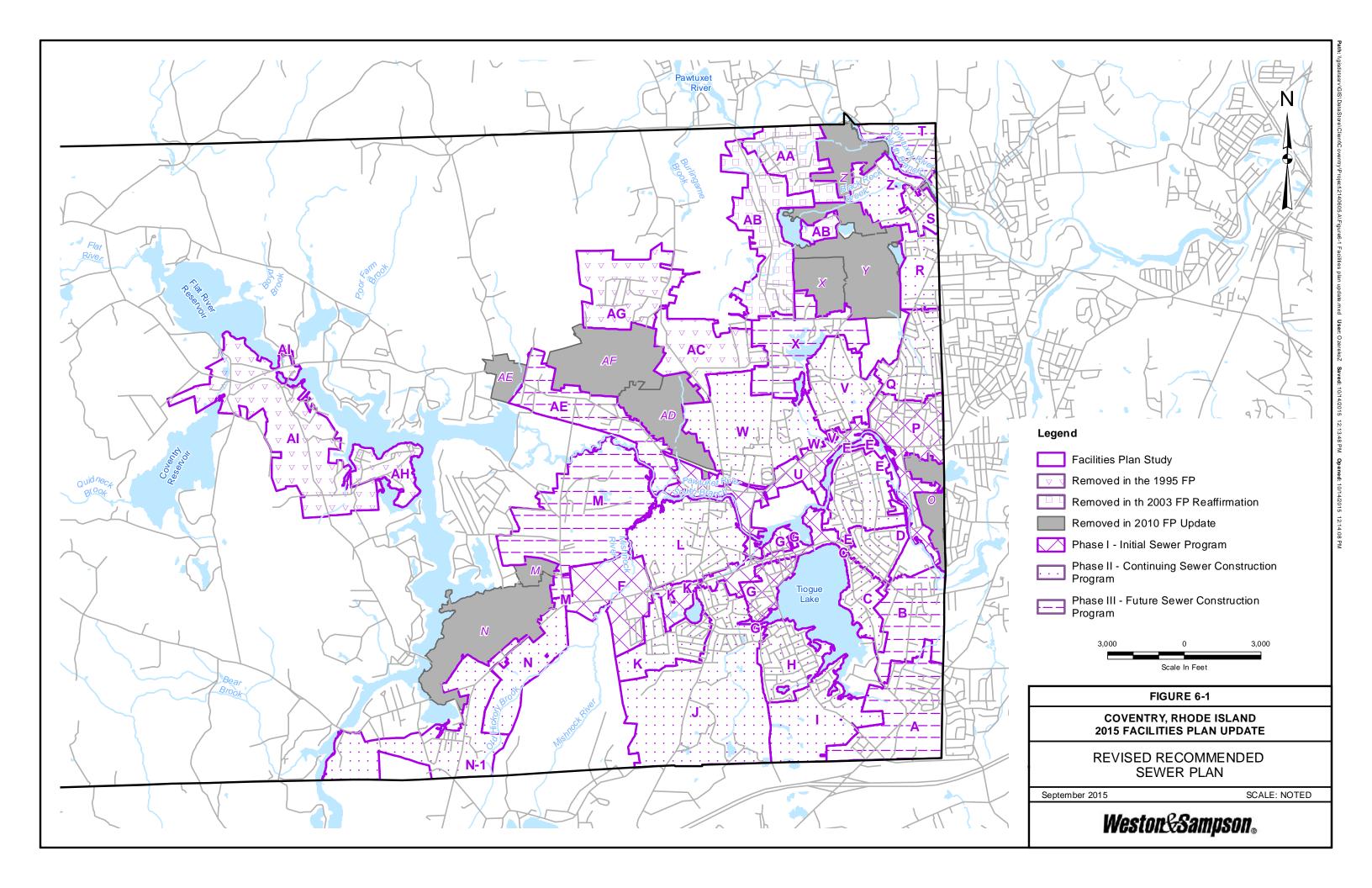
Robert Lawrence, Darton Street, asked that Public Comment be placed at the beginning of the meeting.

A motion was made by Councilman McGee seconded by Councilman Laboissonniere to adjourn meeting. All voted aye.

Town Clerk		

Facilities Plan Update

- 1. Introduction:
 - a. Facility Plan to be updated every 5-years for a 20-year future planning period. Last update was performed in 2010
 - b. History of this edition of the Facility Plan
 - 1995 Facilities Plan
 - 2003 Facilities Plan Reaffirmation
 - 2010 Facilities Plan Update
- 2. Goals of this Facility Plan Update:
 - a. Existing wastewater system
 - Hopkins Hill Road Sewer Project
 - Old North Road Sewer Project
 - New London Turnpike Sewer Project
 - Sewer Contracts 1-7
 - Woodland Manor PS/FM infrastructure acquisition
 - Sewers built by subdivision contractors/other misc. projects
 - b. Current and Future Flows into the Wastewater System
 - Total Coventry ADF Capacity = 2.25 MGD (excluding Woodland Manor)
 - Coventry Existing ADF = \sim 0.23 MGD (excluding Woodland Manor)
 - Woodland Manor ADF Capacity = 0.2 MGD
 - Woodland Manor Existing ADF = ~0.07 MGD
 - c. Assessment of the future wastewater planning
 - Future Sewer Contracts
 - 1. Sewer Contracts 8 10
 - 2. Hopkins Hill Road West Sewer Project
 - 3. Huron Pond Sewer Project
 - 4. Nooseneck Hill Road Sewer Project (added Planning Area N-1)
 - O&M and preventative maintenance items
 - 1. Town owned pump stations
 - Sandy Bottom Road Pump Station
 - Woodland Manor Pump Station
 - Industrial Drive Pump Station
 - 2. Flow Meter Calibration/Coordination
 - 3. Investigation program looking at the older areas of gravity sewers in Town (i.e. North Branch Interceptor, New London Turnpike, etc.)
- 3. Remaining Items:
 - a. Town Review and Comment
 - b. RI-DEM Review and Comment
 - c. Public Advertisement/Meeting
 - d. Final Submittal to RI-DEM



October 15, 2015 Wastewater Facilities Plan Update

2015 Facilities Plan Update

1. Introduction:

- a. Facility Plan to be updated every 5-years for a 20-year future planning period. Last update was performed in 2010.
- b. History of this Facility Plan
 - 1995 Facilities Plan
 - 2003 Facilities Plan Reaffirmation
 - 2010 Facilities Plan Update
- 2. Goals of this Facility Plan Update:
 - a. Assessment of the existing wastewater system (See attached Figure 3-11)
 - Hopkins Hill Road Sewer Project.
 - Old North Road Sewer Project.
 - New London Turnpike Sewer Project.
 - Sewer Contracts 1-7.
 - Woodland Manor PS/FM acquisition (including the increase in flow capacity in the West Warwick system
 - Sewers built by subdivision contractors/other misc. projects (i.e. Pine Ridge, Red Brook Meadow, etc.)
 - b. Assessment Current and Future Flows into the wastewater system (See attached Tables 4-3 to 4-5).
 - c. Assessment of the future wastewater planning (See attached Figure 4-3 and 6-1).
 - Future Sewer Contracts
 - 1. Sewer Contracts 8 10
 - 2. Hopkins Hill Road West Sewer Project
 - 3. Huron Pond Sewer Project
 - 4. Nooseneck Hill Road Sewer Project (added Planning Area N-1)
 - O&M and preventative maintenance items.
 - 1. Town owned pump stations
 - Sandy Bottom Road Pump Station
 - Woodland Manor Pump Station
 - Industrial Drive Pump Station.
 - 2. Investigation program looking at the older areas of gravity sewers in Town (i.e. Hopkins Hill Road, New London Turnpike, etc.)
- 3. Remaining Items:
 - a. Town Review and Comment
 - b. RI-DEM Review and Comment
 - c. Public Advertisement and Public Meeting
 - d. Final Submittal to RI-DEM

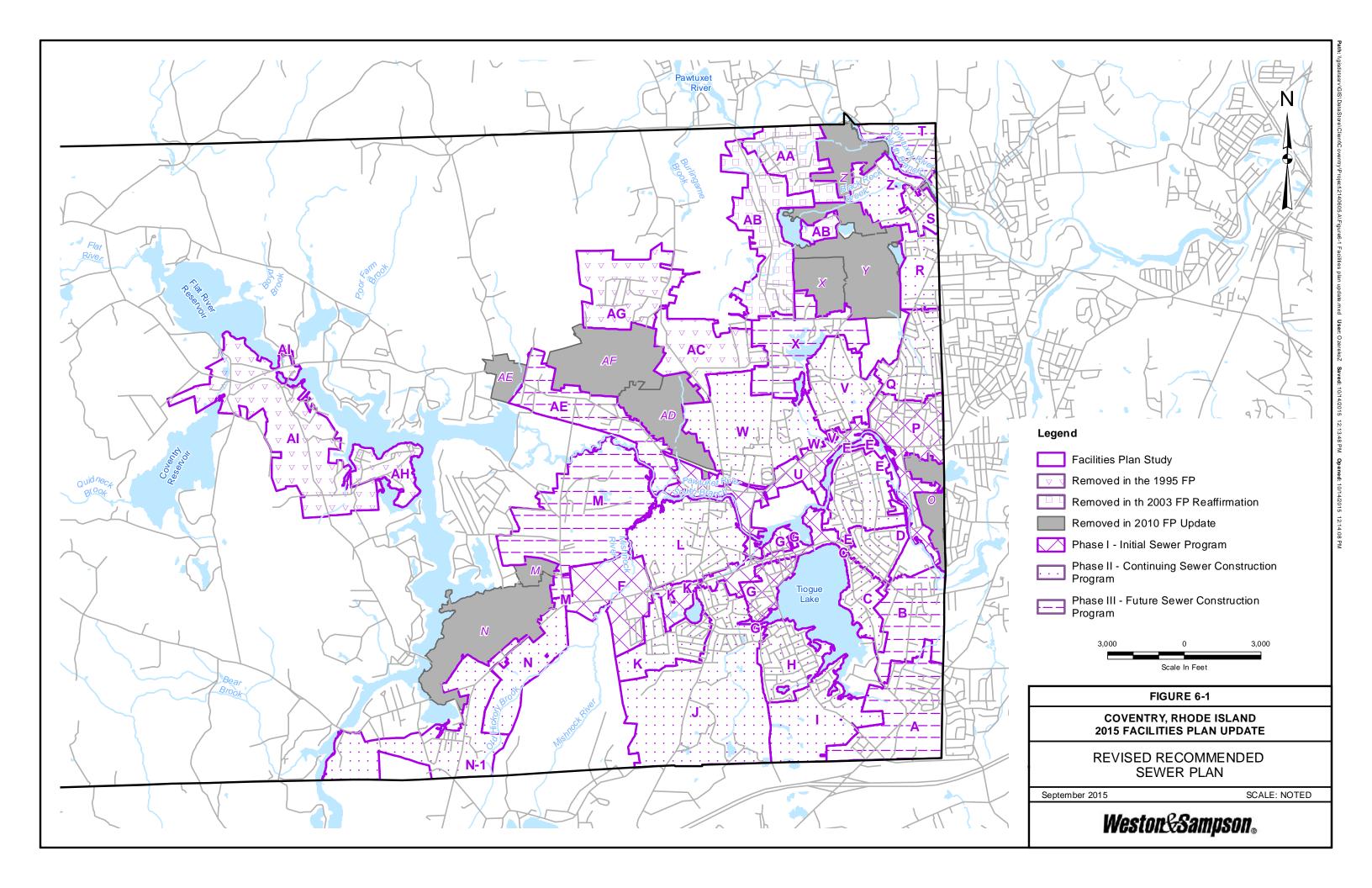


Table 4-3 Study Area Projected Wastewater Flows Average Daily Flow - Design Year 2015

Study Area	Domestic (gpd)	Industrial (gpd)	Commercial (gpd)	Institutional (gpd)	Infiltration and Inflow (gpd)	Total ADF (gpd)		
Α	1,873	922	63,588	0				
В	15,430	0	0	0	1,875	17,304		
С	0	0	0	0	0	0		
D	193	0	0	0	21	213		
E	600	0	0	0	60	660		
F	10,407	0	15,956	963	3,560	30,886		
G	3,396	0	0	0	607	4,002		
Н	0	0	0	0	0	0		
I	0	274	0	0	23	297		
J	14,685	0	0	0	1,307	15,992		
K	143	0	0	0	24	167		
L	743	0	287	0	172	1,202		
M	0	0	14,536	0	12	14,548		
N	0	0	0	0	0	0		
N-1	0	0	0	0	0	0		
0	1,578	0	132	0	2,040	3,750		
Р	3,269	8,186	75	0	592	12,122		
Q	870	0	0	0	170	1,039		
R	1,099	0	0	6	230	1,335		
S	656	0	0	0	110	766		
Т	4,949	920	16,016	0	527	22,412		
U	5,460	3,126	12,840	6,186	2,507	30,119		
V	15,493	0	20	0	827	16,341		
W	0	0	0	0	0	0		
Х	0							
Y		0						
Z	0	0						
AA	0 0 0 0 0 0 Not included in sewer program (2003).							
AB	Not included in sewer program (2003).							
AC	Not included in sewer program (1995).							
AD	Not included in sewer program (2010).					0		
AE	0			59				
AF	Not included in sewer program (2010).							
AG	1,090	0	0	0	0	1,090		
AH	Not included in sewer program (1995).							
Al	Not included in sewer program (1995).							
WM	15,751 0 48,741 205 1,496							

TOTAL TOWN	307,372
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Note:

This table updates information presented in Table F-1 of the 1995 Facility Plan and Table 4-3 of the 2010 Facilities Plan Update.

Domestic flow based upon 3 people/EDU and 70 gallons per day per capita (gpcd).

Industrial flow based upon 500 gallons per day per acre (gpad).

Commercial/Institutional flow based upon 300 gpad.

Infiltration/Inflow based upon 250 gallons per day per inch diameter mile (gpdim).

O:\Coventry RI\2140605 - 2014 Facilities Plan Update\2014 Update Report\Figures\Section 4\[Table 4-2 to Table 4-5 Sewer Flows & Population per Area 1.xis\]Table 4-3 Summary of Flows 2015

4-6



Table 4-4 Study Area Projected Wastewater Flows Average Daily Flow - Design Year 2035

Study Area	Domestic (gpd)	Industrial (gpd)	d) Commercial Institutional (gpd) (gpd)		Infiltration and Inflow (gpd)	Total ADF (gpd)		
Α	14,586				1,103	83,355		
В	18,160	0	0	0	2,038	20,198		
С	42,000	0	52	2,436	4,165	48,654		
D	54,583	0	602	0	7,630	62,814		
E	80,820	3,393	307	4,939	11,025	100,485		
F	36,023	1,457	56,912	1,359	15,050	110,801		
G	58,956	172	721	0	7,070	66,918		
Н	78,120	0	0	2,461	12,250	92,831		
I	22,050	837	12,338	3,384	3,780	42,389		
J	279,379	6,124	7,995	3,111	11,480	308,090		
K	59,993	0	1,695	0	9,730	71,419		
L	78,863	766	1,567	7,609	13,475	102,279		
M	1,260	0	15,576	0	109	16,945		
N	210	0	1,202	0	630	2,042		
N-1	43,470	2,059	17,209	1,010	4,760	68,508		
0	1,788	0	217	0	2,267	4,271		
Р	77,084	80,241	3,425	4,662	10,360	175,771		
Q	79,410	283	186	2,147	13,510	95,536		
R	29,029	0	123	6	4,235	33,394		
S	24,806	0	0	0	3,780	28,586		
Т	5,999	920	17,428	0	731	25,079		
U	64,021	3,126			13,230	114,857		
V	72,823	0	4,408	2,162	4,585	83,978		
W	62,710	0	563	37,845	7,385	108,503		
Х	1,470							
Y		Not included	d in sewer prog	ram (2010).		0		
Z	36,374	45,177						
AA	36,374 4,431 36 1,305 3,031 Not included in sewer program (2003).							
AB	Not included in sewer program (2003).							
AC	Not included in sewer program (1995).							
AD	Not included in sewer program (2010).					0		
AE	0	, § , ,						
AF	Not included in sewer program (2010).							
AG	1,090	0	0	0	0	1,090		
AH	Not included in sewer program (1995).							
Al	Not included in sewer program (1995).							
WM	15,751 0 48,741 205 2,094							

TOTAL TOWN	1,984,818
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Note:

This table updates information presented in Table F-1 of the 1995 Facility Plan and Table 4-3 of the 2010 Facilities Plan Update.

Domestic flow based upon 3 people/EDU and 70 gallons per day per capita (gpcd).

Industrial flow based upon 500 gallons per day per acre (gpad).

Commercial/Institutional flow based upon 300 gpad.

Infiltration/Inflow based upon 350 gallons per day per inch diameter mile (gpdim).

O:\Coventry RI\2140605 - 2014 Facilities Plan Update\2014 Update Report\Figures\Section 4\[Table 4-2 to Table 4-5 Sewer Flows & Population per Area 1.xis\]Table 4-3 Summary of Flows 2015



Table 4-5 Study Area Projected Wastewater Flows Average Daily Flow - Design Year 2065

Study Area	Domestic (gpd)	Industrial (gpd)	Commercial (gpd)	Institutional (gpd)	Infiltration and Inflow (gpd)	Total ADF (gpd)		
Α	66,876	2,796	74,333	0 14,800		158,805		
В	47,770	0	241	41	6,200	54,253		
С	42,630			4,760	49,879			
D	54,583	0	602	0	8,720	63,904		
E	80,820	3,393	307	5,012	12,600	102,133		
F	36,023	1,457	56,912	1,511	17,200	113,102		
G	60,846	172	721	0	8,080	69,818		
Н	78,120	0	0	2,461	14,000	94,581		
I	22,050	837	12,338	3,384	4,320	42,929		
J	279,379	6,124	7,995	3,111	13,120	309,730		
K	59,993	0	1,695	0	11,120	72,809		
L	78,863	766	1,567	7,609	15,400	104,204		
M	17,220	603	24,852	21,623	1,880	66,178		
N	420	0	1,802	0	720	2,942		
N-1	43,470	2,059	17,209	1,010	5,440	69,188		
0	1,998	0	217	0	5,440	7,655		
Р	77,084	80,241	3,425	4,785	11,840	177,374		
Q	82,350	283	186	2,147	15,440	100,406		
R	30,289	0	123	6	4,840	35,259		
S	25,436	0	0	0	4,320	29,756		
Т	35,814	7,468	18,323	0	6,200	67,805		
U	64,441	3,126	20,780	13,874	15,120	117,341		
V	72,823	0	4,408	2,162	5,240	84,633		
W	62,710	0	563	37,845	8,440	109,558		
Х	40,950	0	7,802	2,907	7,300	58,959		
Y		0						
Z	36,374	45,610						
AA	36,374 4,431 36 1,305 3,464 Not included in sewer program (2003).							
AB	Not included in sewer program (2003).							
AC	Not included in sewer program (1995).							
AD	Not included in sewer program (2010).					0		
AE	19,740			62,282				
AF	Not included in sewer program (2010).							
AG	1,090	0	0	0	0	1,090		
AH	Not included in sewer program (1995).							
Al	Not included in sewer program (1995).							
WM	15,751	0	48,741	205	2,393	67,090		

TOTAL TOWN 2,339,270

Note:

This table updates information presented in Table F-1 of the 1995 Facility Plan and Table 4-3 of the 2010 Facilities Plan Update.

Domestic flow based upon 3 people/EDU and 70 gallons per day per capita (gpcd).

Industrial flow based upon 500 gallons per day per acre (gpad).

Commercial/Institutional flow based upon 300 gpad.

Infiltration/Inflow based upon 400 gallons per day per inch diameter mile (gpdim).

O:\Coventry RI\2140605 - 2014 Facilities Plan Update\2014 Update Report\Figures\Section 4\[Table 4-2 to Table 4-5 Sewer Flows & Population per Area 1.xis\]Table 4-3 Summary of Flows 2015



Table 6-2

Summary of Conventional Sewer Collection System Costs

	Length of Sewer	Length of Lateral		Length of Sewer	ventional oew	Ť		÷	,	
	Interceptor	Sewer	Pump Stations	Force Main	Approx. No. of		Total Sewer			
Area	(feet)	(feet)	Required	(feet)	Properties Served		nstruction Cost	С	Cost per Unit	Comments
A	0	15,800	1	1300	230	\$	4,152,000.00		18.052.17	To Existing New London Tpk Sewer
В	0	7,850	1	750	127	\$	2,023,000.00		15,929.13	To West Warwick thru Tiogue Avenue
C	0	7,900	0	0	173	\$	1,817,000.00		10,502.89	To Tiogue Avenue Interceptor - East
D	1,100	12,900	0	0	264	\$	3,352,000.00		12,696.97	To Existing Washington Interceptor
E	3,250	16,100	1	750	306	\$	5,398,500.00		17,642.16	To Existing Washington Interceptor
F	0	0	0	0	0	\$	-	-	N/A	To Existing Tiogue Interceptor & Sandy Bottom Rd. PS
G	600	7,125	0	0	143	\$	1,848,750.00	\$	12.928.32	To Tioque Avenue Interceptor - East
Н	2,475	19,400	1	750	357	\$	5,598,750.00		15,682.77	To Tiogue Avenue Interceptor - East
ï	0	7,100	1	1,525	114	\$	1,988,750.00		17,445.18	To Tiogue Avenue Interceptor - East
J	0	13,825	1	900	224	\$	3,466,750.00		15,476.56	To Existing Hopkins Hill Rd. Sewer
K	0	17,825	0	0	300	\$	4,099,750.00		13,665.83	To Existing Hopkins Hill Rd. Sewer
1	0	23,400	0	0	348	\$	5,382,000.00		15,465.52	To Tioque Avenue Interceptor - West
M	0	3,100	0	0	32	\$	713,000.00		22.281.25	To Tioque Avenue Interceptor - West
N	0	400	0	0	3	\$	92,000.00		30,666.67	
N-1	0	11,125	1	4,000	222	\$	3,298,750.00		14,859.23	Added (2015)
0	0	1.750	0	0	26	\$	402,500.00		15,480.77	To Existing Washington Interceptor. Portions elim. (2009)
P	2,600	13,000	0	0	275	\$	3,900,000.00		14,181.82	To Existing Washington Interceptor
Q	0	23,850	1	800	327	\$	5,956,500.00		18,215.60	To Existing Washington Interceptor
R	0	6,750	0	0	100	Φ	1,552,500.00		15,525.00	
S	2,250		0	0	74	Φ			21,364.86	To North Branch Interceptor
T	,	3,450	-	-		ф	1,581,000.00			To North Branch Interceptor
	1,800	4,550	0	0	80	\$	1,676,500.00	\$	20,956.25	To North Branch Interceptor
U	0	0	0	0	0	\$	-		N/A	To Existing Sandy Bottom Rd. PS
V	3,000	7,550	0	0	150	\$	2,786,500.00		18,576.67	To Existing Washington Interceptor
W	0	16,725	1	450	212	\$	4,037,250.00		19,043.63	To Existing Washington Interceptor
Х	0	11,650	1	750	175	\$	2,897,000.00	\$	16,554.29	To Existing Washington Interceptor. Portions elim. (2009)
Y	0	0	0	0	0	\$	-		N/A	Eliminated from Sewer Program (2009)
Z	0	5,725	1	1,200	87	\$	1,574,750.00	\$	18,100.57	To North Branch Interceptor. Portions elim. (2009)
AA	0	0	0	0	0	\$	-	<u> </u>	N/A	Eliminated from Sewer Program (2003)
AB	0	0	0	0	0	\$	-	<u> </u>	N/A	Eliminated from Sewer Program (2003)
AC	0	0	0	0	0	\$	-	<u> </u>	N/A	Eliminated from Sewer Program (1995)
AD	0	0	0	0	0	\$	-		N/A	Eliminated from Sewer Program (2009)
AE	0	0	0	0	16	\$	108,000.00	\$	6,750.00	To Existing Sandy Bottom Rd. PS. Portions elim. (2009)
AF	0	0	0	0	0	\$	-		N/A	Eliminated from Sewer Program (2009)
AG	0	0	0	0	0	\$	-		N/A	Eliminated from Sewer Program (1995)
AH	0	0	0	0	0	\$	-		N/A	To Community OWTS System
Al	0	0	0	0	0	\$	-		N/A	Eliminated from Sewer Program (1995)
TOTALS	17,075	258,850	11	13,175	4,365	\$	69,703,500.00	\$	15,968.73	

NOTES

O:\Coventry R\\2140605 - 2014 Facilities Plan Update\2014 Update Report\Figures\Section 6\[Table 6-2 - Summary of Sewer Cost.xls\]Summary of Areas and Cost

^{1.} Costs in this table are based on 20 Cities ENR=10038.80 (June 2015)

^{2.} See Appendix F for a detailed breakdown of pipeline lengths and costs.

